

## DECLARATION

I declare that this research report is my own, unaided work. It is being submitted for the Degree of Masters of Science in Engineering in the University of the Witwatersrand, Johannesburg. It has not been submitted before for any degree or examination in any University.

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(Signature of Candidate)

\_\_\_\_\_ day of \_\_\_\_\_ (year) \_\_\_\_\_

## ABSTRACT

A variety of carbonaceous materials are being used for the production of ferrochromium. Reductant materials include carbons such as coal, coke and char. Due to complexity and heterogeneity of carbonaceous reducing materials and a wide range of process requirements, the selection of the most appropriate reducing agent will depend on a number of considerations such as availability of raw material and associated costs, product and process requirements.

Matching the correct carbon reductant for each specific process and product requirements has become a vital function of the ferrochrome industry. This selection process however, has become increasingly difficult. In many cases, the substitution of new a reductant, despite being similar in all relevant chemical specification characteristics to previous material, has resulted in different performance properties relative to that expected.

An investigation prior to the usage of the substituting reductant in the submerged arc furnace was done in order to obtain required performance properties. The investigation concerned the search for a more reliable model in characterizing the reductant according to their reactivity performance, and using the model parameters to choose the appropriate reductant.

The model chosen for this investigation was the Arrhenius model. Sintered chromite ore was reduced with the reductant under investigation in a Thermogravimetric analyzer (TGA) at different temperatures. The resultant data was then fitted into the Arrhenius model to obtain the indication of the reactivity of the reductant.

The TGA tests suggest that the Vietnamese anthracite has the highest reactivity since its activation energies are the lowest and requires less energy to induce the reductant reaction. The tests also suggest that the rate controlling mechanism is the diffusion of species to the reactive site since the effective diffusion constant is of the order  $10^{-10}$  to

$10^{-11}$ , which is far less than the chemical rate constant of the order  $10^{-6}$ . A generalized rate model developed to describe the reduction of chromite shows that at given particle size and up to a reduction of 40%, the rate of reduction is controlled mainly by interfacial-area chemical reaction, and after which the rate is dominated by diffusion.

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## NUMECLATURE

$R_T$  = rate at temperature T (units/sec).

$R_{T_0}$  = rate at temperature  $T_0$  (unit/sec).

$\Delta E$  = activation energy (J/mol).

$R$  = gas constant (J/(mol.K)).

$t_i$  = reaction time (min).

$\tau$  = chemical rate control constant (min).

$t^*$  = dimensionless time for a chemical reaction control.

$\sigma_s^2$  = ratio of dimensionless time for chemical reaction controlled process to  
Dimensionless time for diffusion controlled process.

$X_i$  = fraction reduction of sintered chromite ore.

$k$  = chemical reaction rate constant ( $s^{-1}$ ).

$\rho$  = density ( $kg/m^3$ ).

$F_p$  = shape factor (3 for spherical particles).

$V_p$  = particle volume ( $m^3$ )

$A_p$  = particle cross sectional area ( $m^2$ )

$b$  = stoichiometric factor

$D_e$  = effective diffusion coefficient ( $m.s^{-1}$ )

## CHAPTER 1: INTRODUCTION

### 1.1 Background

Various smelters in South Africa including Assmang Chrome Machadodorp produce high carbon ferrochromium. The production is accomplished by simultaneously smelting chromite ore, reductant (char, coal and coke), fluxes (limestone and serpentine) and silica (quartz) in a submerged arc furnace.

The electric arc and the electrical resistance of the charge generate the heat required for smelting. The heat is most intense at the electrode tip, and this is where most of smelting reactions occur. The smelting reactions involve the reduction of the metal oxides to the metallic state with the formation of a slag. After the initial heating and subsequent reaction of the charge, the reaction products (ferrochromium and slag) drain to the hearth of the furnace. The metal is tapped into a ladle, and cast into a sandpit from where it is broken into smaller pieces for transport purposes.

### 1.2 Motivation

Coal and coke are the main source of carbon for reduction reactions in the production of ferrochromium. The increasing cost of coke and the fact that suppliers are dwindling, as are the availability of coking coals, leads to consumers in the ferroalloy industry searching for alternative sources of carbon. Such alternatives include char, bituminous coal and anthracite. (Visser, 2000, Hendriktz, Sun, 1997)<sup>1</sup>.

A shortage of good quality South African coking coal has led to significant decrease in the production of coke, suitable for utilisation in submerged arc furnaces, at Iscor's coking facilities. The shortage of supply resulted in several price increases which, together with possible discontinuation of required quantities, prompted several investigations into alternative coke suppliers (i.e Zimbabwe and China coke) by Assmang

Chrome Machadodorp. As a result a number of coke suppliers have been changed over the years since 1996.

China nuts coke has been found to complement the operation of the submerged arc furnace in the production of chromium, and have been blended with other reductant in use. In 2003 and 2004, there have been several increase in the cost of China nuts coke, and a decrease in its availability which has led to a higher cost of producing a ton of ferrochromium. This has led Assmang Chrome Machadodorp to look for an alternative cheaper and effective reductant (in terms of chromium recoveries, kg of reductant per ton of metal produced and MW of power consumed per ton of metal produced).

### **1.3 Objective**

Previous investigations done only concentrated on the alternative cokes, in this investigation the aim will be to substitute coke with anthracite. Anthracite is relatively cheaper than coke. Although the alternative anthracite might be of similar chemical analysis when compared to China nuts coke, other physical properties (reactivity, resistivity and strength) considered to be important parameters with regard to desirable burden characteristics during the production of high carbon ferrochromium will differ considerably.

**Table1 : Price for different reductants**

<b>Reductant</b>	<b>Price (R/ton)</b>
<b>China nuts coke</b>	2897.28
<b>Argentine coke</b>	2292.78
<b>Springlake anthracite</b>	442.28
<b>Vietnamese anthracite</b>	745.28

## CHAPTER 2: LITERATURE REVIEW

The most important property of a reducing agent used in submerged arc furnace is electrical resistivity of the material. This property depends on the type of material, processing conditions, material sizing, operating temperatures and pressures within the furnace mix. High burden resistivity is necessary for good overall heat distribution. It depends on resistivity of the reducing agent, a stable coke bed at the tip of the electrodes, volume fraction of the reductants, carbon content and particle size.

Higher resistivity is obtained for the burden where the particle size of the reductant is higher than those of other burden components (Dijs, H.M., Smith, DJ)<sup>2</sup>. Electrical resistivity is a structure sensitive parameter that reflects the internal structure. Therefore the electrical resistivity of carbonaceous material can be correlated with fraction of ordered carbon and reactivity (Feng, B., Bhatia, S.K. and Barry, J.C.)<sup>3</sup>.

Reactivity of reductants towards reduction of oxides plays an important role in many metal-smelting processes. In general, reactivity decreases with the increase in the degree of graphitisation. In addition, the presence of carbon atoms in the amorphous phase or in aliphatic side chains also leads to an increase in reactivity. The combustion/gasification rate for different reduction materials can therefore be significantly different. As combustion proceeds, reactivity decreases due to loss of volatile matter, enhanced thermal annealing and decreased concentration of active site (Smith, I.W.)<sup>4</sup>.

In addition to structural order, physical characteristics such as pore size distribution and surface area, and composition and concentration of ash impurities present in the carbonaceous material also play an important role. Primary electrical contact between the electrode and charge is through a coke bed and electrical properties of this zone are important as it determines the energy and the temperature distribution in the furnace (Olsen, S.E. and Lindstad, T.)<sup>5</sup>.

## 2.1 Characterisation of carbonaceous materials

Carbonaceous materials are complex systems, which are generally heterogeneous in nature. They exhibit a wide variety of physical and chemical properties and chemical properties. While chemical characteristics control the reactivity of the reductant and influence the amount of reduction material used, product quality and energy consumption in the smelting process, physical properties affect the efficiency and productivity of operation to a certain extent. The main carbonaceous materials used in the production of ferrochrome are mainly coal, coke and char.

Coal is composed of mainly carbon, hydrogen, nitrogen, sulphur and inorganic matter. Coal is characterised by its rank, type and grade. Rank characterises the degree of metamorphism of coal and is an important criterion for determining the technological usage of coal. Degree of impurities, maceral composition and calorific value determine the type and grade of coal. Other factors such as texture, porosity, density also affects coal quality. Traditionally, coal selection criteria for ferroalloys production are volatile matter content, ash content, and chemistry and reactivity. Since other reductant material like char and coke are produced from coal their properties will be derived and affected by properties of parent coal material.

Char is formed during pyrolysis, that is the first stage of coal combustion, when heated particles are devolatilised yielding a carbon-rich solid residue. Char properties are affected by chemical and physical properties of the parent coal, temperature and time history.

Coke is produced by heating coal blend in the absence of oxygen to about 1100°C. Quality and properties of coke are affected by the coal rank, fluidity, maceral and mineral matter composition as well as processing conditions. Traditionally, chemistry, particle size, reactivity and strength after reaction are considered as the most important properties of metallurgical coke for blast furnace operations. Electric arc furnace coke, however, requires higher reactivity, lower strength and proper electrical resistivity.



### 2.2.1 Characterisation technique

A variety of analytical tests have been developed to characterize properties of various carbonaceous materials. Many analytical procedure are available around the world from international standards organisations.

Basic chemical analysis to determine concentrations of moisture, ash, volatile matter, and fixed carbon, supplemented with elemental analysis are generally performed for a basic characterisation of most carbonaceous materials.

Most of mechanical and physical tests used were developed for classifying coals for coke making. These include measurements of specific gravity, free- swelling index, grindability and ash fusion temperature. A reacted coke sample is also used to determine Coke Strength after Reaction (CSR), which is an important property, particularly to blast furnace operations. In the Nippon test a sample is tumbled at 20 rev/min. Tumbling is performed only after extensive reactions with carbon dioxide. CSR is defined as the weight percentage of coke larger than 10 mm in size after 600 revolutions<sup>6</sup>.

Reactivity tests play an important role in the assessment of the quality of reduction materials for metallurgical applications. These are based on the gasification of carbonaceous materials in the presence of some oxidizing gas such as carbon dioxide, oxygen, air or steam. There is no universally accepted standard procedure, but reactivity test of coke towards CO<sub>2</sub> developed at Nippon Steel Corporation in Japan in early seventies is widely recognised around the world. In the test, a sample (200g of 20mm particle size) is exposed to CO<sub>2</sub> flow for two hours at 1100°C. The percentage of mass loss is referred to as reactivity.

In addition to the convectional techniques, characterisation of various carbonaceous materials at an atomic level has gained significance. A number of experimental techniques such as XRD, TEM, SEM, FESEM, and HRTEM supplemented with computer simulations are used nowadays to characterise carbons at an atomic level<sup>7</sup>.

Results obtained from these studies have provided a better understanding of the structure of carbonaceous materials, the evolution after heat treatment and oxidation, and interfacial phenomena.

In ferrosilicon production, major gaseous reagent is silicon monoxide. SiO reactivity is the ability of the reducing agent to react with gaseous silicon monoxide at 1650°C to form silicon carbide and carbon monoxide. The SINTEF test<sup>8</sup> is based on the volume of SiO gas required by the reducing agent to attain 10% level of CO in off gases. SiO reactivity generally decreases with coal rank. Coke having isotropic carbon forms proved to be more reactive than cokes with anisotropic carbon forms.

## **2.2 Reaction mechanism in ferrochrome production**

The Chrome charge to the furnace is principally in the form of lump ore and/or pellets. The lump material consists of chromite grains surrounded by solidified host rock. Pellets are made from chromite concentrates that have been agglomerated and pre-treated to form spherical particles. The grain size and microstructure of the chromites are variable from dense rounded grains in the lump to highly fractured acicular grains in the pellets. The particle size ranges of lump ore, pellets and coke are controlled to maximise bed permeability. The chromite forms part of the spinel crystal family, having the general form  $(\text{Fe}^{2+}, \text{Mg}^{2+})\text{O} \cdot (\text{Al}^{3+}, \text{Cr}^{3+}, \text{Fe}^{3+})_2\text{O}_3$ .

As the charge descends and passes through the reaction zones various reactions occur during metal alloy formation. The mechanisms and kinetics of gaseous reduction of solid South African chromites ore have been studied by a number of workers<sup>9</sup>. There appears to be general agreement that in the loose charge zone iron is preferentially reduced from the solid chromite grains by reaction with carbon monoxide gas produced in the lower part of the furnace.

The rate limiting reaction mechanism during the gaseous reduction of dense chromite grains is the ionic diffusion of metal species in the solid spinel phase. Soykan et al<sup>10</sup> proposed that the reduction of chromite occurs by the following sequence:

- a) Initially  $\text{Fe}^{3+}$  and  $\text{Fe}^{2+}$  at the surface of the chromite particle are reduced to the metallic state. This is followed by immediately by the reduction of  $\text{Cr}^{3+}$  ions to the divalent state.
- b)  $\text{Cr}^{2+}$  ions diffusing toward the centre of the particle reduce the  $\text{Fe}^{3+}$  ions in the spinel under the surface of the particle to  $\text{Fe}^{2+}$  at the interface between the inner and outer cores.  $\text{Fe}^{2+}$  ions diffuse towards the surface, where they are reduced to metallic iron.
- c) After the iron has been completely reduced,  $\text{Cr}^{3+}$  and any  $\text{Cr}^{2+}$  that is present are reduced to the metallic state, leaving an iron- and chromium- free spinel,  $\text{MgAl}_2\text{O}_4$ .

The partially altered chromite contains a dispersion of fine iron/chromium metal alloy particles. The solid alloy, formed in the early stage of reduction as the charge descends and is heated through the loose charge zone, is low in chromium. As the reaction time and temperature increases, the chromium concentration in the alloy increases. In the later stages of reduction chromium- iron carbides are observed to form<sup>11</sup>.

The reaction proceeds topochemically, from the surface of the particle in the case of dense ore or from the surface of individual grains for porous materials. In cross section, this compositional variation within a grain is seen in the form of a core of primary spinel surrounded by continuous shell of secondary spinel of variable composition. The composition and thickness of the shell varies with slag composition, temperature, oxygen potential and reaction time. The Fe-Cr alloy forms initially on the outer surfaces of the grains or along microcracks.

The rate and extent of reduction of the chromite ore is dependent on the chemical composition of the chromite, grain and particle size, porosity, and temperature history in pre-treatment and in the furnace<sup>12</sup>. Chromite ores are not uniform in composition; they

vary widely with source of material particularly in iron concentration. The relationship between the degree of reduction and the chromium reduction therefore depends on the initial composition.

Since the rate limiting reaction mechanism involves solid-state diffusion, diffusion path length is a critical factor determining reaction rate. The ionic flux to the gas/solid interface is inversely proportional to the distance, so that reduction rate is enhanced with decreasing particle and grain size. Even cracks and sub-grains boundaries within the grains enhance the rates of reduction of individual chromite grains. The reduction rates of individual grains in pelletised materials are significantly faster than in lump material because of the smaller grain sizes and the higher porosities of the pellets.

The rate of reduction of the chromite can also be influenced by the composition and proportion of matrix material in the particles, since this material fuses and eventually melts as the charge descends through the furnace. The formation of the liquid phase can have multiple effects. If there is a high proportion of matrix material the porosity of the ore, and consequently the ease of reducing gas penetration into the particle, may be diminished. On the other hand the partially reduced spinel may react with and dissolve in the molten slag phase, decreasing the effective particle size and influencing the temperature at which the grains in the chromite particles become dispersed in the bulk.

### CHAPTER 3: METHOD OF STUDY

A common method of test for the reactivity of the reductant (i.e coke or coal) is the exposure of packed bed containing 200g of 20-mm diameter particles to flowing CO<sub>2</sub> at 1100°C for 2hours. The percentage mass loss (by the Boudouard reaction) is quoted as the “coke reactive index” (CRI).

While it is feasible to predict and measure the CRI values, it is not obvious what values of these indices are desirable for coke used in ferroalloy production. Given the apparent importance of CO generation (in direct reduction reactions), it appears that a high reactivity would be required. On the other hand, the primary electrical contact between the electrode and the charge is through a coke bed directly beneath the electrode tips. Use of a less reactive coke would presumably favour maintenance of such coke bed. Smaller-sized and more-reactive coke is stated to give higher resistivity (A deWaal, IJ Barker)<sup>13</sup>. These counteracting requirements perhaps partially explain the general use of a mixture of reductants in ferroalloy production.

In this investigation an alternative method of testing for reactivity was utilized. This method involves reducing the sintered chromite ore with a chosen reductant in a Thermo-gravimetric analyser (TGA) at different temperatures. In this method reactivity was redefined as the inherent capacity of the reductant to induce the reduction reactions of the ore or the resistance to the reduction process. A model which is close (or compliment) to this definition was found to be the Arrhenius model :

$$R_T = R_{T_o} \exp \left[ \frac{-\Delta E}{R} \left( \frac{1}{T} - \frac{1}{T_o} \right) \right] \quad [1]$$

where  $R_T$  and  $R_{T_o}$  are the rates (in units/sec) at temperature  $T$  and  $T_o$  respectively.

$\Delta E$  (J/mol) is the activation energy of the reaction which in this case will be the measure of the capacity of the reductant to induce the reduction reactions of the ore (its reactivity).

$R$  (J/(mol.K)) is a gas constant.

Previous investigations done by R.H. Eric<sup>14</sup> on the solid state reduction of chromite ore suggested that the reaction mechanism of the reduction of the ore involves both the chemical reactions and the diffusion of ionic species ( $\text{Fe}^{3+}$ ,  $\text{Fe}^{2+}$ ,  $\text{Cr}^{3+}$ ,  $\text{Cr}^{2+}$ ,  $\text{Mg}^{2+}$ ,  $\text{Al}^{3+}$  and  $\text{Ti}^{4+}$ ) from and to the reaction sites. This has prompted the use of a mixed rate control model to describe the kinetics of the reduction process of the ore:

$$t_i = \tau \mathcal{G}_c(X_i) + \tau \sigma_s^2 \mathcal{P}_d(X_i), \text{ mixed rate control} \quad [2]$$

$$\mathcal{G}_c(X_i) = 1 - (1 - X_i)^{1/3}, \text{ chemical rate control conversion factor} \quad [3]$$

$$\mathcal{P}_d(X_i) = 1 - 3(1 - X_i)^{2/3} + 2(1 - X_i), \text{ diffusion rate control conversion factor} \quad [4]$$

$$\tau = \frac{t}{t^*} \quad [5]$$

where :

$t^*$  is the dimensionless time for a chemical reaction controlled process

$\sigma_s^2$  is the ratio of dimensionless time for a chemical reaction controlled process to dimensionless time for diffusion controlled process.

$X_i$  is the fraction reduction of the sintered ore and was calculated by use of the following equation :

$$X_i = \frac{\text{Mass of CO evolved}}{\frac{28.01}{15.999} \times \text{mass of original removable oxygen}} \quad [6]$$

From equation [2] it follows that :

$$k = \frac{\rho F_p V_p}{\tau b A_p}, \text{ chemical reaction rate constant} \quad [7]$$

$$D_e = \frac{k V_p}{2 \sigma_s^2 A_p}, \text{ effective diffusion coefficient} \quad [8]$$

where :

$\rho$  is the density ( $\text{kgm}^{-3}$ )

$F_p$  is the shape factor (3 for spherical particles)

$V_p$  is the volume ( $\text{m}^3$ ) =  $\frac{4}{3}\pi r^3$  ( $r$  is the particle radius)

$A_p$  is the cross sectional area ( $\text{m}^2$ ) =  $4\pi r^2$  ( $r$  is the particle radius)

$b$  is the stoichiometric factor ( $\frac{1}{4}$  for the reduction of  $\text{FeCr}_2\text{O}_4$  spinel)

The chemical reaction rate constant ( $k$ , in  $\text{s}^{-1}$ ), and the effective diffusion coefficient ( $D_e$ , in  $\text{ms}^{-1}$ ) obtained at different temperatures are then fitted into the Arrhenius equation [1].

The reactivity of the reductant will then be obtained from the fit of the data to the Arrhenius equation. In order to access the reliability of the method and the data obtained, tests will be done in the arc furnace whereby three different reductants under investigations will substitute the China nuts coke, or be blended with it.

The results in terms of Chromium recovery, MW power consumption per ton of metal produced, and kg of ore per ton of metal produced will be correlated to the reactivity values. The stability of the smelter furnace operation will also be closely monitored by monitoring the electrode currents, voltages and the furnace mix resistance. For these tests, 20000 metric tons of each reductant under investigation was ordered.

## CHAPTER 4: EXPERIMENTAL PROCEDURE

Thermogravimetric analyses (TG) was carried out with a Simultaneous Thermal Analyzer STA 409 PC Luxx as shown in figure 1.

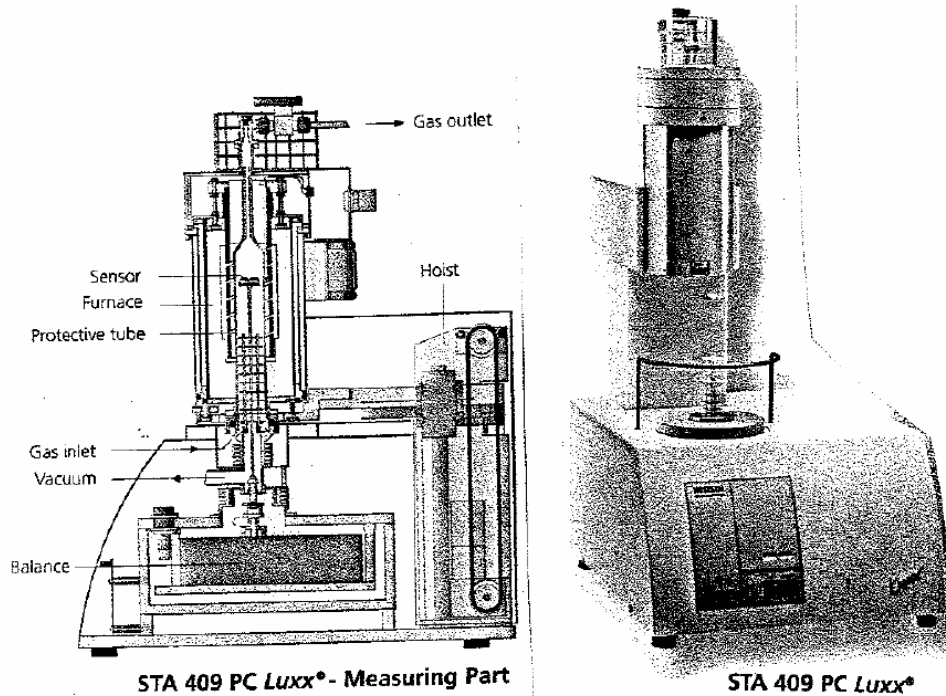


Figure 1: Simultaneous Thermal Analyzer STA 409 PC Luxx.

The reaction mixture consisted of sintered chromite ore (chemical analyses given in table 2), and a reductant under investigation. Reductants under investigation were China nuts coke, Argentine coke, Vietnamese anthracite and Springlake anthracite, and their chemical analyses is given in table 3.

Table 2: Chemical analyses of the sintered chromite ore.

	Cr	Fe total	Fe <sup>2+</sup>	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	MgO	CaO	Na <sub>2</sub> O	K <sub>2</sub> O	Zn
%	30.2	19.2	2.2	3.1	12.9	11.0	0.39	0.10	0.12	0.12



Table 3: Chemical analyses of Reductants under investigation.

	Fixed carbon	Ash	Volatiles
China nuts coke	88.85%	9.73%	1.42%
Argentine coke	88.16%	10.48%	1.36%
Vietnamese anthracite	92.86%	4.03%	3.11%
Springlake anthracite	80.1%	10.83%	9.07%

Both the sintered chromite ore and the reductant under investigation were ground and sized to  $-53 + 75$  microns. The reaction mixture was heated in an alumina sample holder from room temperature to the selected reaction temperature at a heating rate of  $10^{\circ}\text{C}$  per minute, and then held for 120 minutes. The selected temperatures were  $1190^{\circ}\text{C}$ ,  $1240^{\circ}\text{C}$ ,  $1290^{\circ}\text{C}$ ,  $1340^{\circ}\text{C}$  and  $1390^{\circ}\text{C}$ . The furnace was flushed continuously with nitrogen gas at a flowrate of  $70\text{Nml}\cdot\text{min}^{-1}$ . The mass loss caused by the loss of volatile matter from the reductant and the evolution of CO gas by the reduction reactions was measured continuously by the Simultaneous Thermal analyzer.

Literature suggest that the reduction of chromite ore starts around  $900^{\circ}\text{C}$  (M. Honkaniemi, H. Krogerus, J. Daavittila and P. Oikarinen)<sup>15</sup>. The mass loss due to volatiles is calculated from the observed mass loss measured from room temperature till  $900^{\circ}\text{C}$ , and the mass loss due to CO evolution is calculated from the observed mass loss from  $900^{\circ}\text{C}$  till the specified reaction time (i.e. after 120 minutes, at the selected reaction temperature). The percentage reduction at a given time and selected reaction temperature was then calculated by use of equation [6].

## CHAPTER 5: EXPERIMENTAL RESULTS

The mass of removable oxygen in equation [6] is obtained as follows:

The sintered chromite ore contain 30.2% Cr, 17.0% Fe<sup>3+</sup>, and 2.2% Fe<sup>2+</sup>.

If we consider 100mg of sintered chromite ore, then 30.2mg is Cr, 17.0mg is Fe<sup>3+</sup>, and 2.2mg is Fe<sup>2+</sup>.

By stoichiometry: 55.845g Fe<sup>2+</sup> is contained in 71.844g FeO

Then 2.2mg Fe<sup>2+</sup> is contained in 2.8303mg FeO

Hence oxygen in 2.8303mg FeO = 0.6303mg

By stoichiometry: 111.69g Fe<sup>3+</sup> is contained in 159.687g Fe<sub>2</sub>O<sub>3</sub>

Then 17.0mg Fe<sup>3+</sup> is contained in 24.305mg Fe<sub>2</sub>O<sub>3</sub>

Hence oxygen in 24.305mg Fe<sub>2</sub>O<sub>3</sub> = 7.305mg

By stoichiometry: 103.992g Cr is contained in 151.989g Cr<sub>2</sub>O<sub>3</sub>

Then 30.2mg Cr is contained in 44.139mg Cr<sub>2</sub>O<sub>3</sub>

Hence oxygen in 44.139mg Cr<sub>2</sub>O<sub>3</sub> = 13.939mg

Total mass of removable oxygen = 21.8743mg in 100mg of sintered chromite ore sample.

### 5.1 Determination of the reactivity of Argentine coke.

199.5 mg of sintered chromite ore and 58.8mg of Argentine coke was used. The mixture contains 20% excess carbon required to react with Cr<sub>2</sub>O<sub>3</sub> and FeO and Fe<sub>2</sub>O<sub>3</sub> in the chromite ore. The reaction mixture was heated in an alumina sample holder from room temperature to the selected reaction temperature at a heating rate of 10°C per minute, and then held for 120 minutes.

The selected temperatures were 1190°C, 1240°C, 1290°C, 1340°C and 1390°C. Literature suggest that the reduction of chromite ore starts around 900°C (M. Honkaniemi, H. Krogerus, J. Daavittila and P. Oikarinen)<sup>15</sup>. Hence to compute the fraction reduction of the sintered ore ( $X_i$ ) at the selected temperature, a correction should be made to take into account the reduction that occurs from 900°C to the selected temperature. Correlation of the fraction reduction with temperature has been found to be in the form (Y. Yang, Y. Xiao and M.A. Reuter)<sup>16</sup>:

$$X_{corr} = a(T - 900) + b(T - 900)^2 + c(T - 900)^3 \quad [9]$$

where T is the temperature in °C. The data obtained in appendix 1 was fitted into equation [9] (as shown in graph 1) using the curve fitting technique as follows:

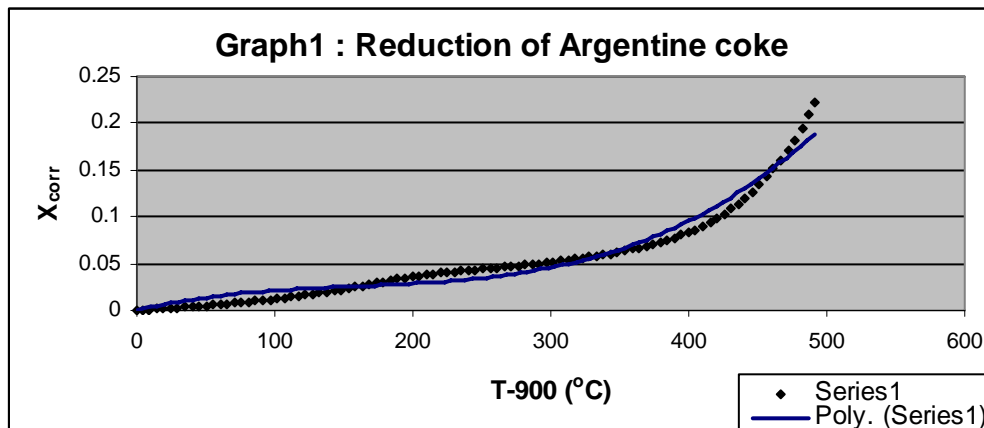
$$\sum Y = a \sum X + b \sum X^2 + c \sum X^3 \quad [10]$$

$$\sum XY = a \sum X^2 + b \sum X^3 + c \sum X^4 \quad [11]$$

$$\sum X^2Y = a \sum X^3 + b \sum X^4 + c \sum X^5 \quad [12]$$

$$\sum X^3Y = a \sum X^4 + b \sum X^5 + c \sum X^6 \quad [13]$$

$$R^2 = \frac{\sum (Y_{fit} - \bar{Y})^2}{\sum (Y - \bar{Y})^2} \quad [14]$$



Graph 1: Reduction of sintered chromite ore using Argentine coke.

The fit yields:

$$X_{corr} = 0.000358088(T - 900) - 1.849494 \times 10^{-6}(T - 900)^2 + 3.88085 \times 10^{-9}(T - 900)^3$$

$$R^2 = 0.967506$$

Table 4: Values of  $X_{corr}$  at different temperatures.

T (°C)	$X_{corr}$
1190	0.042953
1240	0.060482
1290	0.088555
1340	0.130083
1390	0.187978

### 5.1.1 Determination of $\tau$ and $\sigma_s^2$ at 1190°C

$$X_{corr} \text{ at } 1190^\circ\text{C} = 0.042953$$

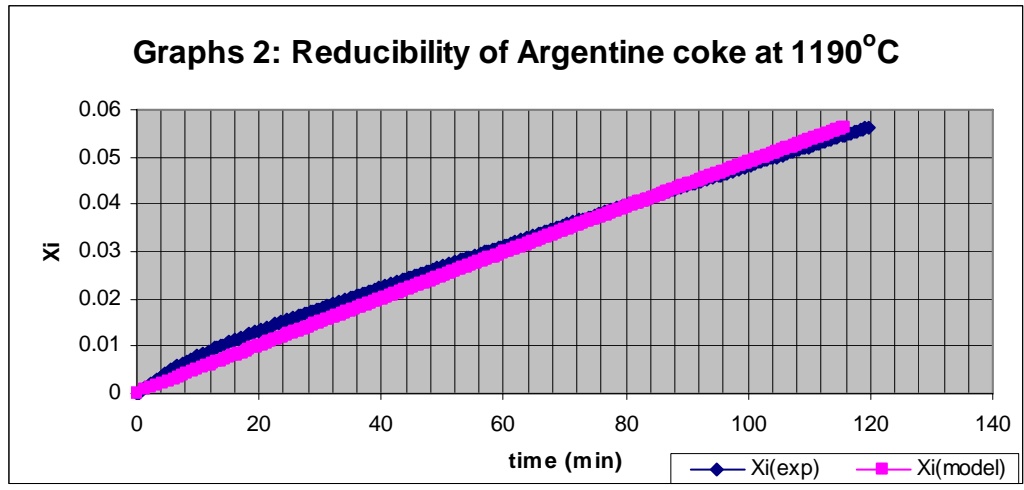
$$X_i \text{ (at } 1190^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.042953$$

The generated data in appendix 2 was fitted into equation [2] (as shown in graph 2) using the sum of least squares as follows:

$$S^2 = \sum_{i=1}^n (error)_i^2 = \sum_{i=1}^n [a_1 \mathcal{P}_1(X_i) + a_2 \mathcal{P}_2(X_i) - t_i]^2 \quad [15]$$

where  $a_1 = \tau$

and  $a_2 = \tau \sigma_s^2$



Graph 2 : Reduction of sintered chromite ore at 1190°C.

The fit yield:

$$\tau = 5945$$

$$\sigma_s^2 = 0.35122$$

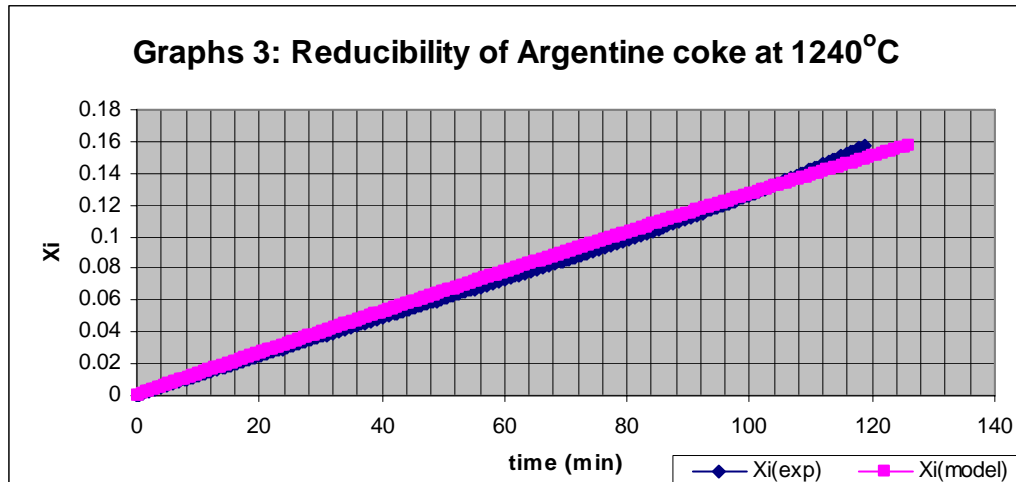
$$\text{and } S^2 = 3928.46$$

### 5.1.2 Determination of $\tau$ and $\sigma_s^2$ at 1240°C

$$X_{corr} \text{ at } 1240^\circ\text{C} = 0.060482$$

$$X_i \text{ (at } 1240^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.060482$$

The generated data in appendix 3 was fitted into equation [2] (as shown in graph 3) using the sum of least squares through equation [15].



Graph 3 : Reduction of sintered chromite ore at 1240°C.

The fit yields:

$$\tau = 2239.3$$

$$\sigma_s^2 = 0.090609$$

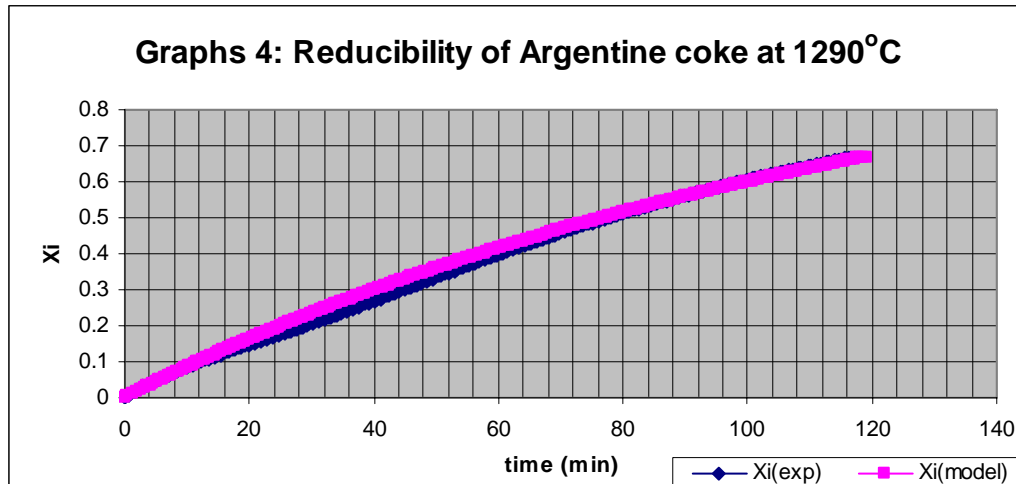
$$\text{and } S^2 = 1879.14$$

### 5.1.3 Determination of $\tau$ and $\sigma_s^2$ at 1290°C

$$X_{corr} \text{ at } 1290^\circ\text{C} = 0.088555$$

$$X_i \text{ (at } 1290^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.088555$$

The generated data in appendix 4 was fitted into equation [2] (as shown in graph 4) using the sum of least squares through equation [15].



Graph 4 : Reduction of sintered chromite ore at 1290°C.

The fit yields:

$$\tau = 337.4$$

$$\sigma_s^2 = 0.195554$$

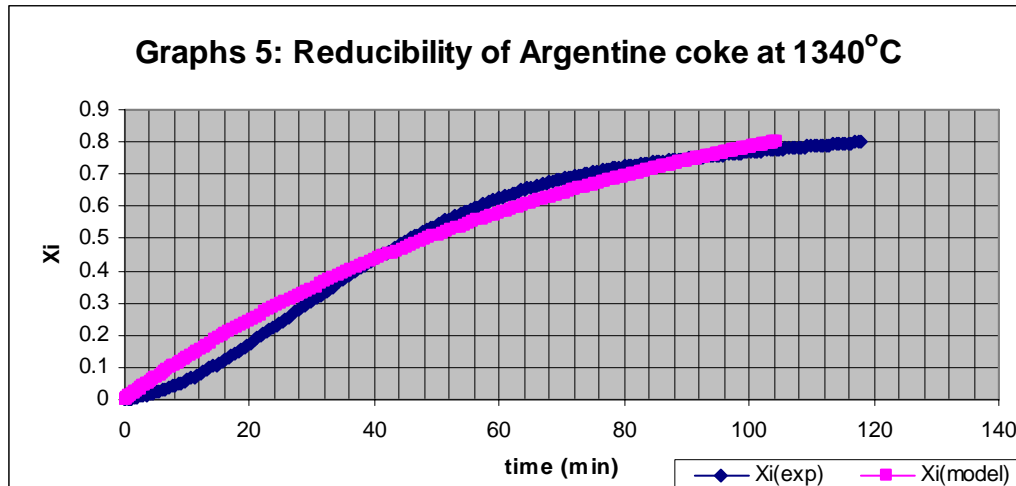
$$\text{and } S^2 = 1723.49$$

#### 5.1.4 Determination of $\tau$ and $\sigma_s^2$ at 1340°C

$$X_{corr} \text{ at } 1340^\circ\text{C} = 0.130083$$

$$X_i \text{ (at } 1340^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.130083$$

The generated data in appendix 5 was fitted into equation [2] (as shown in graph 5) using the sum of least squares through equation [15].



Graph 5 : Reduction of sintered chromite ore at 1340°C.

The fit yields:

$$\tau = 212.79$$

$$\sigma_s^2 = 0.202359$$

and  $S^2 = 8465.11$

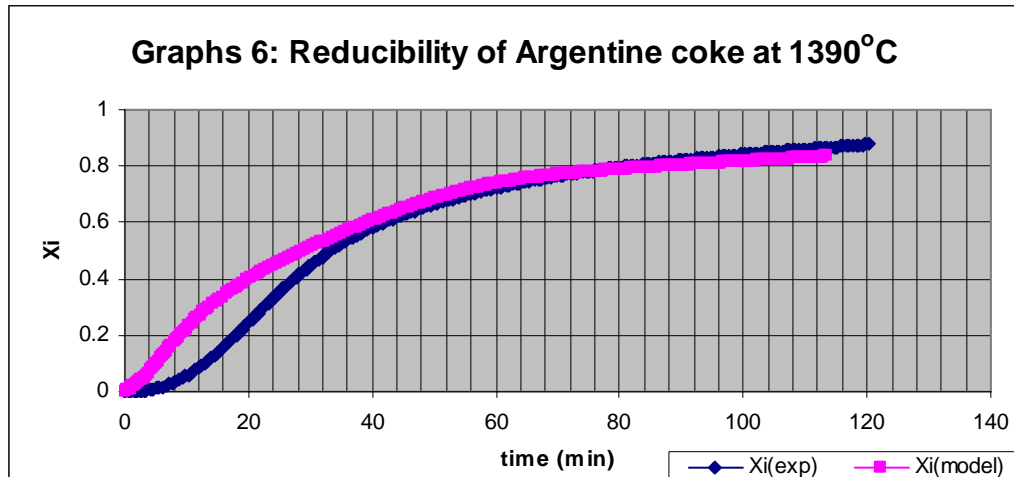
### 5.1.5 Determination of $\tau$ and $\sigma_s^2$ at 1390°C

$$X_{corr} \text{ at } 1390^\circ\text{C} = 0.187978$$

$$X_i \text{ (at } 1390^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.187978$$

The generated data in appendix 6 was fitted into equation [2] (as shown in graph 6) using the sum of least squares through equation [15].





Graph 6 : Reduction of sintered chromite ore at 1390°C.

The fit yields:

$$\tau = 188.12$$

$$\sigma_s^2 = 0.099405$$

$$\text{and } S^2 = 15528.8$$

### 5.1.6 Determination of $\Delta E$ (for chemical reaction) and $\Delta E$ (for diffusion) .

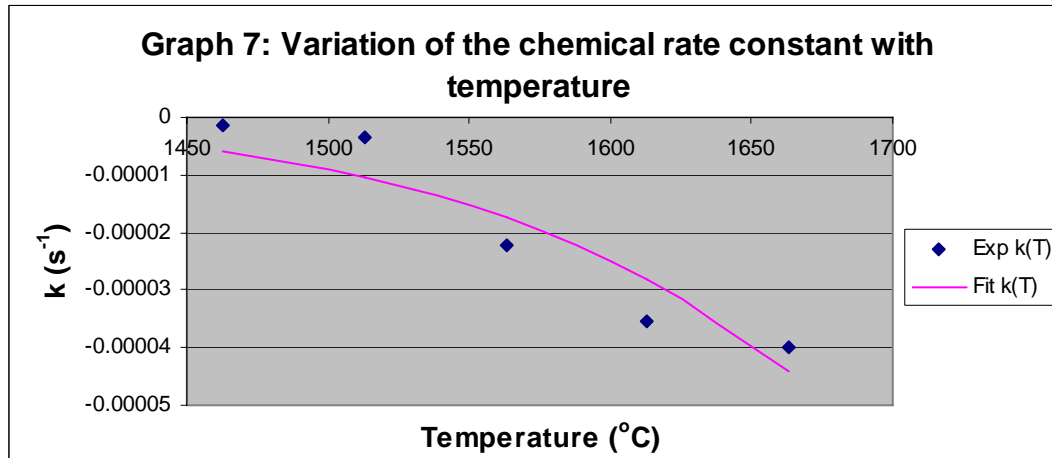
From equation [7] and equation [8], the values of the chemical reaction rate constant ( $k$ , in  $s^{-1}$ ), and the effective diffusion coefficient ( $D_e$ , in  $ms^{-1}$ ) are obtained at different temperatures and are as follows:

Table 5: Values of  $k$  and  $D_e$  at different temperatures

Temp (°C)	$\tau$ (min)	$\tau$ (s)	$\sigma_s^2$	$k$ (s <sup>-1</sup> )	$D_e$ (m.s <sup>-1</sup> )
1190	5945	356700	0.35122	$1.26308 \times 10^{-6}$	$1.88948 \times 10^{-11}$
1240	2239.3	134358	0.090609	$3.35329 \times 10^{-6}$	$1.94442 \times 10^{-10}$
1290	337.4	20244	0.195554	$2.22555 \times 10^{-5}$	$5.97945 \times 10^{-10}$
1340	212.79	12767.4	0.202359	$3.52884 \times 10^{-5}$	$9.16219 \times 10^{-10}$
1390	188.12	11287.2	0.099405	$3.99161 \times 10^{-5}$	$2.10974 \times 10^{-9}$

The values of  $k$  at different temperatures were fitted into Equation [1] (as shown in graph 7) using the sum of least squares as follows:

$$S^2 = \sum_{i=1}^n \left( k_o \exp \left[ \frac{-\Delta E}{R} \left\{ \frac{1}{T_i} - \frac{1}{T_o} \right\} \right] - k_i \right)^2 \quad [16]$$



Graph 7: Variation of the chemical reaction rate constant ( $k$ , in s<sup>-1</sup>) with temperature.

The fit yields:

$$\Delta E = 201813.4 \text{ J/mol (for chemical reaction)}$$

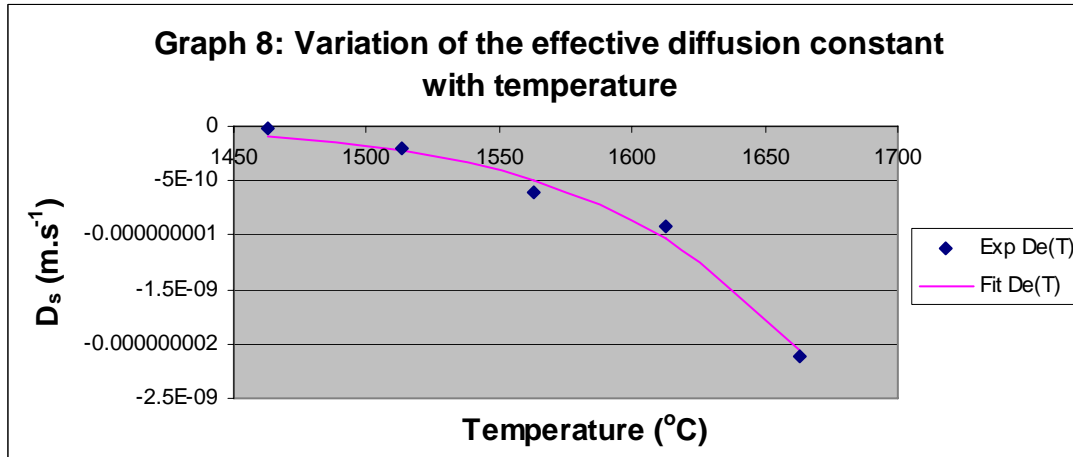
$$k_o = 6.0097 \times 10^{-6} \text{ s}^{-1}$$

$$T_o = 1463.132 \text{ °K}$$

$$\text{and } S^2 = 1.65825 \times 10^{-10}$$

The values of  $D_e$  at different temperatures were also fitted into Equation [1] (as shown in graph 8) using the sum of least squares as follows:

$$S^2 = \sum_{i=1}^n \left( D_o \exp \left[ \frac{-\Delta E}{R} \left\{ \frac{1}{T_i} - \frac{1}{T_o} \right\} \right] - D_{i_i} \right)^2 \quad [17]$$



Graph 8: Variation of the effective diffusion coefficient ( $D_e$ , in  $ms^{-1}$ ) with temperature.

The fit yields:

$$\Delta E = 306809.4 \text{ J/mol (for diffusion)}$$

$$D_e = 9.9634 \times 10^{-11} \text{ m.s}^{-1}$$

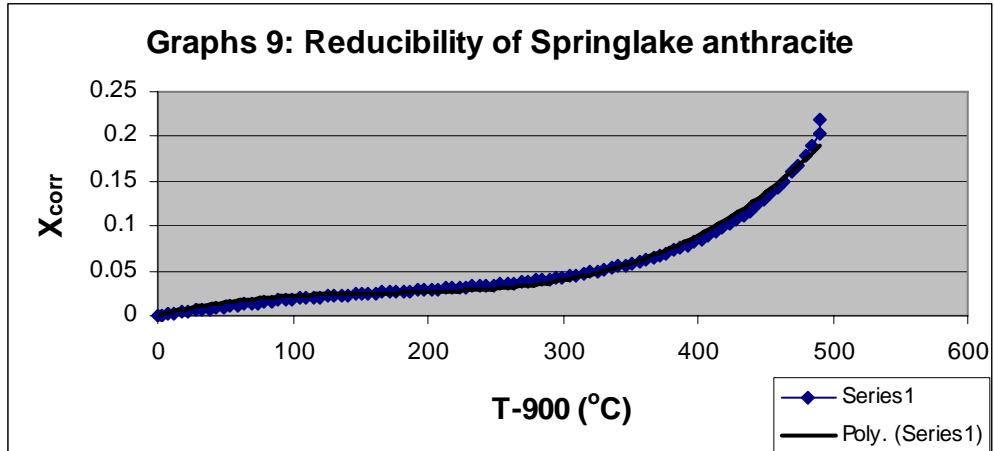
$$T_0 = 1463.132 \text{ } ^\circ\text{K}$$

$$\text{and } S^2 = 3.4227 \times 10^{-20}$$

## 5.2 Determination of the reactivity of Springlake anthracite.

200.1 mg of sintered chromite ore and 59.1mg of Springlake anthracite was used. The mixture contains 20% excess carbon required to react with  $Cr_2O_3$  and  $FeO$  and  $Fe_2O_3$  in the chromite ore . The reaction mixture was heated in an alumina sample holder from room temperature to the selected reaction temperature at a heating rate of  $10^\circ\text{C}$  per

minute, and then held for 120 minutes. The selected temperatures were 1190°C, 1240°C, 1290°C, 1340°C and 1390°C. Determination of the fraction reduction with temperature to account for the reduction occurred from 900°C to the selected temperature is as mentioned in section 5.1.



Graph 9: Reduction of sintered chromite ore using Springlake anthracite.

The fit yields:

$$X_{corr} = 0.00040649641(T - 900) - 2.2910705 \times 10^{-6}(T - 900)^2 + 4.587641 \times 10^{-9}(T - 900)^3$$

$$R^2 = 0.98866$$

Table 6: Values of  $X_{corr}$  at different temperatures.

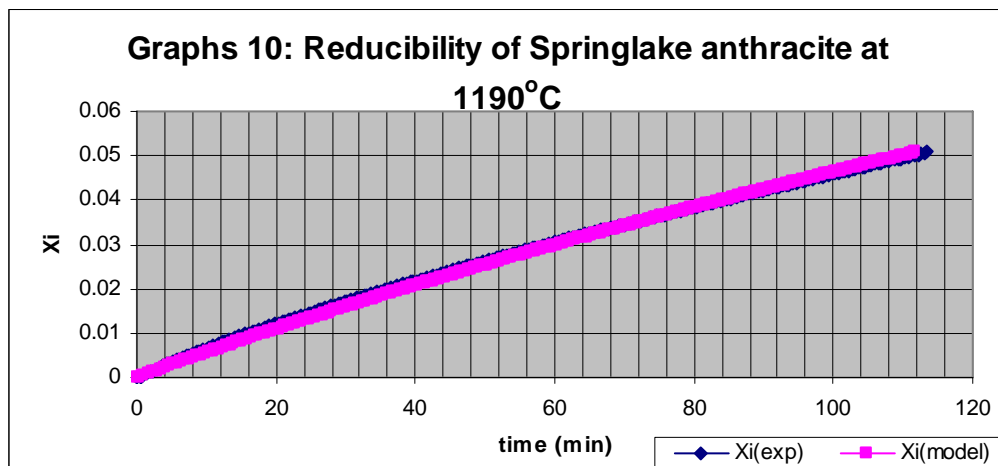
T (°C)	$X_{corr}$
1190	0.037093
1240	0.053674
1290	0.082196
1340	0.126101
1390	0.188829

### 5.2.1 Determination of $\tau$ and $\sigma_s^2$ at 1190°C

$$X_{corr} \text{ at } 1190^\circ\text{C} = 0.037093$$

$$X_i \text{ (at } 1190^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.037093$$

The generated data in appendix 8 was fitted into equation [2] (as shown in graph 10) using the sum of least squares shown in equation [15].



Graph 10 : Reduction of sintered chromite ore at 1190°C.

The fit yields:

$$\tau = 5238$$

$$\sigma_s^2 = 4.694922$$

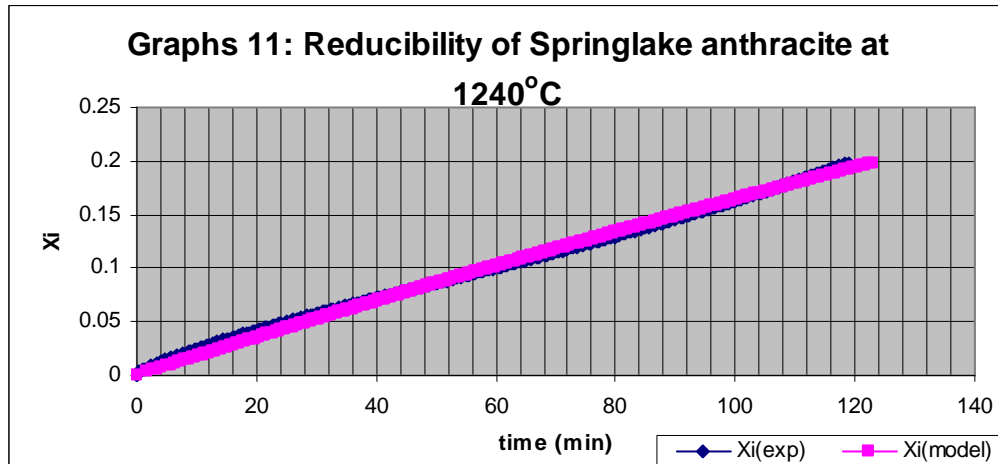
$$\text{and } S^2 = 642.108$$

### 5.2.2 Determination of $\tau$ and $\sigma_s^2$ at 1240°C

$$X_{corr} \text{ at } 1240^\circ\text{C} = 0.053674$$

$$X_i \text{ (at } 1240^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.053674$$

The generated data in appendix 9 was fitted into equation [2] (as shown in graph 11) through equation [15].



Graph 11 : Reduction of sintered chromite ore at 1240°C.

The fit yields:

$$\tau = 1672$$

$$\sigma_s^2 = 0.187081$$

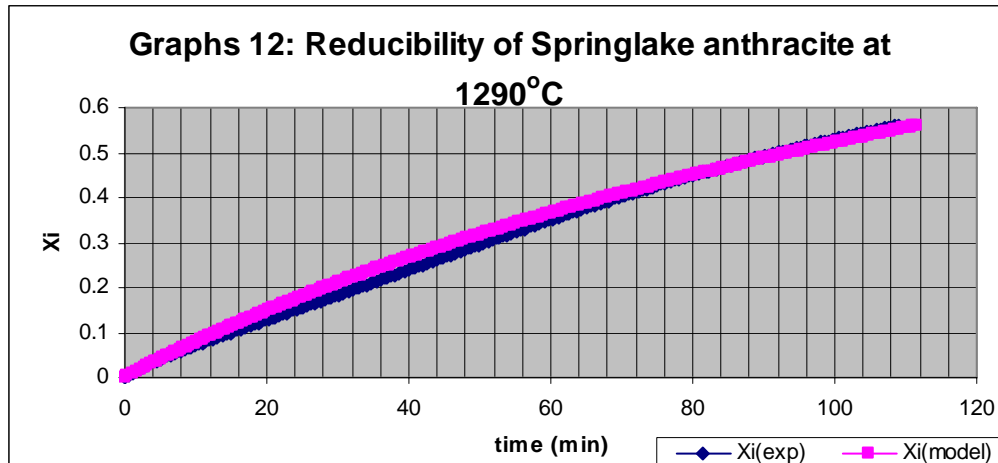
$$\text{and } S^2 = 1383.482$$

### 5.2.3 Determination of $\tau$ and $\sigma_s^2$ at 1290°C

$$X_{corr} \text{ at } 1290^\circ\text{C} = 0.082196$$

$$X_i \text{ (at } 1290^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.082196$$

The generated data in appendix 10 was fitted into equation [2] (as shown in graph 12) using the sum of least squares of equation [15].



Graph 12 : Reduction of sintered chromite ore at 1290°C.

The fit yields:

$$\tau = 357.7$$

$$\sigma_s^2 = 0.502656$$

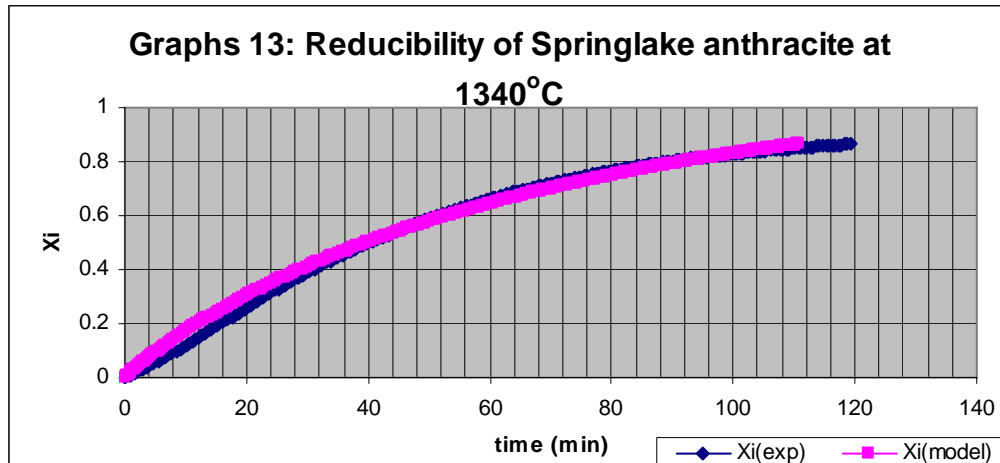
$$\text{and } S^2 = 1829.85970$$

#### 5.2.4 Determination of $\tau$ and $\sigma_s^2$ at 1340°C

$$X_{corr} \text{ at } 1340^\circ\text{C} = 0.126101$$

$$X_i \text{ (at } 1340^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.126101$$

The generated data in appendix 11 was fitted into equation [2] (as shown in graph 13) using the sum of least squares of equation [15].



Graph 13 : Reduction of sintered chromite ore at 1340°C.

The fit yields:

$$\tau = 152.5$$

$$\sigma_s^2 = 0.499672$$

$$\text{and } S^2 = 2305.0092$$

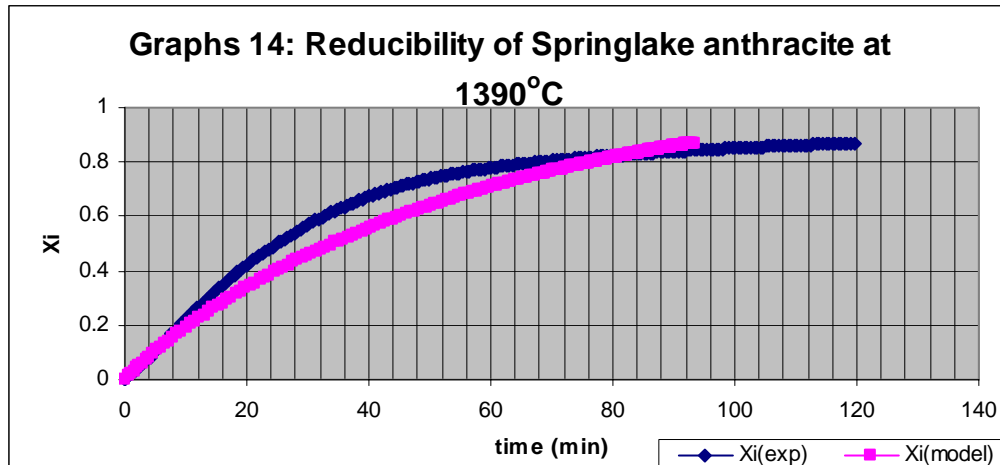
### 5.2.5 Determination of $\tau$ and $\sigma_s^2$ at 1390°C

$$X_{corr} \text{ at } 1390^\circ\text{C} = 0.188829$$

$$X_i \text{ (at } 1390^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.188829$$

The generated data in appendix 12 was fitted into equation [2] (as shown in graph 14) using the sum of least squares of equation [15].





Graph 14 : Reduction of sintered chromite ore at 1390°C.

The fit yields:

$$\tau = 137.00$$

$$\sigma_s^2 = 0.382482$$

$$\text{and } S^2 = 32288.81$$

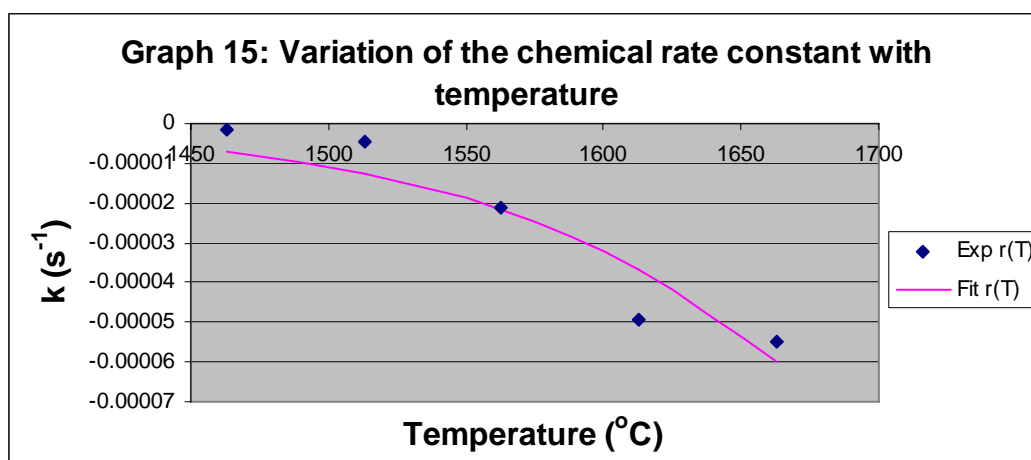
### 5.2.6 Determination of $\Delta E$ (for chemical reaction) and $\Delta E$ (for diffusion) .

From equation [7] and equation [8], the values of the chemical reaction rate constant ( $k$ , in  $s^{-1}$ ), and the effective diffusion coefficient ( $D_e$ , in  $ms^{-1}$ ) are obtained at different temperatures and are as follows:

Table 7: Values of  $k$  and  $D_e$  at different temperatures

Temp ( $^{\circ}\text{C}$ )	$\tau$ (min)	$\tau$ (s)	$\sigma_s^2$	$k$ ( $\text{s}^{-1}$ )	$D_e$ ( $\text{m}\cdot\text{s}^{-1}$ )
1190	5238	314280	4.694922	$1.43357 \times 10^{-6}$	$1.60428 \times 10^{-12}$
1240	1672	100320	0.187081	$4.49104 \times 10^{-6}$	$1.26127 \times 10^{-10}$
1290	357.7	21462	0.502656	$2.09925 \times 10^{-5}$	$2.19424 \times 10^{-10}$
1340	152.5	9150	0.499672	$4.92395 \times 10^{-5}$	$5.17748 \times 10^{-10}$
1390	137.00	8220	0.382482	$5.48103 \times 10^{-5}$	$7.52907 \times 10^{-9}$

The values of  $k$  at different temperatures were fitted into Equation [1] (as shown in graph 15) using the sum of least squares of equation [15]



Graph 15: Variation of the chemical reaction rate constant ( $k$ , in  $\text{s}^{-1}$ ) with temperature.

The fit yields:

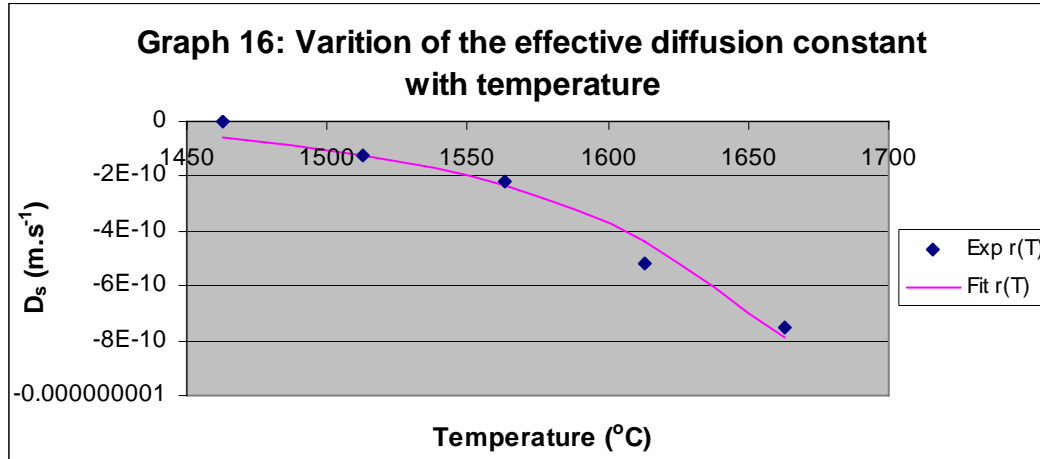
$$\Delta E = 217507.6 \text{ J/mol (for chemical reaction)}$$

$$k_o = 6.97581 \times 10^{-6} \text{ s}^{-1}$$

$$T_0 = 1463.132 \text{ }^{\circ}\text{K}$$

$$\text{and } S^2 = 2.78189 \times 10^{-10}$$

Similarly the values of  $D_e$  at different temperatures were also fitted into Equation [1] (as shown in graph 16) using the sum of least squares of equation [17].



Graph 16: Variation of the effective diffusion coefficient ( $D_e$ , in  $ms^{-1}$ ) with temperature.

The fit yields:

$$\Delta E = 260252.7 \text{ J/mol (for diffusion)}$$

$$D_e = 6.02099 \times 10^{-11} \text{ m.s}^{-1}$$

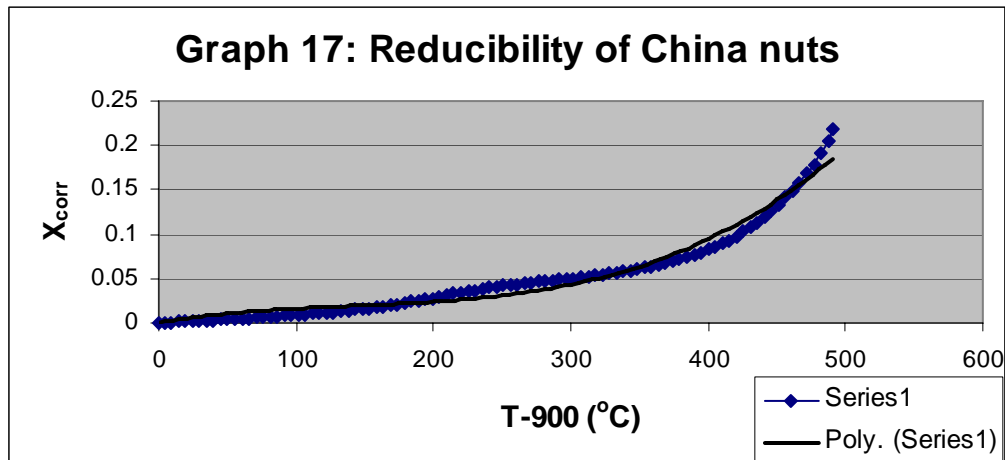
$$T_0 = 1463.132 \text{ } ^\circ\text{K}$$

$$\text{and } S^2 = 1.10551 \times 10^{-20}$$

### 5.3 Determination of the reactivity of China nuts coke.

200.3 mg of sintered chromite ore and 50.6mg of China nuts coke was used. The mixture contains 20% excess carbon required to react with  $Cr_2O_3$  and  $FeO$  and  $Fe_2O_3$  in the chromite ore. The reaction mixture was heated in an alumina sample holder from room temperature to the selected reaction temperature at a heating rate of  $10^\circ\text{C}$  per minute, and then held for 120 minutes. The selected temperatures were  $1190^\circ\text{C}$ ,  $1240^\circ\text{C}$ ,  $1290^\circ\text{C}$ ,  $1340^\circ\text{C}$  and  $1390^\circ\text{C}$ . Determination of the fraction reduction with temperature to account

for the reduction occurred from 900°C to the selected temperature is as mentioned in section 5.1.



Graph 17: Reduction of sintered chromite ore using China nuts coke.

The fit yields:

$$X_{corr} = 0.00027233225(T - 900) - 1.438868029 \times 10^{-6}(T - 900)^2 + 3.371531 \times 10^{-9}(T - 900)^3$$

$$R^2 = 0.971144$$

Table 8: Values of  $X_{corr}$  at different temperatures.

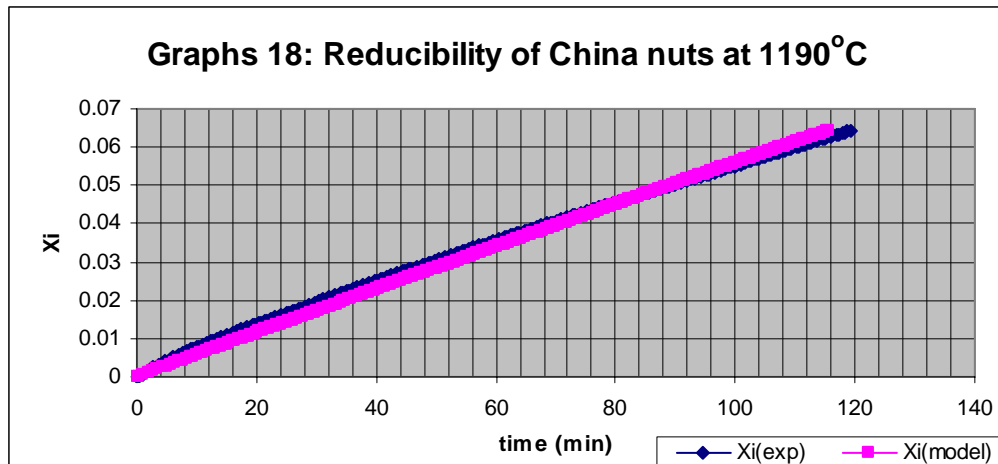
T (°C)	$X_{corr}$
1190	0.040196
1240	0.058774
1290	0.087354
1340	0.128462
1390	0.184628

### 5.3.1 Determination of $\tau$ and $\sigma_s^2$ at 1190°C

$$X_{corr} \text{ at } 1190^\circ\text{C} = 0.040196$$

$$X_i \text{ (at } 1190^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.040196$$

The generated data in appendix 14 was fitted into equation [2] (as shown in graph 18) through equation [15].



Graph 18 : Reduction of sintered chromite ore at 1190°C.

The fit yields:

$$\tau = 5205$$

$$\sigma_s^2 = 0.2244$$

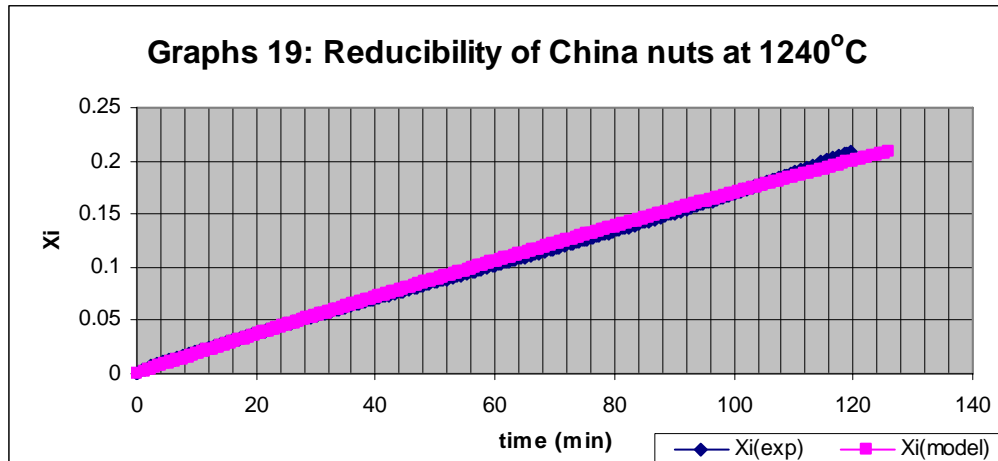
$$\text{and } S^2 = 2193.9534$$

### 5.3.2 Determination of $\tau$ and $\sigma_s^2$ at 1240°C

$$X_{corr} \text{ at } 1240^\circ\text{C} = 0.058774$$

$$X_i \text{ (at } 1240^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.058774$$

The generated data in appendix 15 was fitted into equation [2] (as shown in graph 19) using the sum of least squares of equation [15].



Graph 19 : Reduction of sintered chromite ore at 1240°C.

The fit yields:

$$\tau = 1616.5$$

$$\sigma_s^2 = 0.178781$$

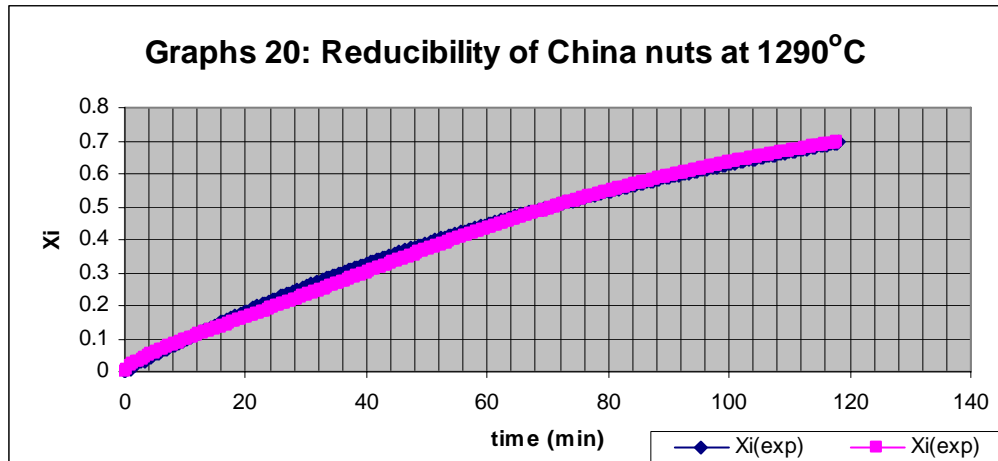
$$\text{and } S^2 = 935.089$$

### 5.3.3 Determination of $\tau$ and $\sigma_s^2$ at 1290°C

$$X_{corr} \text{ at } 1290^\circ\text{C} = 0.087354$$

$$X_i \text{ (at } 1290^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.087354$$

The generated data in appendix 16 was fitted into equation [2] (as shown in graph 20) using the sum of least squares of equation [15].



Graph 20 : Reduction of sintered chromite ore at 1290°C.

The fit yields:

$$\tau = 291.9$$

$$\sigma_s^2 = 0.316204$$

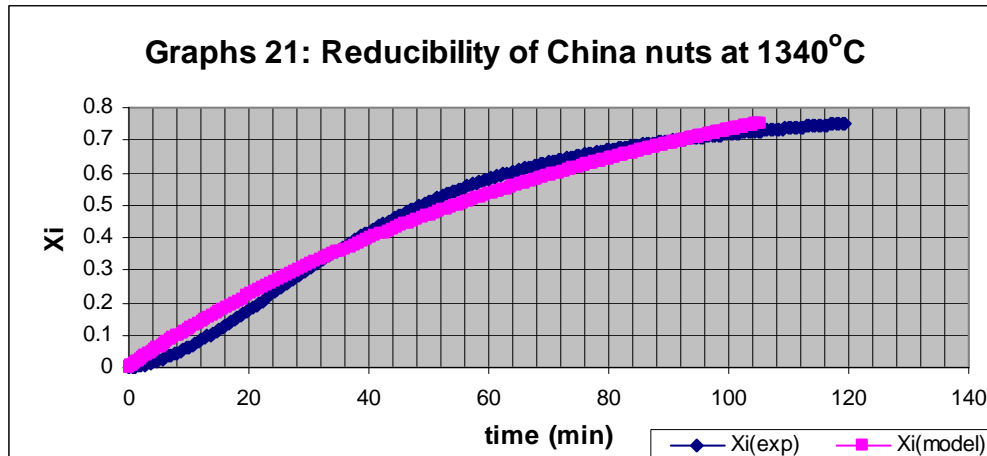
$$\text{and } S^2 = 1147.0396$$

#### 5.3.4 Determination of $\tau$ and $\sigma_s^2$ at 1340°C

$$X_{corr} \text{ at } 1340^\circ\text{C} = 0.128462$$

$$X_i \text{ (at } 1340^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.128462$$

The generated data in appendix 17 was fitted into equation [2] (as shown in graph 21) through equation [15].



Graph 21 : Reduction of sintered chromite ore at 1340°C.

The fit yields:

$$\tau = 234.7$$

$$\sigma_s^2 = 0.246698$$

$$\text{and } S^2 = 8360.67993$$

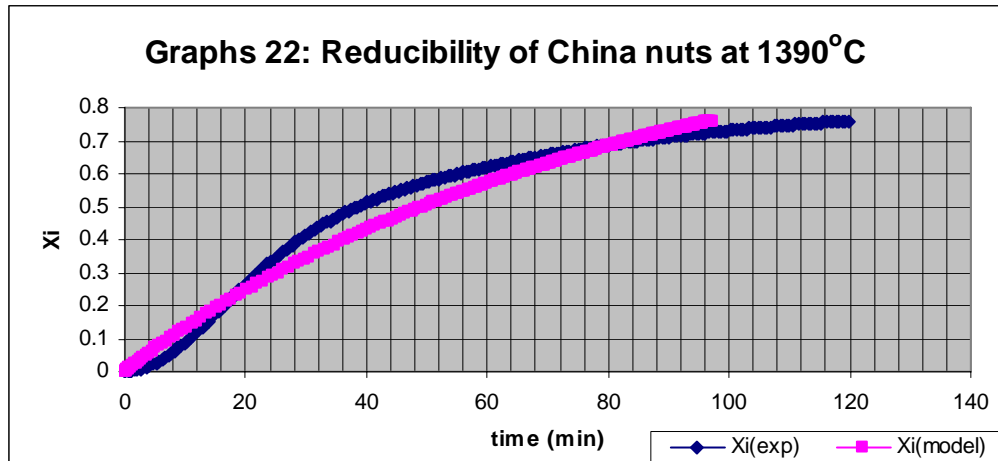
### 5.3.5 Determination of $\tau$ and $\sigma_s^2$ at 1390°C

$$X_{corr} \text{ at } 1390^\circ\text{C} = 0.184628$$

$$X_i \text{ (at } 1390^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.184628$$

The generated data in appendix 18 was fitted into equation [2] (as shown in graph 22) using the sum of least squares of equation [15].





Graph 22 : Reduction of sintered chromite ore at 1390°C.

The fit yields:

$$\tau = 210$$

$$\sigma_s^2 = 0.261905$$

$$\text{and } S^2 = 19569.2$$

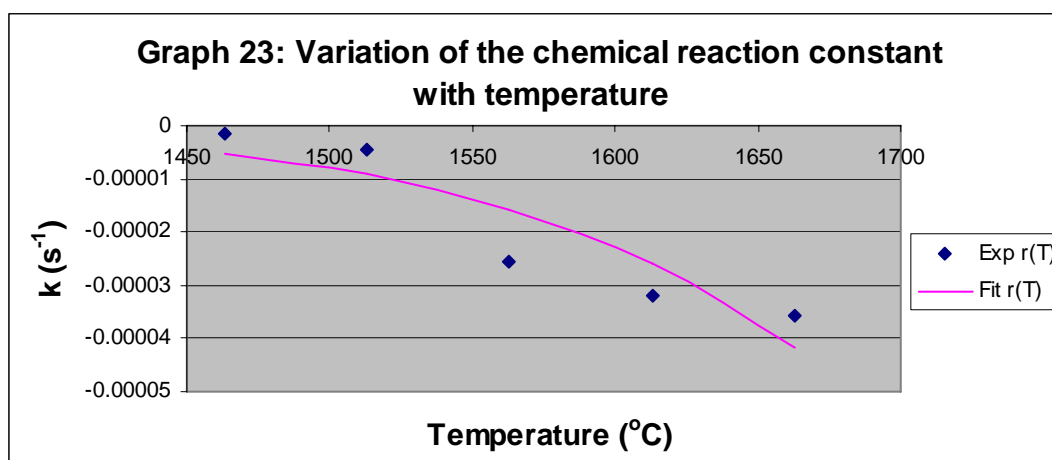
### 5.3.6 Determination of $\Delta E$ (for chemical reaction) and $\Delta E$ (for diffusion) .

From equation [7] and equation [8], the values of the chemical reaction rate constant ( $k$ , in  $s^{-1}$ ), and the effective diffusion coefficient ( $D_e$ , in  $ms^{-1}$ ) are obtained at different temperatures and are as follows:

Table 9: Values of  $k$  and  $D_e$  at different temperatures

Temp (°C)	$\tau$ (min)	$\tau$ (s)	$\sigma_s^2$	$k$ (s <sup>-1</sup> )	$D_e$ (m.s <sup>-1</sup> )
1190	5205	312300	0.2244	$1.44265 \times 10^{-6}$	$3.37777 \times 10^{-11}$
1240	1616.5	96990	0.178781	$4.64523 \times 10^{-6}$	$1.36514 \times 10^{-10}$
1290	291.9	17514	0.316204	$2.57246 \times 10^{-5}$	$4.27437 \times 10^{-10}$
1340	234.7	14082	0.246698	$3.19941 \times 10^{-5}$	$6.81388 \times 10^{-10}$
1390	210	12600	0.261905	$3.57572 \times 10^{-5}$	$7.17315 \times 10^{-10}$

The values of  $k$  at different temperatures were fitted into Equation [1] (as shown in graph 23) using the sum of least squares of equation [16].



Graph 23: Variation of the chemical reaction rate constant ( $k$ , in s<sup>-1</sup>) with temperature.

The fit yields:

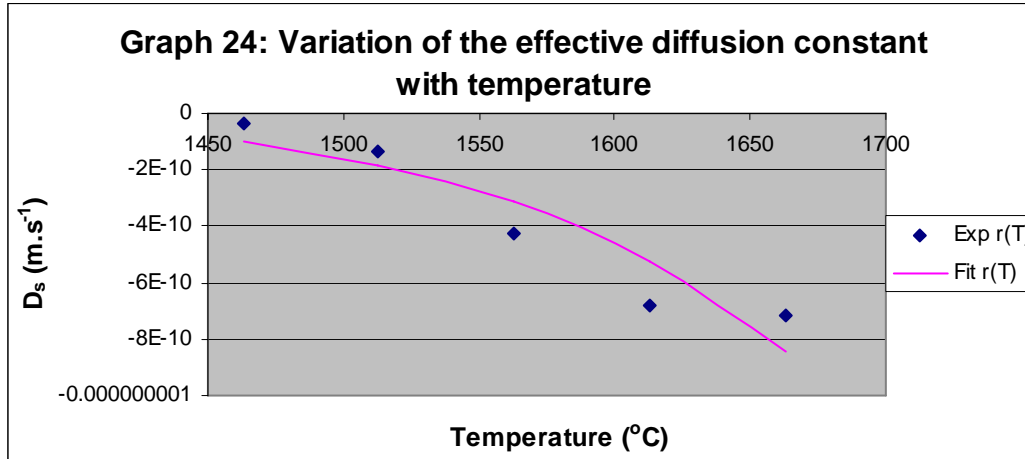
$$\Delta E = 212435.6 \text{ J/mol (for chemical reaction)}$$

$$k_o = 5.12863 \times 10^{-6} \text{ s}^{-1}$$

$$T_0 = 1463.132 \text{ } ^\circ\text{K}$$

$$\text{and } S^2 = 2.0804 \times 10^{-10}$$

The values of  $D_e$  at different temperatures were also fitted into Equation [1] (as shown in graph 24) using the sum of least squares of equation [17].



Graph 24: Variation of the effective diffusion coefficient ( $D_e$ , in  $ms^{-1}$ ) with temperature.

The fit yields:

$$\Delta E = 213134.3 \text{ J/mol (for diffusion)}$$

$$D_e = 1.02363 \times 10^{-10} \text{ m.s}^{-1}$$

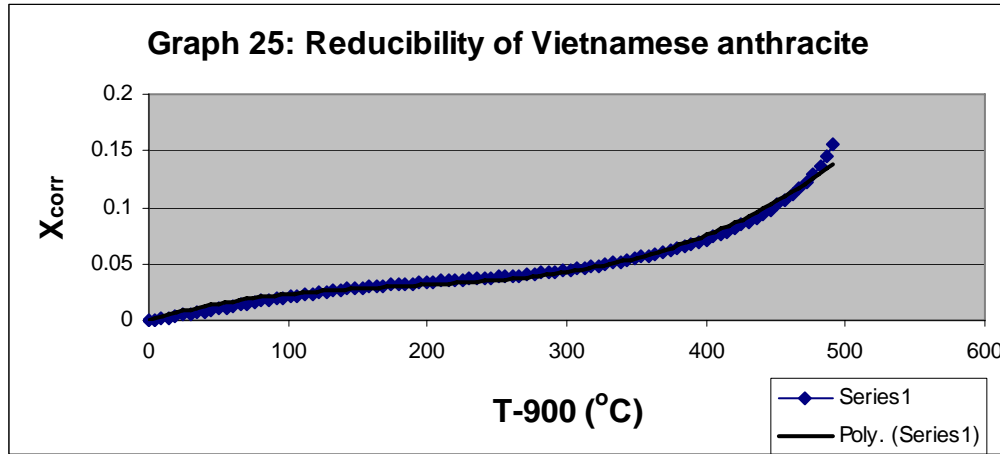
$$T_0 = 1463.132 \text{ } ^\circ\text{K}$$

$$\text{and } S^2 = 6.059277 \times 10^{-20}$$

#### 5.4 Determination of the reactivity of Vietnamese anthracite.

199.4 mg of sintered chromite ore and 47.7mg of Vietnamese anthracite was used. The mixture contains 20% excess carbon required to react with  $Cr_2O_3$  and FeO and  $Fe_2O_3$  in the chromite ore . The reaction mixture was heated in an alumina sample holder from room temperature to the selected reaction temperature at a heating rate of  $10^\circ\text{C}$  per minute, and then held for 120 minutes. The selected temperatures were  $1190^\circ\text{C}$ ,  $1240^\circ\text{C}$ ,  $1290^\circ\text{C}$ ,  $1340^\circ\text{C}$  and  $1390^\circ\text{C}$ .

Determination of the fraction reduction with temperature to account for the reduction occurred from 900°C to the selected temperature is as mentioned in section 5.1.



Graph 25: Reduction of sintered chromite ore using Vietnamese anthracite.

The fit yields:

$$X_{corr} = 0.00036830645389(T - 900) - 1.661003844 \times 10^{-6}(T - 900)^2 + 3.025550 \times 10^{-9}(T - 900)^3$$

$$R^2 = 0.98983565$$

and hence:

Table 10: Values of  $X_{corr}$  at different temperatures.

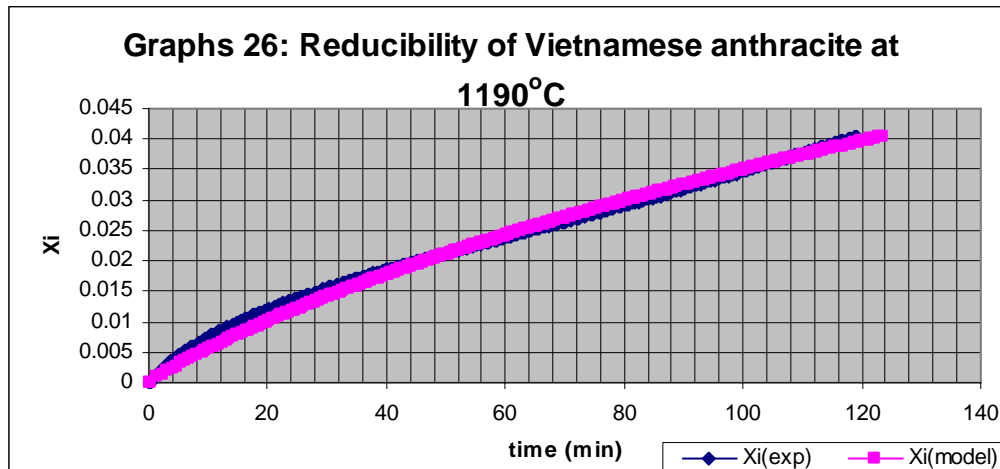
T (°C)	$X_{corr}$
1190	0.040909
1240	0.052128
1290	0.070473
1340	0.098213
1390	0.137616

#### 5.4.1 Determination of $\tau$ and $\sigma_s^2$ at 1190°C

$$X_{corr} \text{ at } 1190^\circ\text{C} = 0.040909$$

$$X_i \text{ (at } 1190^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.040909$$

The generated data in appendix 20 was fitted into equation [2] (as shown in graph 26) using the sum of least squares of equation [15]



Graph 26 : Reduction of sintered chromite ore at 1190°C.

The fit yields:

$$\tau = 4949$$

$$\sigma_s^2 = 20.36654$$

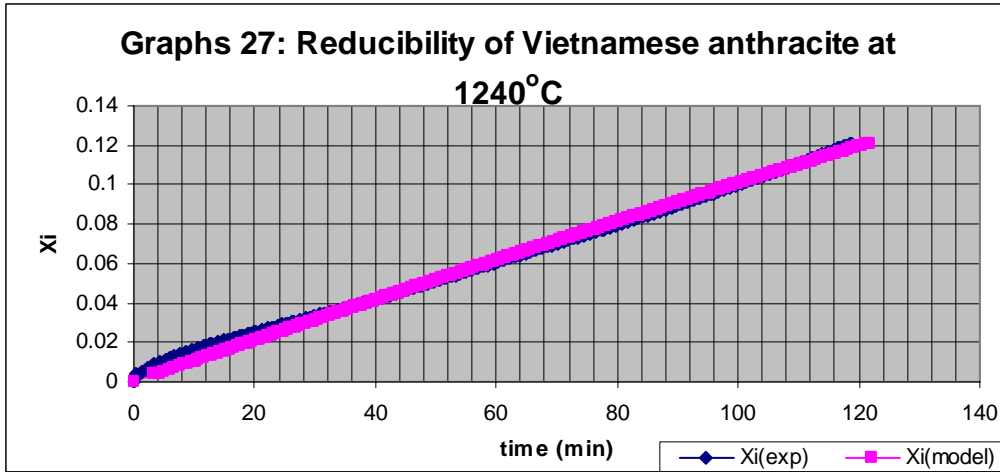
$$\text{and } S^2 = 1934.07057$$

#### 5.4.2 Determination of $\tau$ and $\sigma_s^2$ at 1240°C

$$X_{corr} \text{ at } 1240^\circ\text{C} = 0.052128$$

$$X_i \text{ (at } 1240^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.052128$$

The generated data in appendix 21 was fitted into equation [2] (as shown in graph 27) through equation [15].



Graph 27 : Reduction of sintered chromite ore at 1240°C.

The fit yields:

$$\tau = 2842$$

$$\sigma_s^2 = 0.142153$$

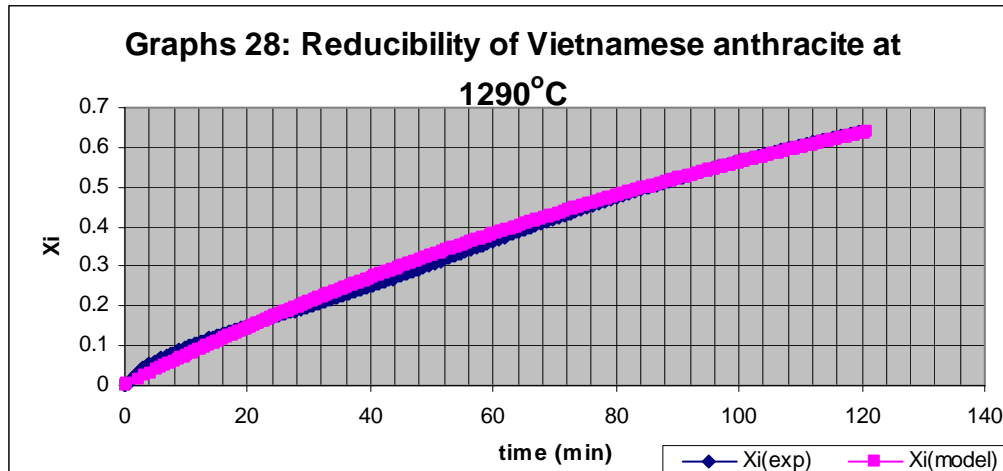
$$\text{and } S^2 = 1462.1046$$

#### 5.4.3 Determination of $\tau$ and $\sigma_s^2$ at 1290°C

$$X_{corr} \text{ at } 1290^\circ\text{C} = 0.070473$$

$$X_i \text{ (at } 1290^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.070473$$

The generated data in appendix 22 was fitted into equation [2] (as shown in graph 28) using the sum of least squares equation [15].



Graph 28 : Reduction of sintered chromite ore at 1290°C.

The fit yields:

$$\tau = 388.3$$

$$\sigma_s^2 = 0.120268$$

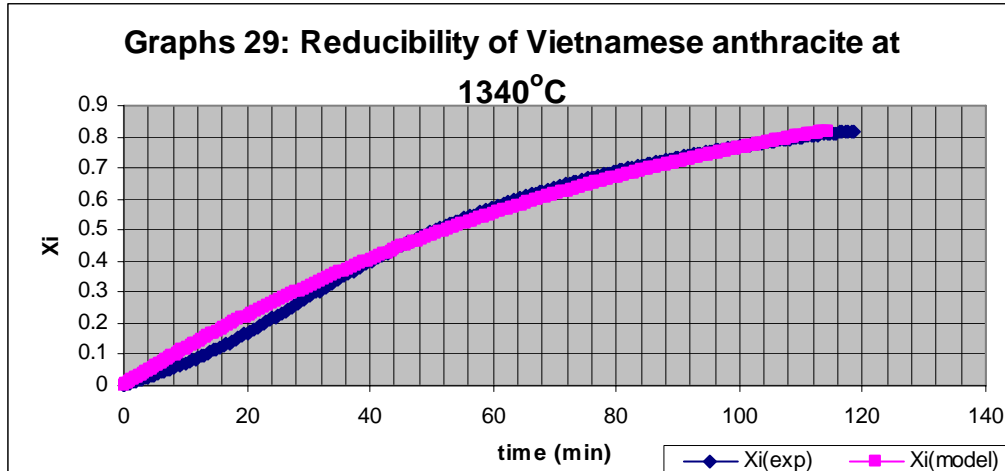
$$\text{and } S^2 = 1152.6086$$

#### 5.4.4 Determination of $\tau$ and $\sigma_s^2$ at 1340°C

$$X_{corr} \text{ at } 1340^\circ\text{C} = 0.098213$$

$$X_i \text{ (at } 1340^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.098213$$

The generated data in appendix 23 was fitted into equation [2] (as shown in graph 29) using the sum of least squares of equation [15].



Graph 29 : Reduction of sintered chromite ore at 1340°C.

The fit yields:

$$\tau = 241.1$$

$$\sigma_s^2 = 0.100$$

and  $S^2 = 2298.5379$

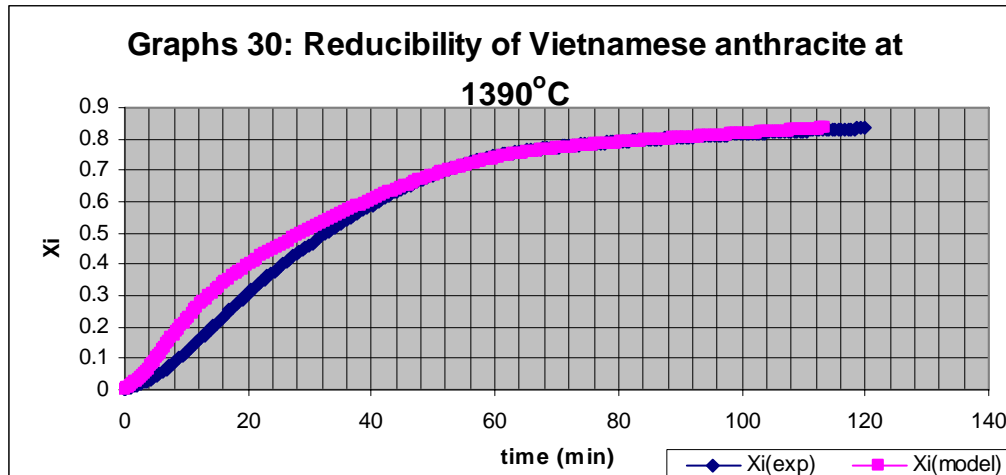
#### 5.4.5 Determination of $\tau$ and $\sigma_s^2$ at 1390°C

$$X_{corr} \text{ at } 1390^\circ\text{C} = 0.137616$$

$$X_i \text{ (at } 1390^\circ\text{C)} = X_i \text{ (from } 900^\circ\text{C)} - 0.137616$$

The generated data in appendix 24 was fitted into equation [2] (as shown in graph 30) using the sum of least squares of equation [15].





Graph 30 : Reduction of sintered chromite ore at 1390°C.

The fit yields:

$$\tau = 187.9$$

$$\sigma_s^2 = 0.10644$$

$$\text{and } S^2 = 30562.24$$

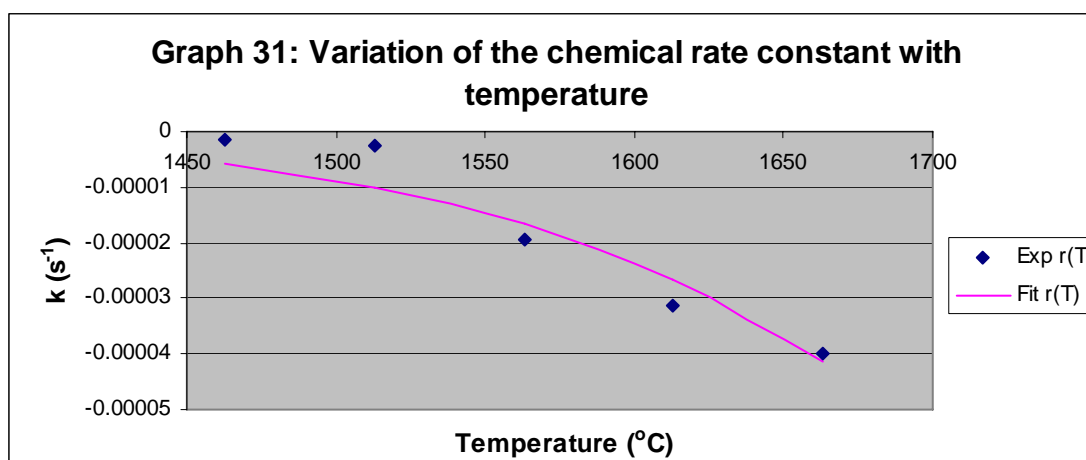
#### 5.4.6 Determination of $\Delta E$ (for chemical reaction) and $\Delta E$ (for diffusion) .

From equation [7] and equation [8], the values of the chemical reaction rate constant ( $k$ , in  $s^{-1}$ ), and the effective diffusion coefficient ( $D_e$ , in  $ms^{-1}$ ) are obtained at different temperatures and are as follows:

Table 11: Values of  $k$  and  $D_e$  at different temperatures

Temp ( $^{\circ}\text{C}$ )	$\tau$ (min)	$\tau$ (s)	$\sigma_s^2$	$k$ ( $\text{s}^{-1}$ )	$D_e$ ( $\text{m}\cdot\text{s}^{-1}$ )
1190	4949	296940	20.36654	$1.51728 \times 10^{-6}$	$3.91416 \times 10^{-13}$
1240	2842	170520	0.142153	$2.64216 \times 10^{-6}$	$9.76547 \times 10^{-11}$
1290	388.3	23298	0.120268	$1.93382 \times 10^{-5}$	$8.44803 \times 10^{-10}$
1340	241.1	14466	0.100	$3.11448 \times 10^{-5}$	$1.63635 \times 10^{-9}$
1390	187.9	11274	0.10644	$3.99628 \times 10^{-5}$	$1.97261 \times 10^{-9}$

The values of  $k$  at different temperatures were fitted into Equation [1] (as shown in graph 31) using the sum of least squares of equation [16]



Graph 31: Variation of the chemical reaction rate constant ( $k$ , in  $\text{s}^{-1}$ ) with temperature.

The fit yields:

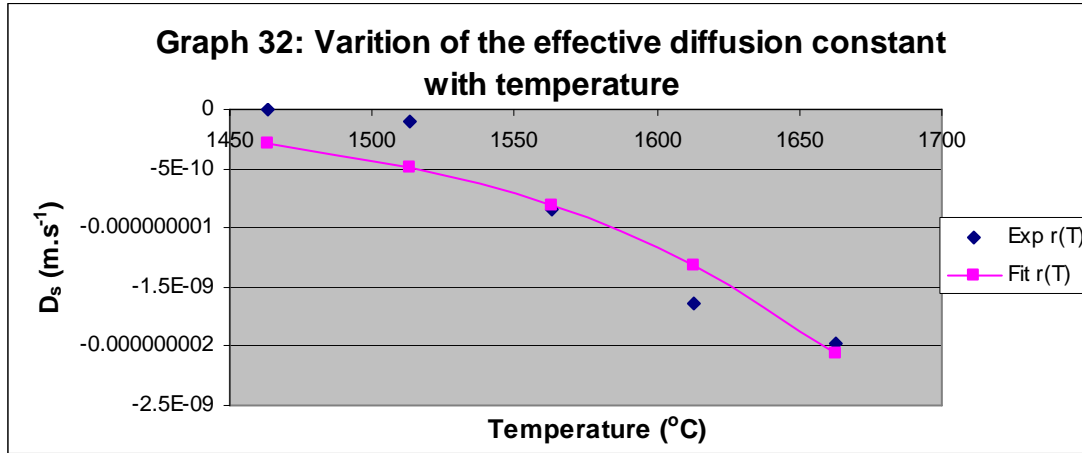
$$\Delta E = 197024.2 \text{ J/mol (for chemical reaction)}$$

$$k_o = 5.92088 \times 10^{-6} \text{ s}^{-1}$$

$$T_0 = 1463.132 \text{ }^{\circ}\text{K}$$

$$\text{and } S^2 = 1.04396 \times 10^{-10}$$

The values of  $D_e$  at different temperatures were also fitted into Equation [1] (as shown in graph 32) through equation [17].



Graph 32: Variation of the effective diffusion coefficient ( $D_e$ , in  $ms^{-1}$ ) with temperature.

The fit yields:

$$\Delta E = 200057 \text{ J/mol (for diffusion)}$$

$$D_e = 2.84626 \times 10^{-10} \text{ m.s}^{-1}$$

$$T_0 = 1463.132 \text{ } ^\circ\text{K}$$

$$\text{and } S^2 = 3.469368 \times 10^{-19}$$

## CHAPTER 6: DISCUSSION OF RESULTS

The values of the activation energies obtained from fitting the data into the Arrhenius equation was then used to determine the relative reactivity of the reductants. The values of the chemical reaction rate constant and effective diffusion constant were used to determine the relative speed at which the reductants can reduce the chromite ore. The summary of the results of the TGA tests are as follows:

Table 12: Summary of the TGA test results.

Reductant	Chemical reaction		Effective diffusion	
	$\Delta E$	$k_o$	$\Delta E$	$D_e$
Vietnamese anthracite	197 024.2	$5.9209 \times 10^{-6}$	200 057	$2.8463 \times 10^{-10}$
China nuts coke	212 435.6	$5.1286 \times 10^{-6}$	213 134.3	$1.0236 \times 10^{-10}$
Springlake anthracite	217 507.6	$6.9758 \times 10^{-6}$	260 252.7	$6.0210 \times 10^{-11}$
Argentine coke	201 813.4	$6.0097 \times 10^{-6}$	306 809.4	$9.9634 \times 10^{-11}$

The TGA tests suggest that the Vietnamese anthracite has the highest reactivity since its activation energies are the lowest and requires less energy to induce the reductant reaction. The reduction of  $\text{FeCr}_2\text{O}_4$  by activated carbon in argon atmosphere was studied by C.P.J. Van Vuuren<sup>17</sup>. The activation energy of the reaction was found to be 197 kJ/mol, which is in good agreement to the activation energy values obtained in the TGA tests.

The tests also suggest that the rate controlling mechanism is the diffusion of species to the reactive site since the effective diffusion constant is of the order  $10^{-10}$  to  $10^{-11}$ , which is far less than the chemical rate constant of the order  $10^{-6}$ . A generalized rate model developed to describe the reduction of chromite shows that at given particle size and up

to a reduction of 40%, the rate of reduction is controlled mainly by interfacial-area chemical reaction, and after which the rate is dominated by diffusion<sup>7</sup>.

The tests also suggest that the Vietnamese anthracite is the fastest to react since its effective diffusion constant is high, and Argentine coke being the less reactive and slowest to react (highest activation energy and lowest effective diffusion constant).

## CHAPTER 7: CONCLUSION

The TGA tests suggested that the Vietnamese anthracite has the highest relative reactivity followed by China nuts coke only. Since the rate controlling mechanism is diffusion of species to the reactive site, then Vietnamese anthracite is the fastest to react followed by China nuts, and Argentine coke being the slowest to react.

Tests were also conducted in the smelter furnace to determine if the performance of the reductant is with accordance to the TGA tests analysis. In performing these tests, 10 to 30% (in terms of fixed carbon) of China nuts being used in the furnace was substituted with the reductant under study. Another test was carried out whereby the China nuts coke was completely substituted with Argentine coke. The sizing of the material was kept at -40+10mm.

Due to management of the company considering these tests as their competitive advantage, the tests were considered highly confidential. The publishing of the data of the smelter furnace operation during these tests was not approved. Overall the results of the tests done in the smelter furnace were in good agreement to those obtained in the TGA tests.

Hence the TGA test can be used to determine the reactivity of the reductant to a higher degree of confidence. The values of the chemical rate constant and effective diffusion constant obtained in the TGA tests can be used in deciding on the material size to be used, especially when one wants to maintain a stable coke bed underneath the electrodes. Follow-up tests involving the resistivity of the reductant will have to be done to establish the total performance of the reductant and its usability.

Overall, the investigation showed that anthracite has a significant potential to substitute coke as a reductant of choice. This is also supported by the fact that anthracite is used as one of the raw material in the production of a submerged arc furnace electrode paste.

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APPENDIX 1: Data for the reactivity of Argentine coke.

##Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./(t V/mW)	Segment	Mass change (mg)	Mass loss (mg)	CO evolved (mg)	X <sub>i</sub>	T-900 (°C)	X <sub>i</sub>
888.440	86.867	99.446	0.180	0.258	1.000	256.868	1.432				
893.568	87.381	99.434	0.183	0.257	1.000	256.838	1.462				
898.725	87.895	99.422	0.186	0.256	1.000	256.806	1.494	0.000	0.000	0.000	0.000
903.876	88.409	99.409	0.189	0.255	1.000	256.774	1.526	0.032	0.000	3.876	0.0004
909.023	88.923	99.395	0.192	0.254	1.000	256.736	1.564	0.070	0.001	9.023	0.0009
914.170	89.437	99.381	0.194	0.253	1.000	256.700	1.600	0.106	0.001	14.170	0.0014
919.305	89.951	99.367	0.198	0.252	1.000	256.666	1.634	0.140	0.002	19.305	0.0018
924.444	90.465	99.353	0.202	0.251	1.000	256.628	1.672	0.179	0.002	24.444	0.0023
929.595	90.979	99.337	0.203	0.249	1.000	256.588	1.712	0.218	0.003	29.595	0.0029
934.737	91.493	99.323	0.206	0.248	1.000	256.552	1.748	0.254	0.003	34.737	0.0033
939.886	92.007	99.309	0.208	0.247	1.000	256.514	1.786	0.292	0.004	39.886	0.0038
945.019	92.521	99.291	0.211	0.246	1.000	256.468	1.832	0.338	0.004	45.019	0.0044
950.153	93.035	99.274	0.213	0.245	1.000	256.425	1.875	0.381	0.005	50.153	0.0050
955.296	93.549	99.257	0.215	0.244	1.000	256.380	1.920	0.426	0.006	55.296	0.0056
960.431	94.063	99.237	0.218	0.242	1.000	256.330	1.970	0.476	0.006	60.431	0.0062
965.582	94.577	99.216	0.220	0.241	1.000	256.276	2.024	0.530	0.007	65.582	0.0069
970.709	95.091	99.196	0.222	0.240	1.000	256.224	2.076	0.583	0.008	70.709	0.0076
975.866	95.605	99.174	0.224	0.239	1.000	256.168	2.132	0.639	0.008	75.866	0.0084
981.013	96.119	99.153	0.226	0.238	1.000	256.112	2.188	0.694	0.009	81.013	0.0091
986.151	96.633	99.129	0.228	0.236	1.000	256.051	2.249	0.756	0.010	86.151	0.0099
991.300	97.147	99.106	0.230	0.235	1.000	255.990	2.310	0.816	0.011	91.300	0.0107
996.443	97.661	99.079	0.232	0.234	1.000	255.922	2.378	0.884	0.012	96.443	0.0116
1001.590	98.175	99.053	0.234	0.232	1.000	255.855	2.445	0.952	0.012	101.590	0.0124
1006.740	98.689	99.029	0.237	0.231	1.000	255.792	2.508	1.014	0.013	106.740	0.0133
1011.885	99.203	98.999	0.239	0.230	1.000	255.714	2.586	1.092	0.014	111.885	0.0143
1017.045	99.717	98.968	0.241	0.229	1.000	255.635	2.665	1.172	0.015	117.045	0.0153
1022.195	100.231	98.936	0.244	0.227	1.000	255.552	2.748	1.254	0.016	122.195	0.0164
1027.328	100.745	98.903	0.246	0.226	1.000	255.467	2.833	1.339	0.018	127.328	0.0175
1032.500	101.259	98.870	0.248	0.224	1.000	255.382	2.918	1.424	0.019	132.500	0.0186
1037.627	101.773	98.833	0.250	0.223	1.000	255.286	3.014	1.520	0.020	137.627	0.0199
1042.778	102.287	98.798	0.250	0.222	1.000	255.194	3.106	1.612	0.021	142.778	0.0211
1047.908	102.801	98.758	0.253	0.220	1.000	255.092	3.208	1.715	0.022	147.908	0.022
1053.068	103.315	98.717	0.253	0.219	1.000	254.987	3.313	1.819	0.024	153.068	0.024
1058.198	103.829	98.678	0.256	0.217	1.000	254.886	3.414	1.920	0.025	158.198	0.025
1063.335	104.343	98.638	0.258	0.216	1.000	254.781	3.519	2.025	0.026	163.335	0.026
1068.483	104.857	98.598	0.259	0.215	1.000	254.678	3.622	2.128	0.028	168.483	0.028
1073.606	105.371	98.554	0.259	0.213	1.000	254.564	3.736	2.243	0.029	173.606	0.029
1078.769	105.885	98.514	0.259	0.212	1.000	254.463	3.837	2.344	0.031	178.769	0.031
1083.908	106.399	98.474	0.260	0.210	1.000	254.358	3.942	2.448	0.032	183.908	0.032
1089.056	106.913	98.436	0.261	0.209	1.000	254.260	4.040	2.547	0.033	189.056	0.033
1094.176	107.427	98.399	0.262	0.207	1.000	254.165	4.135	2.641	0.035	194.176	0.035
1099.319	107.941	98.365	0.262	0.206	1.000	254.076	4.224	2.731	0.036	199.319	0.036
1104.462	108.455	98.331	0.263	0.204	1.000	253.990	4.310	2.816	0.037	204.462	0.037
1109.615	108.969	98.299	0.264	0.203	1.000	253.906	4.394	2.900	0.038	209.615	0.038

1114.760	109.483	98.270	0.265	0.201	1.000	253.831	4.469	2.976	0.039	214.760	0.039
1119.894	109.997	98.243	0.265	0.200	1.000	253.762	4.538	3.044	0.040	219.894	0.040
1125.043	110.511	98.218	0.265	0.198	1.000	253.698	4.602	3.108	0.041	225.043	0.041
1130.182	111.025	98.193	0.265	0.197	1.000	253.632	4.668	3.175	0.042	230.182	0.042
1135.327	111.539	98.170	0.265	0.195	1.000	253.574	4.726	3.232	0.042	235.327	0.042
1140.471	112.053	98.147	0.266	0.194	1.000	253.514	4.786	3.292	0.043	240.471	0.043
1145.621	112.567	98.126	0.267	0.192	1.000	253.460	4.840	3.347	0.044	245.621	0.044
1150.756	113.081	98.108	0.268	0.190	1.000	253.412	4.888	3.395	0.044	250.756	0.044
1155.896	113.595	98.087	0.268	0.189	1.000	253.358	4.942	3.449	0.045	255.896	0.045
1161.040	114.109	98.065	0.270	0.187	1.000	253.302	4.998	3.504	0.046	261.040	0.046
1166.179	114.623	98.045	0.272	0.186	1.000	253.251	5.049	3.555	0.046	266.179	0.046
1171.320	115.137	98.026	0.273	0.184	1.000	253.202	5.098	3.604	0.047	271.320	0.047
1176.471	115.652	98.004	0.274	0.183	1.000	253.144	5.156	3.662	0.048	276.471	0.048
1181.599	116.166	97.981	0.276	0.181	1.000	253.084	5.216	3.723	0.049	281.599	0.049
1186.748	116.680	97.961	0.277	0.179	1.000	253.034	5.266	3.772	0.049	286.748	0.049
1191.892	117.194	97.936	0.277	0.178	1.000	252.968	5.332	3.838	0.050	291.892	0.050
1197.029	117.708	97.910	0.279	0.176	1.000	252.902	5.398	3.904	0.051	297.029	0.051
1202.172	118.222	97.885	0.282	0.175	1.000	252.836	5.464	3.970	0.052	302.172	0.052
1207.305	118.736	97.858	0.285	0.173	1.000	252.766	5.534	4.040	0.053	307.305	0.053
1212.453	119.250	97.829	0.287	0.171	1.000	252.692	5.608	4.114	0.054	312.453	0.054
1217.596	119.764	97.795	0.290	0.170	1.000	252.606	5.694	4.201	0.055	317.596	0.055
1222.740	120.278	97.763	0.293	0.168	1.000	252.522	5.778	4.285	0.056	322.740	0.056
1227.886	120.792	97.730	0.294	0.166	1.000	252.436	5.864	4.371	0.057	327.886	0.057
1233.022	121.306	97.695	0.297	0.165	1.000	252.346	5.954	4.461	0.058	333.022	0.058
1238.165	121.820	97.657	0.299	0.163	1.000	252.248	6.052	4.558	0.060	338.165	0.060
1243.301	122.334	97.619	0.302	0.162	1.000	252.151	6.149	4.656	0.061	343.301	0.061
1248.453	122.848	97.577	0.305	0.160	1.000	252.040	6.260	4.766	0.062	348.453	0.062
1253.601	123.362	97.530	0.307	0.158	1.000	251.919	6.381	4.887	0.064	353.601	0.064
1258.736	123.876	97.486	0.311	0.157	1.000	251.806	6.494	5.001	0.065	358.736	0.065
1263.889	124.390	97.436	0.314	0.155	1.000	251.676	6.624	5.130	0.067	363.889	0.067
1269.009	124.904	97.383	0.317	0.153	1.000	251.540	6.760	5.266	0.069	369.009	0.069
1274.164	125.418	97.322	0.320	0.152	1.000	251.382	6.918	5.424	0.071	374.164	0.071
1279.300	125.932	97.264	0.321	0.150	1.000	251.234	7.066	5.573	0.073	379.300	0.073
1284.441	126.446	97.195	0.324	0.149	1.000	251.054	7.246	5.752	0.075	384.441	0.075
1289.583	126.960	97.120	0.327	0.147	1.000	250.862	7.438	5.944	0.078	389.583	0.078
1294.721	127.474	97.043	0.334	0.145	1.000	250.661	7.639	6.145	0.080	394.721	0.080
1299.870	127.988	96.957	0.342	0.144	1.000	250.440	7.860	6.367	0.083	399.870	0.083
1305.008	128.502	96.864	0.355	0.142	1.000	250.199	8.101	6.607	0.086	405.008	0.086
1310.140	129.016	96.757	0.371	0.140	1.000	249.922	8.378	6.884	0.090	410.140	0.090
1315.287	129.530	96.640	0.388	0.139	1.000	249.622	8.678	7.184	0.094	415.287	0.094
1320.431	130.044	96.512	0.409	0.137	1.000	249.290	9.010	7.517	0.098	420.431	0.098
1325.559	130.558	96.368	0.426	0.136	1.000	248.917	9.383	7.889	0.103	425.559	0.103
1330.689	131.072	96.211	0.447	0.134	1.000	248.512	9.788	8.294	0.108	430.689	0.108
1335.841	131.586	96.043	0.472	0.132	1.000	248.080	10.220	8.727	0.114	435.841	0.114
1340.994	132.100	95.858	0.498	0.131	1.000	247.600	10.700	9.206	0.120	440.994	0.120
1346.120	132.614	95.658	0.528	0.129	1.000	247.084	11.216	9.723	0.127	446.120	0.127
1351.268	133.128	95.434	0.561	0.128	1.000	246.507	11.793	10.300	0.135	451.268	0.135
1356.412	133.642	95.195	0.599	0.126	1.000	245.888	12.412	10.918	0.143	456.412	0.143

1361.551	134.156	94.935	0.640	0.125	1.000	245.217	13.083	11.589	0.152	461.551	0.152
1366.701	134.670	94.654	0.686	0.123	1.000	244.492	13.808	12.314	0.161	466.701	0.161
1371.828	135.184	94.349	0.738	0.121	1.000	243.704	14.596	13.102	0.171	471.828	0.171
1376.983	135.698	94.021	0.796	0.120	1.000	242.857	15.443	13.949	0.182	476.983	0.182
1382.117	136.212	93.665	0.867	0.118	1.000	241.936	16.364	14.870	0.194	482.117	0.194
1387.257	136.726	93.227	0.947	0.117	1.000	240.806	17.494	16.000	0.209	487.257	0.209
1390.742	137.240	92.812	1.006	0.116	1.000	239.734	18.566	17.072	0.223	490.742	0.223

APPENDIX 2: Data for the reactivity of Argentine coke at 1190°C.

Temp./-C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\frac{t}{V/mW}$ )	Segment	mg change	mg evolved	mg CO evolved	bouyancy			Pf(X)	ti(model)	ti(exp)
									%R / X	%R(adj)	lf(X)			
1188.388	116.847	97.942	0.3582	0.17881	1	253.572	5.328	3.838	0	0	0	0	0	0
1191.488	117.320	97.922	0.36685	0.17784	2	253.521	5.379	3.889	0.04292	0.00000	0.00000	1.03E-12	0.003	0.473
1191.612	117.793	97.899	0.50015	0.17781	2	253.461	5.439	3.949	0.04358	0.00066	0.00022	1.47E-07	1.316	0.946
1191.168	118.266	97.882	0.60599	0.17794	2	253.416	5.484	3.994	0.04407	0.00116	0.00039	4.48E-07	2.298	1.419
1190.983	118.739	97.864	0.61615	0.178	2	253.369	5.531	4.041	0.04460	0.00168	0.00056	9.46E-07	3.341	1.892
1190.864	119.212	97.847	0.62003	0.17804	2	253.326	5.574	4.084	0.04507	0.00215	0.00072	1.55E-06	4.272	2.365
1190.737	119.685	97.832	0.62566	0.17808	2	253.286	5.614	4.124	0.04551	0.00259	0.00086	2.24E-06	5.146	2.838
1190.638	120.158	97.816	0.63051	0.17811	2	253.245	5.655	4.165	0.04596	0.00305	0.00102	3.1E-06	6.054	3.311
1190.548	120.631	97.802	0.63591	0.17814	2	253.209	5.691	4.200	0.04636	0.00344	0.00115	3.95E-06	6.834	3.785
1190.466	121.104	97.789	0.64083	0.17816	2	253.175	5.725	4.235	0.04674	0.00382	0.00128	4.88E-06	7.593	4.258
1190.410	121.577	97.776	0.64575	0.17818	2	253.141	5.759	4.269	0.04711	0.00420	0.00140	5.88E-06	8.339	4.731
1190.337	122.050	97.761	0.65092	0.1782	2	253.104	5.796	4.306	0.04752	0.00461	0.00154	7.08E-06	9.155	5.204
1190.288	122.523	97.747	0.65531	0.17822	2	253.068	5.832	4.342	0.04792	0.00500	0.00167	8.36E-06	9.947	5.677
1190.250	122.996	97.735	0.66089	0.17823	2	253.036	5.864	4.374	0.04827	0.00535	0.00179	9.57E-06	10.646	6.150
1190.199	123.470	97.723	0.66682	0.17825	2	253.004	5.896	4.406	0.04863	0.00571	0.00191	1.09E-05	11.364	6.623
1190.170	123.943	97.712	0.67123	0.17826	2	252.976	5.924	4.434	0.04893	0.00601	0.00201	1.21E-05	11.964	7.096
1190.151	124.416	97.702	0.67569	0.17826	2	252.951	5.949	4.459	0.04921	0.00630	0.00210	1.33E-05	12.535	7.569
1190.132	124.889	97.691	0.68109	0.17827	2	252.922	5.978	4.488	0.04953	0.00662	0.00221	1.46E-05	13.173	8.042
1190.103	125.362	97.680	0.68654	0.17828	2	252.893	6.007	4.517	0.04985	0.00693	0.00232	1.61E-05	13.804	8.515
1190.089	125.835	97.671	0.69186	0.17828	2	252.869	6.031	4.541	0.05011	0.00719	0.00240	1.73E-05	14.327	8.988
1190.071	126.308	97.660	0.69706	0.17829	2	252.843	6.057	4.567	0.05040	0.00749	0.00250	1.88E-05	14.916	9.461
1190.058	126.781	97.648	0.70168	0.17829	2	252.812	6.088	4.598	0.05075	0.00783	0.00262	2.05E-05	15.604	9.934
1190.049	127.254	97.638	0.70652	0.17829	2	252.785	6.115	4.625	0.05104	0.00813	0.00272	2.21E-05	16.196	10.407
1190.035	127.727	97.629	0.71152	0.1783	2	252.761	6.139	4.649	0.05130	0.00839	0.00280	2.35E-05	16.720	10.880
1190.025	128.200	97.620	0.7163	0.1783	2	252.737	6.163	4.673	0.05157	0.00865	0.00289	2.51E-05	17.252	11.354
1190.022	128.673	97.609	0.72174	0.1783	2	252.709	6.191	4.701	0.05188	0.00897	0.00300	2.69E-05	17.884	11.827
1190.020	129.146	97.599	0.72645	0.1783	2	252.684	6.216	4.726	0.05215	0.00924	0.00309	2.86E-05	18.419	12.300
1190.000	129.619	97.589	0.73167	0.17831	2	252.658	6.242	4.752	0.05245	0.00953	0.00319	3.04E-05	19.013	12.773
1190.012	130.092	97.581	0.73699	0.17831	2	252.637	6.263	4.773	0.05268	0.00976	0.00326	3.19E-05	19.476	13.246
1190.007	130.565	97.572	0.74201	0.17831	2	252.615	6.285	4.795	0.05292	0.01000	0.00335	3.35E-05	19.962	13.719
1190.010	131.039	97.563	0.74626	0.17831	2	252.590	6.310	4.820	0.05320	0.01028	0.00344	3.54E-05	20.517	14.192
1190.005	131.512	97.552	0.75098	0.17831	2	252.563	6.337	4.847	0.05349	0.01057	0.00354	3.74E-	21.100	14.665

												05		
1190.000	131.985	97.545	0.75644	0.17831	2	252.544	6.356	4.866	0.05370	0.01079	0.00361	3.9E-05	21.537	15.138
1190.005	132.458	97.536	0.76209	0.17831	2	252.520	6.380	4.890	0.05397	0.01105	0.00370	4.09E-05	22.068	15.611
1190.002	132.931	97.527	0.76679	0.17831	2	252.498	6.402	4.911	0.05420	0.01129	0.00378	4.27E-05	22.541	16.084
1190.005	133.404	97.519	0.77161	0.17831	2	252.476	6.424	4.934	0.05445	0.01153	0.00386	4.45E-05	23.030	16.557
1190.008	133.877	97.510	0.77766	0.17831	2	252.453	6.447	4.957	0.05471	0.01179	0.00395	4.66E-05	23.555	17.030
1190.001	134.350	97.502	0.78296	0.17831	2	252.432	6.468	4.978	0.05494	0.01203	0.00402	4.85E-05	24.029	17.503
1189.991	134.823	97.494	0.78738	0.17831	2	252.412	6.488	4.998	0.05516	0.01224	0.00410	5.02E-05	24.467	17.976
1189.985	135.296	97.485	0.79247	0.17831	2	252.390	6.510	5.020	0.05540	0.01249	0.00418	5.23E-05	24.958	18.449
1190.002	135.769	97.476	0.79721	0.17831	2	252.366	6.534	5.044	0.05566	0.01275	0.00427	5.45E-05	25.479	18.923
1189.998	136.242	97.469	0.80176	0.17831	2	252.347	6.553	5.063	0.05588	0.01296	0.00434	5.63E-05	25.917	19.396
1189.992	136.715	97.460	0.80648	0.17831	2	252.325	6.575	5.085	0.05612	0.01320	0.00442	5.84E-05	26.400	19.869
1190.005	137.188	97.453	0.81125	0.17831	2	252.305	6.595	5.105	0.05633	0.01342	0.00449	6.04E-05	26.838	20.342
1190.000	137.661	97.444	0.81674	0.17831	2	252.284	6.616	5.126	0.05657	0.01366	0.00457	6.26E-05	27.322	20.815
1189.988	138.134	97.436	0.82209	0.17831	2	252.262	6.638	5.148	0.05681	0.01390	0.00465	6.48E-05	27.805	21.288
1189.998	138.608	97.428	0.82703	0.17831	2	252.240	6.660	5.170	0.05705	0.01414	0.00473	6.7E-05	28.289	21.761
1190.001	139.081	97.419	0.83107	0.17831	2	252.218	6.682	5.192	0.05729	0.01438	0.00482	6.93E-05	28.773	22.234
1189.991	139.554	97.412	0.83645	0.17831	2	252.199	6.701	5.211	0.05751	0.01459	0.00489	7.15E-05	29.212	22.707
1189.997	140.027	97.403	0.84114	0.17831	2	252.177	6.723	5.233	0.05775	0.01483	0.00497	7.38E-05	29.695	23.180
1189.994	140.500	97.396	0.8467	0.17831	2	252.157	6.743	5.253	0.05797	0.01505	0.00504	7.6E-05	30.141	23.653
1189.991	140.973	97.389	0.85177	0.17831	2	252.141	6.759	5.269	0.05814	0.01523	0.00510	7.78E-05	30.495	24.126
1190.000	141.446	97.382	0.8558	0.17831	2	252.122	6.778	5.288	0.05835	0.01544	0.00517	8E-05	30.922	24.599
1189.998	141.919	97.373	0.86109	0.17831	2	252.098	6.802	5.312	0.05862	0.01570	0.00526	8.28E-05	31.452	25.072
1190.011	142.392	97.365	0.86664	0.17831	2	252.079	6.821	5.331	0.05884	0.01592	0.00534	8.51E-05	31.897	25.545
1189.992	142.865	97.357	0.87168	0.17831	2	252.057	6.843	5.353	0.05908	0.01616	0.00542	8.77E-05	32.382	26.018
1189.994	143.338	97.350	0.87612	0.17831	2	252.039	6.861	5.371	0.05928	0.01636	0.00548	8.99E-05	32.787	26.492
1190.000	143.811	97.342	0.88089	0.17831	2	252.019	6.881	5.391	0.05949	0.01657	0.00556	9.22E-05	33.220	26.965
1189.991	144.284	97.335	0.88628	0.17831	2	252.001	6.899	5.409	0.05969	0.01678	0.00562	9.45E-05	33.634	27.438
1189.998	144.757	97.329	0.89018	0.17831	2	251.986	6.914	5.424	0.05986	0.01694	0.00568	9.64E-05	33.972	27.911
1189.991	145.230	97.321	0.89492	0.17831	2	251.963	6.937	5.447	0.06011	0.01720	0.00577	9.94E-05	34.486	28.384
1189.995	145.704	97.313	0.89977	0.17831	2	251.944	6.956	5.466	0.06032	0.01740	0.00584	0.000102	34.905	28.857
1189.999	146.177	97.305	0.90485	0.17831	2	251.923	6.977	5.487	0.06055	0.01764	0.00591	0.000105	35.375	29.330
1189.988	146.650	97.298	0.90955	0.17831	2	251.905	6.995	5.505	0.06076	0.01784	0.00598	0.000107	35.789	29.803
1189.986	147.123	97.290	0.91486	0.17831	2	251.884	7.016	5.526	0.06098	0.01807	0.00606	0.00011	36.251	30.276
1189.989	147.596	97.282	0.91907	0.17831	2	251.863	7.037	5.547	0.06121	0.01830	0.00614	0.000113	36.716	30.749
1190.003	148.069	97.275	0.92409	0.17831	2	251.845	7.055	5.565	0.06141	0.01849	0.00620	0.000115	37.116	31.222
1190.004	148.542	97.268	0.92927	0.17831	2	251.826	7.074	5.584	0.06162	0.01870	0.00627	0.00011	37.544	31.695

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1190.009	149.015	97.260	0.9346	0.17831	2	251.806	7.094	5.604	0.06184	0.01892	0.00635	0.00012	37.993	32.168
1190.004	149.488	97.253	0.93958	0.17831	2	251.787	7.113	5.623	0.06205	0.01914	0.00642	0.00012	38.425	32.641
1189.997	149.961	97.244	0.94416	0.17831	2	251.765	7.135	5.645	0.06229	0.01938	0.00650	0.00012	38.915	33.114
1189.991	150.434	97.237	0.94878	0.17831	2	251.748	7.152	5.662	0.06249	0.01957	0.00657	0.00012	39.307	33.588
1189.993	150.907	97.231	0.9529	0.17831	2	251.730	7.170	5.680	0.06268	0.01977	0.00663	0.00013	39.709	34.061
1189.989	151.380	97.223	0.95815	0.17831	2	251.711	7.189	5.699	0.06290	0.01998	0.00671	0.00013	40.147	34.534
1189.995	151.853	97.217	0.96381	0.17831	2	251.696	7.204	5.714	0.06306	0.02015	0.00676	0.00013	40.482	35.007
1189.995	152.326	97.209	0.96858	0.17831	2	251.673	7.227	5.737	0.06331	0.02040	0.00685	0.00014	40.987	35.480
1189.993	152.799	97.200	0.97338	0.17831	2	251.651	7.249	5.759	0.06355	0.02064	0.00693	0.00014	41.476	35.953
1189.994	153.273	97.193	0.97827	0.17831	2	251.633	7.267	5.777	0.06375	0.02083	0.00699	0.00014	41.883	36.426
1189.998	153.746	97.186	0.98308	0.17831	2	251.614	7.286	5.796	0.06396	0.02105	0.00706	0.00014	42.313	36.899
1190.003	154.219	97.179	0.98766	0.17831	2	251.597	7.303	5.813	0.06415	0.02124	0.00713	0.00015	42.704	37.372
1189.995	154.692	97.172	0.9924	0.17831	2	251.579	7.321	5.831	0.06435	0.02143	0.00720	0.00015	43.107	37.845
1189.991	155.165	97.166	0.99704	0.17831	2	251.561	7.339	5.848	0.06454	0.02163	0.00726	0.00015	43.500	38.318
1189.989	155.638	97.158	1.00181	0.17831	2	251.543	7.357	5.867	0.06475	0.02184	0.00733	0.00016	43.927	38.791
1189.995	156.111	97.151	1.00718	0.17831	2	251.524	7.376	5.886	0.06496	0.02204	0.00740	0.00016	44.349	39.264
1190.003	156.584	97.144	1.01185	0.17831	2	251.505	7.395	5.905	0.06516	0.02225	0.00747	0.00016	44.771	39.737
1189.999	157.057	97.137	1.01635	0.17831	2	251.487	7.413	5.923	0.06537	0.02245	0.00754	0.00017	45.187	40.210
1189.997	157.530	97.129	1.02104	0.17831	2	251.466	7.434	5.944	0.06559	0.02268	0.00762	0.00017	45.649	40.683
1190.003	158.003	97.120	1.02564	0.17831	2	251.444	7.456	5.966	0.06584	0.02292	0.00770	0.00017	46.142	41.157
1190.006	158.476	97.113	1.03089	0.17831	2	251.427	7.473	5.983	0.06603	0.02312	0.00777	0.00018	46.543	41.630
1189.999	158.949	97.106	1.03641	0.17831	2	251.407	7.493	6.003	0.06625	0.02333	0.00784	0.00018	46.985	42.103
1190.003	159.422	97.097	1.04138	0.17831	2	251.385	7.515	6.025	0.06649	0.02357	0.00792	0.00018	47.479	42.576
1190.003	159.895	97.090	1.0459	0.17831	2	251.365	7.535	6.045	0.06671	0.02380	0.00800	0.00019	47.938	43.049
1189.994	160.368	97.084	1.05069	0.17831	2	251.350	7.550	6.060	0.06688	0.02397	0.00805	0.00019	48.281	43.522
1190.001	160.842	97.075	1.05555	0.17831	2	251.327	7.573	6.083	0.06713	0.02421	0.00814	0.00019	48.782	43.995
1190.004	161.315	97.068	1.0605	0.17831	2	251.308	7.592	6.102	0.06734	0.02443	0.00821	0.00020	49.224	44.468
1190.012	161.788	97.060	1.06496	0.17831	2	251.289	7.611	6.121	0.06755	0.02463	0.00828	0.00020	49.643	44.941
1189.993	162.261	97.054	1.0699	0.17831	2	251.273	7.627	6.137	0.06773	0.02481	0.00834	0.00020	50.016	45.414
1190.002	162.734	97.047	1.07407	0.17831	2	251.253	7.647	6.157	0.06794	0.02503	0.00841	0.00021	50.456	45.887
1190.003	163.207	97.039	1.07942	0.17831	2	251.235	7.665	6.175	0.06815	0.02523	0.00848	0.00021	50.878	46.360
1190.012	163.680	97.031	1.08459	0.17831	2	251.214	7.686	6.196	0.06838	0.02546	0.00856	0.00021	51.348	46.833
1190.023	164.153	97.025	1.08952	0.1783	2	251.198	7.702	6.212	0.06855	0.02564	0.00862	0.00022	51.705	47.306
1190.006	164.626	97.017	1.09442	0.17831	2	251.178	7.722	6.232	0.06878	0.02586	0.00870	0.00022	52.168	47.779
1189.991	165.099	97.010	1.09988	0.17831	2	251.159	7.741	6.251	0.06899	0.02607	0.00877	0.00022	52.598	48.252

1190.011	165.572	97.004	1.10383	0.17831	2	251.143	7.757	6.267	0.06916	0.02624	0.00882	0.00023 2	52.949	48.726
1189.999	166.045	96.997	1.10906	0.17831	2	251.124	7.776	6.285	0.06937	0.02645	0.00890	0.00023 6	53.377	49.199
1190.005	166.518	96.988	1.11413	0.17831	2	251.101	7.799	6.309	0.06962	0.02671	0.00898	0.00024 1	53.908	49.672
1189.994	166.991	96.981	1.11907	0.17831	2	251.084	7.816	6.326	0.06981	0.02690	0.00905	0.00024 4	54.297	50.145
1189.992	167.464	96.974	1.12274	0.17831	2	251.066	7.834	6.344	0.07001	0.02710	0.00912	0.00024 8	54.711	50.618
1190.013	167.937	96.966	1.12781	0.1783	2	251.044	7.856	6.366	0.07025	0.02734	0.00920	0.00025 2	55.204	51.091
1189.995	168.411	96.959	1.13351	0.17831	2	251.027	7.873	6.383	0.07044	0.02753	0.00926	0.00025 6	55.590	51.564
1189.997	168.884	96.953	1.13785	0.17831	2	251.013	7.887	6.397	0.07060	0.02769	0.00931	0.00025 9	55.917	52.037
1189.998	169.357	96.944	1.14263	0.17831	2	250.987	7.913	6.423	0.07088	0.02797	0.00941	0.00026 4	56.502	52.510
1190.014	169.830	96.938	1.14727	0.1783	2	250.971	7.929	6.439	0.07105	0.02814	0.00947	0.00026 7	56.851	52.983
1189.999	170.303	96.931	1.15252	0.17831	2	250.956	7.944	6.454	0.07123	0.02831	0.00953	0.00027 1	57.212	53.456
1190.004	170.776	96.924	1.15772	0.17831	2	250.936	7.964	6.474	0.07145	0.02853	0.00960	0.00027 5	57.662	53.929
1190.003	171.249	96.917	1.16287	0.17831	2	250.918	7.982	6.492	0.07164	0.02873	0.00967	0.00027 9	58.065	54.402
1189.997	171.722	96.910	1.16698	0.17831	2	250.900	8.000	6.510	0.07184	0.02892	0.00974	0.00028 2	58.467	54.875
1190.001	172.195	96.902	1.17186	0.17831	2	250.879	8.021	6.531	0.07208	0.02916	0.00982	0.00028 7	58.962	55.348
1189.996	172.668	96.896	1.17723	0.17831	2	250.863	8.037	6.547	0.07225	0.02934	0.00988	0.00029 1	59.321	55.821
1190.007	173.141	96.887	1.18238	0.17831	2	250.841	8.059	6.569	0.07249	0.02957	0.00996	0.00029 5	59.810	56.295
1190.001	173.614	96.880	1.18718	0.17831	2	250.821	8.079	6.588	0.07271	0.02979	0.01003	0.0003	60.264	56.768
1190.001	174.087	96.873	1.19214	0.17831	2	250.803	8.097	6.607	0.07291	0.02999	0.01010	0.00030 4	60.675	57.241
1189.984	174.560	96.867	1.19709	0.17831	2	250.790	8.110	6.620	0.07306	0.03015	0.01015	0.00030 7	60.992	57.714
1189.989	175.033	96.861	1.20206	0.17831	2	250.773	8.127	6.637	0.07325	0.03033	0.01022	0.00031 1	61.379	58.187
1189.995	175.506	96.852	1.20671	0.17831	2	250.751	8.149	6.659	0.07349	0.03058	0.01030	0.00031 6	61.878	58.660
1190.001	175.980	96.846	1.2107	0.17831	2	250.733	8.167	6.677	0.07368	0.03077	0.01036	0.00032	62.277	59.133
1189.994	176.453	96.836	1.21631	0.17831	2	250.708	8.192	6.702	0.07396	0.03105	0.01046	0.00032 6	62.855	59.606
1189.994	176.926	96.829	1.22144	0.17831	2	250.691	8.209	6.719	0.07415	0.03124	0.01052	0.00033	63.245	60.079
1190.003	177.399	96.822	1.22549	0.17831	2	250.672	8.228	6.738	0.07436	0.03144	0.01059	0.00033 4	63.669	60.552
1190.000	177.872	96.814	1.23015	0.17831	2	250.652	8.248	6.758	0.07458	0.03167	0.01067	0.00033 9	64.134	61.025
1190.002	178.345	96.808	1.23565	0.17831	2	250.635	8.265	6.775	0.07476	0.03185	0.01073	0.00034 3	64.511	61.498
1190.005	178.818	96.802	1.24059	0.17831	2	250.620	8.280	6.790	0.07493	0.03201	0.01079	0.00034 7	64.856	61.971
1190.008	179.291	96.794	1.24537	0.17831	2	250.601	8.299	6.809	0.07514	0.03223	0.01086	0.00035 1	65.301	62.444
1190.006	179.764	96.788	1.25025	0.17831	2	250.584	8.316	6.825	0.07532	0.03241	0.01092	0.00035 5	65.673	62.917
1189.991	180.237	96.780	1.25478	0.17831	2	250.565	8.335	6.845	0.07554	0.03263	0.01100	0.00036	66.129	63.390
1190.001	180.710	96.772	1.25936	0.17831	2	250.542	8.358	6.868	0.07579	0.03288	0.01108	0.00036 6	66.638	63.864
1189.998	181.183	96.764	1.26459	0.17831	2	250.522	8.378	6.888	0.07602	0.03310	0.01116	0.00037 1	67.105	64.337
1189.997	181.656	96.757	1.2693	0.17831	2	250.504	8.396	6.906	0.07621	0.03330	0.01122	0.00037 5	67.514	64.810
1190.000	182.129	96.749	1.2738	0.17831	2	250.484	8.416	6.926	0.07643	0.03351	0.01130	0.00038	67.963	65.283

1189.997	182.602	96.743	1.27916	0.17831	2	250.468	8.432	6.942	0.07661	0.03370	0.01136	0.000384	68.340	65.756
1190.006	183.076	96.736	1.28373	0.17831	2	250.448	8.452	6.962	0.07683	0.03391	0.01143	0.000389	68.791	66.229
1190.009	183.549	96.728	1.28826	0.17831	2	250.428	8.472	6.982	0.07705	0.03413	0.01151	0.000394	69.248	66.702
1190.000	184.022	96.721	1.29373	0.17831	2	250.412	8.488	6.998	0.07723	0.03431	0.01157	0.000399	69.625	67.175
1189.994	184.495	96.713	1.29891	0.17831	2	250.390	8.510	7.020	0.07747	0.03456	0.01166	0.000404	70.134	67.648
1189.996	184.968	96.705	1.30316	0.17831	2	250.369	8.531	7.041	0.07770	0.03478	0.01173	0.00041	70.601	68.121
1190.000	185.441	96.698	1.30795	0.17831	2	250.351	8.549	7.059	0.07790	0.03499	0.01180	0.000414	71.022	68.594
1189.996	185.914	96.691	1.31345	0.17831	2	250.332	8.568	7.078	0.07811	0.03520	0.01187	0.00042	71.463	69.067
1189.999	186.387	96.684	1.31784	0.17831	2	250.315	8.585	7.095	0.07829	0.03538	0.01193	0.000424	71.837	69.540
1190.008	186.860	96.678	1.32261	0.17831	2	250.300	8.600	7.110	0.07847	0.03555	0.01199	0.000428	72.200	70.013
1190.002	187.333	96.672	1.32777	0.17831	2	250.284	8.616	7.126	0.07864	0.03572	0.01205	0.000432	72.550	70.486
1190.001	187.806	96.665	1.33296	0.17831	2	250.266	8.634	7.144	0.07884	0.03593	0.01212	0.000437	72.977	70.960
1189.999	188.279	96.656	1.33777	0.17831	2	250.243	8.657	7.167	0.07909	0.03618	0.01221	0.000443	73.496	71.433
1190.000	188.752	96.649	1.34247	0.17831	2	250.223	8.677	7.187	0.07931	0.03640	0.01228	0.000449	73.958	71.906
1190.004	189.225	96.643	1.34813	0.17831	2	250.208	8.692	7.202	0.07948	0.03657	0.01234	0.000453	74.316	72.379
1190.003	189.698	96.637	1.35305	0.17831	2	250.194	8.706	7.216	0.07964	0.03672	0.01239	0.000457	74.631	72.852
1190.005	190.171	96.630	1.35758	0.17831	2	250.175	8.725	7.235	0.07984	0.03693	0.01246	0.000462	75.063	73.325
1189.994	190.645	96.622	1.36231	0.17831	2	250.154	8.746	7.256	0.08007	0.03716	0.01254	0.000468	75.546	73.798
1189.999	191.118	96.616	1.36737	0.17831	2	250.138	8.762	7.272	0.08025	0.03734	0.01260	0.000473	75.916	74.271
1190.003	191.591	96.609	1.37221	0.17831	2	250.121	8.779	7.289	0.08044	0.03752	0.01267	0.000477	76.307	74.744
1189.995	192.064	96.601	1.37709	0.17831	2	250.100	8.800	7.310	0.08067	0.03775	0.01275	0.000483	76.784	75.217
1190.003	192.537	96.594	1.38197	0.17831	2	250.083	8.817	7.327	0.08086	0.03795	0.01281	0.000488	77.186	75.690
1190.000	193.010	96.589	1.38624	0.17831	2	250.069	8.831	7.341	0.08101	0.03810	0.01286	0.000492	77.508	76.163
1189.990	193.483	96.581	1.39111	0.17831	2	250.049	8.851	7.361	0.08124	0.03832	0.01294	0.000498	77.970	76.636
1189.989	193.956	96.574	1.39549	0.17831	2	250.029	8.871	7.381	0.08145	0.03854	0.01302	0.000504	78.428	77.109
1190.006	194.429	96.567	1.40047	0.17831	2	250.012	8.888	7.398	0.08164	0.03872	0.01308	0.000509	78.813	77.582
1190.000	194.902	96.559	1.40611	0.17831	2	249.990	8.910	7.420	0.08188	0.03897	0.01316	0.000515	79.325	78.055
1189.990	195.375	96.551	1.41112	0.17831	2	249.972	8.928	7.438	0.08209	0.03917	0.01323	0.000521	79.753	78.529
1189.993	195.848	96.546	1.41631	0.17831	2	249.957	8.943	7.453	0.08225	0.03934	0.01329	0.000525	80.099	79.002
1189.997	196.321	96.539	1.42081	0.17831	2	249.939	8.961	7.471	0.08245	0.03953	0.01336	0.00053	80.503	79.475
1190.014	196.794	96.531	1.42537	0.1783	2	249.919	8.981	7.491	0.08267	0.03976	0.01343	0.000536	80.977	79.948
1190.008	197.267	96.524	1.43005	0.17831	2	249.901	8.999	7.509	0.08287	0.03995	0.01350	0.000542	81.377	80.421
1190.000	197.740	96.515	1.43535	0.17831	2	249.877	9.023	7.533	0.08314	0.04022	0.01359	0.000549	81.946	80.894
1189.998	198.214	96.510	1.44026	0.17831	2	249.863	9.037	7.547	0.08328	0.04037	0.01364	0.000553	82.253	81.367
1189.996	198.687	96.503	1.44521	0.17831	2	249.846	9.054	7.564	0.08348	0.04056	0.01371	0.000559	82.663	81.840



1189.999	199.160	96.497	1.44983	0.17831	2	249.832	9.068	7.578	0.08363	0.04072	0.01376	0.000563	82.981	82.313
1189.998	199.633	96.490	1.45458	0.17831	2	249.814	9.086	7.596	0.08383	0.04092	0.01383	0.000568	83.403	82.786
1189.997	200.106	96.483	1.45922	0.17831	2	249.794	9.106	7.616	0.08405	0.04114	0.01391	0.000575	83.867	83.259
1190.000	200.579	96.474	1.46416	0.17831	2	249.772	9.128	7.638	0.08429	0.04137	0.01399	0.000581	84.362	83.732
1189.998	201.052	96.467	1.469	0.17831	2	249.754	9.146	7.656	0.08449	0.04157	0.01405	0.000587	84.774	84.205
1189.992	201.525	96.459	1.47453	0.17831	2	249.733	9.167	7.677	0.08473	0.04181	0.01414	0.000594	85.278	84.678
1189.995	201.998	96.452	1.47877	0.17831	2	249.715	9.185	7.695	0.08492	0.04200	0.01420	0.000599	85.681	85.151
1190.000	202.471	96.447	1.48384	0.17831	2	249.701	9.199	7.709	0.08507	0.04215	0.01425	0.000604	85.999	85.624
1190.002	202.944	96.441	1.49011	0.17831	2	249.685	9.215	7.724	0.08525	0.04233	0.01431	0.000609	86.368	86.098
1189.993	203.417	96.433	1.49441	0.17831	2	249.666	9.234	7.744	0.08546	0.04255	0.01439	0.000615	86.825	86.571
1189.999	203.890	96.428	1.49945	0.17831	2	249.652	9.248	7.758	0.08561	0.04270	0.01444	0.00062	87.144	87.044
1190.007	204.363	96.420	1.50403	0.17831	2	249.632	9.268	7.778	0.08583	0.04292	0.01452	0.000626	87.600	87.517
1189.998	204.836	96.412	1.51021	0.17831	2	249.611	9.289	7.799	0.08607	0.04316	0.01460	0.000633	88.104	87.990
1190.003	205.309	96.405	1.51428	0.17831	2	249.593	9.307	7.817	0.08627	0.04335	0.01467	0.000639	88.519	88.463
1190.006	205.783	96.398	1.51942	0.17831	2	249.575	9.325	7.835	0.08646	0.04355	0.01473	0.000645	88.928	88.936
1190.002	206.256	96.391	1.52375	0.17831	2	249.555	9.345	7.855	0.08668	0.04377	0.01481	0.000651	89.386	89.409
1190.007	206.729	96.384	1.529	0.17831	2	249.538	9.362	7.872	0.08688	0.04396	0.01487	0.000657	89.798	89.882
1189.999	207.202	96.376	1.53443	0.17831	2	249.518	9.382	7.892	0.08710	0.04418	0.01495	0.000664	90.258	90.355
1190.006	207.675	96.371	1.53917	0.17831	2	249.504	9.396	7.906	0.08725	0.04434	0.01500	0.000669	90.592	90.828
1190.010	208.148	96.365	1.54374	0.17831	2	249.489	9.411	7.921	0.08742	0.04450	0.01506	0.000674	90.937	91.301
1190.005	208.621	96.356	1.54843	0.17831	2	249.467	9.433	7.943	0.08766	0.04474	0.01514	0.000681	91.446	91.774
1190.005	209.094	96.351	1.55329	0.17831	2	249.453	9.447	7.957	0.08782	0.04490	0.01520	0.000686	91.778	92.247
1190.002	209.567	96.343	1.55796	0.17831	2	249.432	9.468	7.978	0.08804	0.04513	0.01527	0.000693	92.254	92.720
1189.997	210.040	96.336	1.56354	0.17831	2	249.413	9.487	7.997	0.08826	0.04534	0.01535	0.000699	92.704	93.193
1190.000	210.513	96.331	1.56885	0.17831	2	249.400	9.500	8.010	0.08840	0.04548	0.01540	0.000704	93.007	93.667
1190.005	210.986	96.322	1.5736	0.17831	2	249.377	9.523	8.033	0.08865	0.04574	0.01548	0.000712	93.538	94.140
1190.002	211.459	96.316	1.57887	0.17831	2	249.361	9.539	8.049	0.08883	0.04591	0.01554	0.000717	93.910	94.613
1190.008	211.932	96.310	1.58348	0.17831	2	249.346	9.554	8.064	0.08899	0.04608	0.01560	0.000723	94.253	95.086
1190.009	212.405	96.304	1.58901	0.17831	2	249.330	9.570	8.080	0.08917	0.04625	0.01566	0.000728	94.624	95.559
1190.001	212.879	96.297	1.59379	0.17831	2	249.313	9.587	8.097	0.08935	0.04644	0.01573	0.000734	95.019	96.032
1189.999	213.352	96.290	1.59841	0.17831	2	249.294	9.606	8.116	0.08957	0.04665	0.01580	0.000741	95.476	96.505
1190.002	213.825	96.283	1.60354	0.17831	2	249.275	9.625	8.134	0.08977	0.04686	0.01587	0.000747	95.901	96.978
1190.008	214.298	96.276	1.60824	0.17831	2	249.257	9.643	8.153	0.08997	0.04705	0.01594	0.000754	96.323	97.451
1190.003	214.771	96.270	1.61246	0.17831	2	249.243	9.657	8.167	0.09013	0.04722	0.01599	0.000759	96.665	97.924

1190.001	215.244	96.264	1.61746	0.17831	2	249.227	9.673	8.183	0.09031	0.04739	0.01605	0.000765	97.038	98.397
1189.988	215.717	96.256	1.62292	0.17831	2	249.207	9.693	8.203	0.09052	0.04761	0.01613	0.000772	97.493	98.870
1189.996	216.190	96.249	1.62726	0.17831	2	249.188	9.712	8.222	0.09074	0.04782	0.01620	0.000779	97.949	99.343
1190.004	216.663	96.241	1.63216	0.17831	2	249.167	9.733	8.243	0.09097	0.04806	0.01628	0.000787	98.442	99.816
1189.999	217.136	96.232	1.63757	0.17831	2	249.146	9.754	8.264	0.09120	0.04829	0.01636	0.000794	98.929	100.289
1190.000	217.609	96.225	1.64123	0.17831	2	249.128	9.772	8.282	0.09140	0.04849	0.01643	0.000801	99.357	100.762
1190.007	218.082	96.219	1.64551	0.17831	2	249.110	9.790	8.300	0.09160	0.04868	0.01650	0.000808	99.769	101.236
1190.015	218.555	96.212	1.65119	0.17831	2	249.092	9.808	8.318	0.09179	0.04888	0.01657	0.000814	100.183	101.709
1190.004	219.028	96.205	1.6562	0.17831	2	249.074	9.826	8.336	0.09199	0.04908	0.01663	0.000821	100.602	102.182
1189.998	219.501	96.198	1.66085	0.17831	2	249.057	9.843	8.353	0.09218	0.04926	0.01670	0.000827	101.002	102.655
1189.998	219.974	96.190	1.66584	0.17831	2	249.037	9.863	8.373	0.09241	0.04949	0.01678	0.000835	101.485	103.128
1189.993	220.448	96.183	1.67103	0.17831	2	249.018	9.882	8.392	0.09261	0.04969	0.01685	0.000842	101.908	103.601
1190.004	220.921	96.178	1.67614	0.17831	2	249.005	9.895	8.405	0.09275	0.04984	0.01690	0.000847	102.220	104.074
1190.001	221.394	96.171	1.68079	0.17831	2	248.987	9.913	8.423	0.09296	0.05004	0.01697	0.000854	102.652	104.547
1189.998	221.867	96.164	1.68547	0.17831	2	248.968	9.932	8.442	0.09316	0.05024	0.01704	0.000861	103.079	105.020
1190.007	222.340	96.158	1.69031	0.17831	2	248.953	9.947	8.457	0.09333	0.05042	0.01710	0.000867	103.445	105.493
1189.994	222.813	96.150	1.69496	0.17831	2	248.933	9.967	8.477	0.09355	0.05064	0.01717	0.000875	103.918	105.966
1189.997	223.286	96.142	1.69985	0.17831	2	248.913	9.987	8.497	0.09377	0.05086	0.01725	0.000882	104.382	106.439
1190.001	223.759	96.137	1.70454	0.17831	2	248.898	10.002	8.512	0.09393	0.05102	0.01730	0.000888	104.726	106.912
1189.994	224.232	96.130	1.70927	0.17831	2	248.881	10.019	8.529	0.09413	0.05121	0.01737	0.000895	105.140	107.385
1189.999	224.705	96.123	1.71481	0.17831	2	248.862	10.038	8.548	0.09434	0.05142	0.01744	0.000902	105.583	107.858
1190.000	225.178	96.117	1.72034	0.17831	2	248.847	10.053	8.563	0.09450	0.05158	0.01750	0.000908	105.926	108.332
1189.993	225.651	96.110	1.72536	0.17831	2	248.829	10.071	8.581	0.09470	0.05179	0.01757	0.000915	106.358	108.805
1189.997	226.124	96.102	1.73009	0.17831	2	248.809	10.091	8.601	0.09492	0.05200	0.01764	0.000923	106.822	109.278
1189.992	226.597	96.097	1.73521	0.17831	2	248.795	10.105	8.615	0.09507	0.05216	0.01770	0.000928	107.143	109.751
1189.990	227.070	96.090	1.73996	0.17831	2	248.776	10.124	8.634	0.09528	0.05237	0.01777	0.000936	107.595	110.224
1190.002	227.543	96.082	1.7445	0.17831	2	248.757	10.143	8.653	0.09549	0.05257	0.01784	0.000944	108.035	110.697
1190.009	228.017	96.076	1.74961	0.17831	2	248.742	10.158	8.668	0.09566	0.05274	0.01790	0.00095	108.399	111.170
1190.007	228.490	96.070	1.75478	0.17831	2	248.726	10.174	8.684	0.09583	0.05292	0.01796	0.000956	108.762	111.643
1189.997	228.963	96.064	1.75998	0.17831	2	248.709	10.191	8.701	0.09602	0.05311	0.01802	0.000963	109.168	112.116
1190.001	229.436	96.056	1.76412	0.17831	2	248.688	10.212	8.722	0.09625	0.05334	0.01810	0.000971	109.662	112.589
1189.996	229.909	96.050	1.76859	0.17831	2	248.672	10.228	8.738	0.09643	0.05351	0.01816	0.000978	110.031	113.062
1189.991	230.382	96.043	1.77404	0.17831	2	248.655	10.245	8.755	0.09662	0.05370	0.01823	0.000985	110.436	113.535
1189.997	230.855	96.036	1.77877	0.17831	2	248.638	10.262	8.772	0.09681	0.05389	0.01830	0.000992	110.847	114.008

1189.996	231.328	96.027	1.78399	0.17831	2	248.613	10.287	8.797	0.09708	0.05417	0.01839	0.00100 2	111.429	114.481
1190.001	231.801	96.021	1.78905	0.17831	2	248.600	10.300	8.810	0.09723	0.05431	0.01844	0.00100 8	111.747	114.954
1189.999	232.274	96.014	1.79426	0.17831	2	248.580	10.320	8.830	0.09745	0.05454	0.01852	0.00101 6	112.220	115.427
1190.006	232.747	96.008	1.79916	0.17831	2	248.564	10.336	8.846	0.09762	0.05470	0.01858	0.00102 2	112.576	115.901
1190.005	233.220	96.002	1.80363	0.17831	2	248.550	10.350	8.860	0.09777	0.05486	0.01863	0.00102 8	112.907	116.374
1189.993	233.693	95.995	1.8085	0.17831	2	248.532	10.368	8.878	0.09797	0.05506	0.01870	0.00103 6	113.335	116.847
1190.010	234.166	95.988	1.81355	0.17831	2	248.513	10.387	8.897	0.09819	0.05527	0.01877	0.00104 4	113.796	117.320
1190.003	234.639	95.982	1.81881	0.17831	2	248.497	10.403	8.913	0.09836	0.05544	0.01883	0.00105 1	114.161	117.793
1190.008	235.112	95.976	1.82369	0.17831	2	248.481	10.419	8.929	0.09854	0.05562	0.01890	0.00105 8	114.544	118.266
1190.004	235.586	95.967	1.82859	0.17831	2	248.458	10.442	8.952	0.09880	0.05588	0.01899	0.00106 8	115.098	118.739
1189.993	236.059	95.963	1.83357	0.17831	2	248.448	10.452	8.962	0.09890	0.05599	0.01902	0.00107 2	115.327	119.212
1190.015	236.532	95.955	1.838	0.1783	2	248.428	10.472	8.982	0.09912	0.05621	0.01910	0.00108	115.796	119.685

APPENDIX 3: Data for the reactivity of Argentine coke at 1240°C.

Temp./- C	Time/min	Mass/%	DTA/(m W/mg)	Sensit./( $\frac{d}{V/mW}$ )	Segm ent	mg change	mg evolved	mg CO evolved	bouyancy				ti(model)	ti(exp)
									%R(X)	%R(adj)	lf(X)	Pf(X)		
1241.44 72	122.69894	97.56284	0.39176	0.16212	2	252.88288	6.31712	4.60744	0	0	0	0	0	0
1240.97 291	123.182	97.54113	0.52764	0.16227	2	252.82661	6.37339	4.66371	0.0608 586	0.00037 656	0.0001 255	4.727E- 08	0.2811219	0.48306
1240.81 469	123.66507	97.51765	0.53214	0.16232	2	252.76575	6.43425	4.72457	0.0616 527	0.00117 075	0.0003 904	4.571E- 07	0.8743196	0.96613
1240.69 61	124.14814	97.49393	0.53404	0.16236	2	252.70427	6.49573	4.78605	0.0624 551	0.00197 305	0.0006 581	1.299E- 06	1.4739867	1.4492
1240.58 698	124.6312	97.47229	0.53774	0.16239	2	252.64818	6.55182	4.84214	0.0631 87	0.00270 501	0.0009 025	2.442E- 06	2.0214256	1.93226
1240.48 626	125.11427	97.45189	0.53978	0.16243	2	252.59530	6.60470	4.89502	0.0638 77	0.00339 502	0.0011 33	3.848E- 06	2.5378074	2.41533
1240.41 244	125.59734	97.43331	0.54183	0.16245	2	252.54714	6.65286	4.94318	0.0645 055	0.00402 347	0.0013 43	5.406E- 06	3.0083835	2.8984
1240.34 629	126.0804	97.41352	0.5457	0.16247	2	252.49584	6.70416	4.99447	0.0651 748	0.00469 284	0.0015 667	7.356E- 06	3.5098819	3.38146
1240.29 039	126.56347	97.39509	0.54851	0.16249	2	252.44807	6.75193	5.04224	0.0657 982	0.00531 622	0.0017 752	9.443E- 06	3.9771735	3.86453
1240.24 028	127.04654	97.37641	0.55149	0.1625	2	252.39965	6.80035	5.09066	0.0664 301	0.00594 805	0.0019 866	1.182E- 05	4.451057	4.3476
1240.20 417	127.5296	97.35792	0.55508	0.16252	2	252.35173	6.84827	5.13859	0.0670 555	0.00657 346	0.0021 96	1.445E- 05	4.9203716	4.83066
1240.16 542	128.01267	97.34118	0.55785	0.16253	2	252.30834	6.89166	5.18198	0.0676 217	0.00713 967	0.0023 856	1.705E- 05	5.3454834	5.31373
1240.12 449	128.49574	97.32379	0.5606	0.16254	2	252.26326	6.93674	5.22705	0.0682 099	0.00772 787	0.0025 826	1.998E- 05	5.7873193	5.7968
1240.10 149	128.9788	97.30781	0.56348	0.16255	2	252.22184	6.97816	5.26847	0.0687 504	0.00826 838	0.0027 638	2.287E- 05	6.193526	6.27986
1240.08 927	129.46187	97.29089	0.56663	0.16255	2	252.17799	7.02201	5.31233	0.0693 227	0.00884 069	0.0029 556	2.616E- 05	6.6238315	6.76293
1240.08 19	129.94494	97.27166	0.56998	0.16255	2	252.12814	7.07186	5.36217	0.0699 731	0.00949 112	0.0031 738	3.015E- 05	7.1131397	7.246
1240.07 037	130.428	97.25441	0.57341	0.16256	2	252.08343	7.11657	5.40689	0.0705 566	0.01007 459	0.0033 695	3.398E- 05	7.552298	7.72906
1240.06 085	130.91107	97.23797	0.57728	0.16256	2	252.04082	7.15918	5.44950	0.0711 127	0.01063 065	0.0035 562	3.785E- 05	7.9710387	8.21213
1240.04 17	131.39414	97.22042	0.58112	0.16257	2	251.99533	7.20467	5.49499	0.0717 063	0.01122 426	0.0037 555	4.221E- 05	8.4182717	8.6952
1240.02 527	131.8772	97.20504	0.58343	0.16257	2	251.95546	7.24454	5.53485	0.0722 265	0.01174 448	0.0039 303	4.622E- 05	8.8103926	9.17826
1240.01 445	132.36027	97.18855	0.58625	0.16258	2	251.91272	7.28728	5.57760	0.0727 842	0.01230 224	0.0041 177	5.073E- 05	9.2310073	9.66133
1240.01 952	132.84334	97.17135	0.59015	0.16257	2	251.86814	7.33186	5.62218	0.0733 66	0.01288 401	0.0043 132	5.565E- 05	9.6699461	10.1444
1240.01 626	133.3264	97.15456	0.59348	0.16258	2	251.82462	7.37538	5.66570	0.0739 339	0.01345 191	0.0045 042	6.068E- 05	10.098633	10.62746
1240.00 963	133.80947	97.13568	0.59628	0.16258	2	251.77568	7.42432	5.71463	0.0745 725	0.01409 051	0.0047 191	6.66E- 05	10.580931	11.11053
1240.00 863	134.29254	97.11899	0.60021	0.16258	2	251.73242	7.46758	5.75789	0.0751 37	0.01465 504	0.0049 091	7.206E- 05	11.007505	11.5936
1240.00 461	134.7756	97.10296	0.60367	0.16258	2	251.69087	7.50913	5.79944	0.0756 792	0.01519 723	0.0050 916	7.751E- 05	11.417404	12.07666
1240.00 61	135.25867	97.08475	0.60724	0.16258	2	251.64367	7.55633	5.84664	0.0762 952	0.01581 317	0.0052 991	8.394E- 05	11.883279	12.55973
1240.00 272	135.74174	97.06594	0.61024	0.16258	2	251.59492	7.60508	5.89540	0.0769 314	0.01644 94	0.0055 135	9.086E- 05	12.364762	13.0428
1239.98 877	136.2248	97.04805	0.61306	0.16258	2	251.54855	7.65145	5.94177	0.0775 365	0.01705 451	0.0057 175	9.769E- 05	12.82294	13.52586
1239.99 154	136.70787	97.03234	0.61654	0.16258	2	251.50783	7.69217	5.98249	0.0780 679	0.01758 589	0.0058 967	0.00010 39	13.225483	14.00893
1240.00	137.19094	97.0153	0.61999	0.16258	2	251.46366	7.73634	6.02666	0.0786	0.01816	0.0060	0.00011	13.662313	14.492

089									442	225	911	09		
1239.99 569	137.674	96.99787	0.62356	0.16258	2	251.41848	7.78152	6.07184	0.0792 338	0.01875 18	0.0062 901	0.00011 82	14.109365	14.97506
1240.00 514	138.15707	96.97998	0.62661	0.16258	2	251.37211	7.82789	6.11821	0.0798 389	0.01935 691	0.0064 944	0.00012 6	14.56845	15.45813
1240.00 413	138.64014	96.96068	0.63002	0.16258	2	251.32208	7.87792	6.16823	0.0804 917	0.02000 972	0.0067 149	0.00013 47	15.063987	15.9412
1239.99 48	139.1232	96.94147	0.633	0.16258	2	251.27229	7.92771	6.21803	0.0811 415	0.02065 948	0.0069 345	0.00014 36	15.55749	16.42426
1240.00 244	139.60627	96.92464	0.6355	0.16258	2	251.22867	7.97133	6.26165	0.0817 107	0.02122 874	0.0071 269	0.00015 17	15.990077	16.90733
1239.99 845	140.08934	96.90739	0.63926	0.16258	2	251.18395	8.01605	6.30636	0.0822 942	0.02181 22	0.0073 242	0.00016 01	16.43368	17.3904
1239.99 321	140.5724	96.88973	0.64276	0.16258	2	251.13818	8.06182	6.35214	0.0828 915	0.02240 953	0.0075 263	0.00016 91	16.888058	17.87346
1239.98 625	141.05547	96.87365	0.64563	0.16258	2	251.09650	8.10350	6.39382	0.0834 354	0.02295 342	0.0077 104	0.00017 74	17.301988	18.35653
1239.99 953	141.53854	96.85506	0.64889	0.16258	2	251.04832	8.15168	6.44200	0.0840 642	0.02358 221	0.0079 234	0.00018 73	17.780772	18.8396
1239.98 422	142.0216	96.83641	0.65222	0.16259	2	250.99997	8.20003	6.49034	0.0846 95	0.02421 303	0.0081 37	0.00019 76	18.261362	19.32266
1239.99 641	142.50467	96.81939	0.65537	0.16258	2	250.95586	8.24414	6.53446	0.0852 707	0.02478 871	0.0083 321	0.00020 71	18.700177	19.80573
1239.99 57	142.98774	96.80161	0.6586	0.16258	2	250.90977	8.29023	6.58054	0.0858 721	0.02539 011	0.0085 36	0.00021 73	19.158821	20.2888
1239.99 875	143.4708	96.78448	0.66172	0.16258	2	250.86537	8.33463	6.62494	0.0864 515	0.02596 951	0.0087 325	0.00022 74	19.600922	20.77186
1239.99 898	143.95387	96.76613	0.66539	0.16258	2	250.81781	8.38219	6.67251	0.0870 722	0.02659 018	0.0089 431	0.00023 85	20.074756	21.25493
1240.00 356	144.43694	96.74864	0.66839	0.16258	2	250.77247	8.42753	6.71784	0.0876 638	0.02718 176	0.0091 439	0.00024 93	20.52662	21.738
1239.99 356	144.92	96.731	0.67167	0.16258	2	250.72675	8.47325	6.76356	0.0882 604	0.02777 842	0.0093 466	0.00026 04	20.982594	22.22106
1239.99 194	145.40307	96.71372	0.67414	0.16258	2	250.68196	8.51804	6.80835	0.0888 449	0.02836 29	0.0095 451	0.00027 16	21.429491	22.70413
1239.99 59	145.88614	96.69613	0.67745	0.16258	2	250.63637	8.56363	6.85395	0.0894 399	0.02895 786	0.0097 473	0.00028 32	21.884637	23.1872
1239.99 592	146.3692	96.6781	0.68109	0.16258	2	250.58964	8.61036	6.90068	0.0900 497	0.02956 771	0.0099 547	0.00029 53	22.351413	23.67026
1239.98 976	146.85227	96.66098	0.68441	0.16258	2	250.54526	8.65474	6.94506	0.0906 288	0.03014 678	0.0101 516	0.00030 71	22.794858	24.15333
1239.99 314	147.33534	96.64318	0.6872	0.16258	2	250.49912	8.70088	6.99119	0.0912 308	0.03074 885	0.0103 565	0.00031 95	23.256153	24.6364
1239.99 82	147.8184	96.62613	0.69051	0.16258	2	250.45493	8.74507	7.03539	0.0918 075	0.03132 555	0.0105 528	0.00033 17	23.698237	25.11946
1240.00 098	148.30147	96.60713	0.69321	0.16258	2	250.40568	8.79432	7.08464	0.0924 502	0.03196 82	0.0107 717	0.00034 56	24.191143	25.60253
1239.99 284	148.78454	96.58871	0.69645	0.16258	2	250.35794	8.84206	7.13238	0.0930 732	0.03259 124	0.0109 84	0.00035 93	24.669265	26.0856
1240.00 554	149.2676	96.57217	0.69914	0.16258	2	250.31506	8.88494	7.17525	0.0936 327	0.03315 069	0.0111 746	0.00037 18	25.09881	26.56866
1240.00 32	149.75067	96.55608	0.70302	0.16258	2	250.27336	8.92664	7.21696	0.0941 769	0.03369 492	0.0113 602	0.00038 42	25.516868	27.05173
1239.99 829	150.23374	96.53834	0.70601	0.16258	2	250.22738	8.97262	7.26294	0.0947 77	0.03429 496	0.0115 649	0.00039 81	25.978028	27.5348
1239.99 56	150.7168	96.52174	0.70921	0.16258	2	250.18435	9.01565	7.30597	0.0953 384	0.03485 644	0.0117 565	0.00041 14	26.40977	28.01786
1239.99 401	151.19987	96.50498	0.71271	0.16258	2	250.14091	9.05909	7.34941	0.0959 053	0.03542 333	0.0119 5	0.00042 5	26.845888	28.50093
1239.99 518	151.68294	96.48703	0.71501	0.16258	2	250.09438	9.10562	7.39594	0.0965 125	0.03603 047	0.0121 574	0.00043 98	27.313211	28.984
1240.00 002	152.166	96.47058	0.71814	0.16258	2	250.05174	9.14826	7.43857	0.0970 689	0.03658 687	0.0123 475	0.00045 36	27.741698	29.46706
1239.99 426	152.64907	96.45307	0.72161	0.16258	2	250.00636	9.19364	7.48396	0.0976 611	0.03717 913	0.0125 499	0.00046 85	28.198025	29.95013
1239.99 293	153.13214	96.4349	0.72534	0.16258	2	249.95926	9.24074	7.53106	0.0982 757	0.03779 372	0.0127 6	0.00048 43	28.671802	30.4332

1240.00 19	153.6152	96.41929	0.72867	0.16258	2	249.91880	9.28120	7.57152	0.0988 037	0.03832 171	0.0129 406	0.00049 8	29.07903	30.91626
1240.00 364	154.09827	96.40166	0.73162	0.16258	2	249.87310	9.32690	7.61721	0.0994	0.03891 803	0.0131 447	0.00051 38	29.539181	31.39933
1239.99 873	154.58134	96.38517	0.73516	0.16258	2	249.83036	9.36964	7.65996	0.0999 578	0.03947 578	0.0133 356	0.00052 88	29.969795	31.8824
1239.99 731	155.0644	96.36758	0.73759	0.16258	2	249.78477	9.41523	7.70555	0.1005 527	0.04007 075	0.0135 394	0.00054 5	30.429365	32.36546
1240.00 536	155.54747	96.34958	0.74069	0.16258	2	249.73811	9.46189	7.75221	0.1011 616	0.04067 958	0.0137 48	0.00056 18	30.899895	32.84853
1240.00 359	156.03054	96.33252	0.74487	0.16258	2	249.69389	9.50611	7.79642	0.1017 386	0.04125 662	0.0139 458	0.00057 8	31.346084	33.3316
1240.00 071	156.5136	96.31463	0.74717	0.16258	2	249.64752	9.55248	7.84280	0.1023 437	0.04186 173	0.0141 533	0.00059 53	31.814223	33.81466
1239.99 391	156.99667	96.29825	0.7503	0.16258	2	249.60506	9.59494	7.88525	0.1028 978	0.04241 577	0.0143 433	0.00061 13	32.243066	34.29773
1240.00 16	157.47974	96.28055	0.75384	0.16258	2	249.55919	9.64081	7.93113	0.1034 965	0.04301 445	0.0145 488	0.00062 88	32.706703	34.7808
1239.99 562	157.9628	96.26327	0.75656	0.16258	2	249.51440	9.68560	7.97592	0.1040 809	0.04359 893	0.0147 495	0.00064 62	33.159572	35.26386
1239.99 816	158.44587	96.24708	0.75951	0.16258	2	249.47243	9.72757	8.01789	0.1046 285	0.04414 654	0.0149 375	0.00066 27	33.584086	35.74693
1240.00 426	158.92894	96.22854	0.76278	0.16258	2	249.42438	9.77562	8.06594	0.1052 556	0.04477 364	0.0151 53	0.00068 19	34.070469	36.23
1239.99 711	159.412	96.21132	0.76553	0.16258	2	249.37974	9.82026	8.11058	0.1058 381	0.04535 609	0.0153 532	0.00069 99	34.522462	36.71306
1240.00 115	159.89507	96.19423	0.76837	0.16258	2	249.33544	9.86456	8.15487	0.1064 161	0.04593 414	0.0155 52	0.00071 81	34.971272	37.19613
1239.98 973	160.37814	96.1779	0.77234	0.16258	2	249.29312	9.90688	8.19720	0.1069 685	0.04648 649	0.0157 42	0.00073 56	35.400336	37.6792
1239.98 96	160.8612	96.16085	0.77456	0.16258	2	249.24892	9.95108	8.24139	0.1075 452	0.04706 319	0.0159 405	0.00075 42	35.848541	38.16226
1239.99 733	161.34427	96.14446	0.77805	0.16258	2	249.20644	9.99356	8.28388	0.1080 996	0.04761 757	0.0161 313	0.00077 23	36.279609	38.64533
1240.00 711	161.82734	96.12829	0.78099	0.16258	2	249.16453	10.03547	8.32579	0.1086 465	0.04816 45	0.0163 197	0.00079 03	36.705098	39.1284
1239.99 613	162.3104	96.10891	0.78523	0.16258	2	249.11429	10.08571	8.37602	0.1093 02	0.04882 001	0.0165 456	0.00081 22	37.215322	39.61146
1240.00 384	162.79347	96.09245	0.78748	0.16258	2	249.07163	10.12837	8.41869	0.1098 588	0.04937 675	0.0167 375	0.00083 11	37.648902	40.09453
1240.00 182	163.27654	96.07695	0.78992	0.16258	2	249.03145	10.16855	8.45886	0.1103 83	0.04990 103	0.0169 183	0.00084 9	38.057389	40.5776
1240.00 831	163.7596	96.05992	0.79409	0.16258	2	248.98731	10.21269	8.50300	0.1109 59	0.05047 705	0.0171 17	0.00086 89	38.506414	41.06066
1239.98 73	164.24267	96.04278	0.79798	0.16258	2	248.94289	10.25711	8.54743	0.1115 388	0.05105 679	0.0173 171	0.00088 93	38.958571	41.54373
1239.99 295	164.72574	96.02728	0.80047	0.16258	2	248.90271	10.29729	8.58761	0.1120 631	0.05158 107	0.0174 981	0.00090 78	39.367663	42.0268
1239.99 002	165.2088	96.00789	0.80341	0.16258	2	248.85245	10.34755	8.63787	0.1127 189	0.05223 691	0.0177 246	0.00093 13	39.87969	42.50986
1239.99 096	165.69187	95.99079	0.80599	0.16258	2	248.80813	10.39187	8.68219	0.1132 973	0.05281 53	0.0179 245	0.00095 23	40.331493	42.99293
1239.99 196	166.17494	95.97448	0.80911	0.16258	2	248.76585	10.43415	8.72446	0.1138 49	0.05336 697	0.0181 152	0.00097 26	40.762637	43.476
1240.00 105	166.658	95.95816	0.81328	0.16258	2	248.72355	10.47645	8.76677	0.1144 01	0.05391 898	0.0183 061	0.00099 31	41.194256	43.95906
1240.00 302	167.14107	95.93953	0.81579	0.16258	2	248.67526	10.52474	8.81506	0.1150 311	0.05454 912	0.0185 241	0.00101 67	41.687226	44.44213
1239.99 89	167.62414	95.92326	0.81888	0.16258	2	248.63309	10.56691	8.85723	0.1155 814	0.05509 944	0.0187 145	0.00103 76	42.117973	44.9252
1239.99 605	168.1072	95.90693	0.82229	0.16258	2	248.59076	10.60924	8.89955	0.1161 338	0.05565 179	0.0189 058	0.00105 88	42.550519	45.40826
1240.00 212	168.59027	95.88979	0.82489	0.16258	2	248.54634	10.65366	8.94398	0.1167 135	0.05623 153	0.0191 066	0.00108 12	43.004748	45.89133
1240.00 178	169.07334	95.87119	0.82851	0.16258	2	248.49812	10.70188	8.99219	0.1173 427	0.05686 066	0.0193 246	0.00110 59	43.497932	46.3744
1240.00	169.5564	95.85495	0.83172	0.16258	2	248.45603	10.74397	9.03429	0.1178	0.05740	0.0195	0.00112	43.928765	46.85746

139									92	996	15	76		
1240.01 203	170.03947	95.83772	0.83443	0.16258	2	248.41137	10.78863	9.07895	0.1184 747	0.05799 275	0.0197 171	0.00115 1	44.386091	47.34053
1240.00 112	170.52254	95.81921	0.83773	0.16258	2	248.36339	10.83661	9.12692	0.1191 008	0.05861 883	0.0199 343	0.00117 63	44.877656	47.8236
1239.99 286	171.00561	95.80365	0.84084	0.16258	2	248.32306	10.87694	9.16726	0.1196 271	0.05914 513	0.0201 17	0.00119 78	45.291089	48.30667
1239.99 782	171.48867	95.78492	0.84356	0.16258	2	248.27451	10.92549	9.21580	0.1202 607	0.05977 866	0.0203 37	0.00122 4	45.789006	48.78973
1240.00 818	171.97174	95.76802	0.84705	0.16258	2	248.23071	10.96929	9.25961	0.1208 323	0.06035 028	0.0205 356	0.00124 78	46.238516	49.2728
1240.00 401	172.45481	95.75156	0.84942	0.16258	2	248.18804	11.01196	9.30227	0.1213 89	0.06090 703	0.0207 291	0.00127 13	46.676541	49.75587
1240.00 548	172.93787	95.73387	0.85281	0.16258	2	248.14219	11.05781	9.34813	0.1219 874	0.06150 537	0.0209 371	0.00129 67	47.147541	50.23893
1239.99 544	173.42094	95.71814	0.85545	0.16258	2	248.10142	11.09858	9.38890	0.1225 194	0.06203 743	0.0211 221	0.00131 96	47.566566	50.722
1239.99 463	173.90401	95.69872	0.85935	0.16258	2	248.05108	11.14892	9.43923	0.1231 763	0.06269 429	0.0213 507	0.00134 81	48.084161	51.20507
1239.99 001	174.38707	95.68265	0.86178	0.16258	2	248.00943	11.19057	9.48089	0.1237 198	0.06323 784	0.0215 399	0.00137 19	48.512698	51.68813
1239.99 57	174.87014	95.6663	0.86641	0.16258	2	247.96705	11.23295	9.52327	0.1242 729	0.06379 086	0.0217 325	0.00139 64	48.948915	52.1712
1239.99 798	175.35321	95.64988	0.86875	0.16258	2	247.92449	11.27551	9.56583	0.1248 283	0.06434 625	0.0219 26	0.00142 12	49.387216	52.65427
1239.99 861	175.83627	95.63188	0.87208	0.16258	2	247.87783	11.32217	9.61248	0.1254 371	0.06495 509	0.0221 382	0.00144 86	49.867942	53.13733
1240.00 448	176.31934	95.61419	0.87621	0.16258	2	247.83198	11.36802	9.65834	0.1260 354	0.06555 343	0.0223 468	0.00147 58	50.340643	53.6204
1240.00 064	176.80241	95.59692	0.87902	0.16258	2	247.78722	11.41278	9.70310	0.1266 196	0.06613 757	0.0225 506	0.00150 26	50.802365	54.10347
1239.99 271	177.28547	95.57842	0.88266	0.16258	2	247.73926	11.46074	9.75105	0.1272 453	0.06676 332	0.0227 689	0.00153 17	51.297238	54.58653
1239.99 677	177.76854	95.56235	0.88604	0.16258	2	247.69761	11.50239	9.79271	0.1277 889	0.06730 687	0.0229 587	0.00155 71	51.727334	55.0696
1239.99 895	178.25161	95.54581	0.88927	0.16258	2	247.65474	11.54526	9.83558	0.1283 483	0.06786 632	0.0231 541	0.00158 35	52.170227	55.55267
1239.99 825	178.73467	95.52777	0.89204	0.16258	2	247.60798	11.59202	9.88234	0.1289 585	0.06847 651	0.0233 673	0.00161 26	52.653538	56.03573
1240.00 317	179.21774	95.51025	0.89566	0.16258	2	247.56257	11.63743	9.92775	0.1295 511	0.06906 91	0.0235 744	0.00164 11	53.123171	56.5188
1240.00 661	179.70081	95.49369	0.89805	0.16258	2	247.51964	11.68036	9.97067	0.1301 112	0.06962 923	0.0237 703	0.00166 82	53.567299	57.00187
1239.99 953	180.18387	95.47495	0.90126	0.16258	2	247.47107	11.72893	10.01925	0.1307 451	0.07026 309	0.0239 92	0.00169 92	54.070162	57.48493
1239.99 773	180.66694	95.4572	0.90435	0.16258	2	247.42506	11.77494	10.06525	0.1313 455	0.07086 347	0.0242 022	0.00172 89	54.546723	57.968
1240.00 18	181.15001	95.43938	0.90742	0.16258	2	247.37887	11.82113	10.11144	0.1319 482	0.07146 621	0.0244 132	0.00175 89	55.025422	58.45107
1239.99 928	181.63307	95.42258	0.91059	0.16258	2	247.33533	11.86467	10.15499	0.1325 165	0.07203 446	0.0246 123	0.00178 75	55.476957	58.93413
1240.00 547	182.11614	95.40604	0.91385	0.16258	2	247.29246	11.90754	10.19786	0.1330 759	0.07259 391	0.0248 083	0.00181 58	55.921729	59.4172
1240.00 935	182.59921	95.38803	0.91692	0.16258	2	247.24577	11.95423	10.24454	0.1336 851	0.07320 308	0.0250 219	0.00184 7	56.406285	59.90027
1240.00 331	183.08227	95.37019	0.91967	0.16258	2	247.19953	12.00047	10.29078	0.1342 885	0.07380 65	0.0252 335	0.00187 81	56.886528	60.38333
1239.99 852	183.56534	95.35243	0.92272	0.16258	2	247.15350	12.04650	10.33682	0.1348 892	0.07440 721	0.0254 443	0.00190 93	57.364877	60.8664
1240.00 485	184.04841	95.33559	0.92607	0.16258	2	247.10985	12.09015	10.38047	0.1354 588	0.07497 681	0.0256 443	0.00193 92	57.818684	61.34947
1239.99 338	184.53147	95.31926	0.92952	0.16258	2	247.06752	12.13248	10.42279	0.1360 112	0.07552 915	0.0258 383	0.00196 83	58.258971	61.83253
1239.99 053	185.01454	95.30175	0.93259	0.16258	2	247.02214	12.17786	10.46818	0.1366 034	0.07612 141	0.0260 463	0.00199 99	58.731315	62.3156
1239.99 415	185.49761	95.28455	0.93544	0.16258	2	246.97755	12.22245	10.51276	0.1371 852	0.07670 319	0.0262 508	0.00203 11	59.195542	62.79867

1240.01 06	185.98067	95.26843	0.93831	0.16258	2	246.93577	12.26423	10.55455	0.1377 304	0.07724 843	0.0264 425	0.00206 06	59.630841	63.28173
1240.00 385	186.46374	95.24992	0.94157	0.16258	2	246.88779	12.31221	10.60252	0.1383 565	0.07787 451	0.0266 628	0.00209 48	60.130942	63.7648
1240.00 309	186.94681	95.23258	0.94461	0.16258	2	246.84285	12.35715	10.64747	0.1389 43	0.07846 102	0.0268 692	0.00212 71	60.599689	64.24787
1239.99 892	187.42987	95.21428	0.94792	0.16258	2	246.79541	12.40459	10.69490	0.1395 62	0.07908	0.0270 871	0.00216 14	61.094656	64.73093
1239.99 491	187.91294	95.19832	0.95055	0.16258	2	246.75405	12.44595	10.73627	0.1401 018	0.07961 983	0.0272 772	0.00219 16	61.526558	65.214
1240.01 105	188.39601	95.18169	0.95357	0.16258	2	246.71094	12.48906	10.77938	0.1406 643	0.08018 233	0.0274 754	0.00222 32	61.976815	65.69707
1240.00 149	188.87907	95.16302	0.95734	0.16258	2	246.66255	12.53745	10.82777	0.1412 958	0.08081 382	0.0276 98	0.00225 9	62.482578	66.18013
1240.00 073	189.36214	95.14456	0.96005	0.16258	2	246.61470	12.58530	10.87562	0.1419 202	0.08143 821	0.0279 182	0.00229 48	62.982936	66.6632
1240.00 347	189.84521	95.12772	0.9631	0.16258	2	246.57105	12.62895	10.91927	0.1424 898	0.08200 781	0.0281 192	0.00232 76	63.43963	67.14627
1239.99 778	190.32827	95.10968	0.96651	0.16258	2	246.52429	12.67571	10.96603	0.1431	0.08261 799	0.0283 346	0.00236 31	63.929129	67.62933
1239.98 978	190.81134	95.09263	0.96943	0.16258	2	246.48010	12.71990	11.01022	0.1436 767	0.08319 469	0.0285 382	0.00239 68	64.392014	68.1124
1239.99 46	191.29441	95.07345	0.97221	0.16258	2	246.43038	12.76962	11.05993	0.1443 254	0.08384 344	0.0287 674	0.00243 51	64.913014	68.59547
1240.00 63	191.77747	95.05697	0.97629	0.16258	2	246.38767	12.81233	11.10265	0.1448 829	0.08440 086	0.0289 645	0.00246 82	65.360917	69.07853
1240.00 709	192.26054	95.04062	0.97958	0.16258	2	246.34529	12.85471	11.14503	0.1454 359	0.08495 388	0.0291 6	0.00250 13	65.80551	69.5616
1240.00 245	192.74361	95.02253	0.98208	0.16258	2	246.29840	12.90160	11.19192	0.1460 478	0.08556 576	0.0293 764	0.00253 82	66.297678	70.04467
1240.00 788	193.22667	95.00357	0.98563	0.16258	2	246.24925	12.95075	11.24106	0.1466 891	0.08620 706	0.0296 034	0.00257 72	66.813809	70.52773
1240.00 026	193.70974	94.98525	0.98872	0.16258	2	246.20177	12.99823	11.28855	0.1473 087	0.08682 672	0.0298 228	0.00261 51	67.312804	71.0108
1239.99 878	194.19281	94.96632	0.99182	0.16258	2	246.15270	13.04730	11.33762	0.1479 49	0.08746 701	0.0300 496	0.00265 47	67.828708	71.49387
1240.00 125	194.67587	94.94993	0.99533	0.16258	2	246.11022	13.08978	11.38010	0.1485 034	0.08802 138	0.0302 461	0.00268 91	68.275632	71.97693
1239.99 882	195.15894	94.93113	0.99774	0.16258	2	246.06149	13.13851	11.42883	0.1491 393	0.08865 727	0.0304 715	0.00272 9	68.788549	72.46
1239.99 902	195.64201	94.91288	1.00153	0.16258	2	246.01418	13.18582	11.47613	0.1497 566	0.08927 456	0.0306 905	0.00276 79	69.286745	72.94307
1240.00 108	196.12507	94.89772	1.00513	0.16258	2	245.97489	13.22511	11.51543	0.1502 693	0.08978 734	0.0308 724	0.00280 05	69.700801	73.42613
1239.99 644	196.60814	94.8789	1.00785	0.16258	2	245.92611	13.27389	11.56421	0.1509 059	0.09042 39	0.0310 984	0.00284 12	70.21509	73.9092
1239.99 237	197.09121	94.86098	1.0113	0.16258	2	245.87966	13.32034	11.61066	0.1515 12	0.09103 003	0.0313 137	0.00288 02	70.705062	74.39227
1239.99 658	197.57427	94.8438	1.01449	0.16258	2	245.83513	13.36487	11.65519	0.1520 931	0.09161 113	0.0315 201	0.00291 79	71.175056	74.87533
1240.00 105	198.05734	94.8255	1.01742	0.16258	2	245.78770	13.41230	11.70262	0.1527 121	0.09223 011	0.0317 401	0.00295 84	71.675963	75.3584
1240.00 078	198.54041	94.80682	1.02048	0.16258	2	245.73928	13.46072	11.75104	0.1533 439	0.09286 194	0.0319 648	0.00299 99	72.187563	75.84147
1240.00 762	199.02347	94.78819	1.02391	0.16258	2	245.69099	13.50901	11.79933	0.1539 741	0.09349 208	0.0321 89	0.00304 17	72.698088	76.32453
1240.00 139	199.50654	94.76955	1.02679	0.16258	2	245.64267	13.55733	11.84764	0.1546 046	0.09412 256	0.0324 135	0.00308 38	73.209181	76.8076
1239.99 381	199.98961	94.75092	1.02963	0.16258	2	245.59438	13.60562	11.89593	0.1552 347	0.09475 27	0.0326 379	0.00312 62	73.720294	77.29067
1240.00 311	200.47267	94.73228	1.03318	0.16258	2	245.54607	13.65393	11.94425	0.1558 652	0.09538 318	0.0328 625	0.00316 89	74.231977	77.77373
1239.99 736	200.95574	94.71364	1.03686	0.16258	2	245.49775	13.70225	11.99256	0.1564 957	0.09601 366	0.0330 872	0.00321 19	74.743955	78.2568
1239.99 409	201.43881	94.69503	1.03876	0.16258	2	245.44952	13.75048	12.04080	0.1571 251	0.09664 313	0.0333 117	0.00325 51	75.255403	78.73987
1240.00	201.92187	94.67629	1.04202	0.16258	2	245.40094	13.79906	12.08937	0.1577	0.09727	0.0335	0.00329	75.770722	79.22293



749									59	699	379	89		
1240.01 184	202.40494	94.65812	1.04608	0.16258	2	245.35385	13.84615	12.13647	0.1583 736	0.09789 157	0.0337 573	0.00334 17	76.270654	79.706
1240.00 363	202.88801	94.6398	1.04941	0.16258	2	245.30636	13.89364	12.18396	0.1589 932	0.09851 123	0.0339 785	0.00338 52	76.774997	80.18907
1240.01 18	203.37107	94.6192	1.05238	0.16258	2	245.25297	13.94703	12.23735	0.1596 9	0.09920 8	0.0342 275	0.00343 44	77.342451	80.67213
1240.01 029	203.85414	94.59934	1.05516	0.16258	2	245.20149	13.99851	12.28883	0.1603 617	0.09987 975	0.0344 676	0.00348 22	77.889864	81.1552
1239.99 548	204.33721	94.58067	1.05844	0.16258	2	245.15310	14.04690	12.33722	0.1609 932	0.10051 124	0.0346 935	0.00352 74	78.404784	81.63827
1239.99 493	204.82027	94.56073	1.06168	0.16258	2	245.10141	14.09859	12.38890	0.1616 677	0.10118 57	0.0349 348	0.00357 6	78.955062	82.12133
1240.00 289	205.30334	94.54314	1.06454	0.16258	2	245.05582	14.14418	12.43450	0.1622 627	0.10178 066	0.0351 478	0.00361 93	79.44077	82.6044
1239.99 451	205.78641	94.52345	1.06766	0.16258	2	245.00478	14.19522	12.48553	0.1629 287	0.10244 665	0.0353 863	0.00366 8	79.984781	83.08747
1240.00 216	206.26947	94.50314	1.07035	0.16258	2	244.95214	14.24786	12.53818	0.1636 156	0.10313 362	0.0356 325	0.00371 85	80.546271	83.57053
1240.00 771	206.75254	94.4863	1.07381	0.16258	2	244.90849	14.29151	12.58183	0.1641 852	0.10370 322	0.0358 367	0.00376 08	81.012099	84.0536
1239.99 187	207.23561	94.46573	1.0772	0.16258	2	244.85517	14.34483	12.63514	0.1648 81	0.10439 898	0.0360 862	0.00381 27	81.581438	84.53667
1240.00 371	207.71867	94.44597	1.08053	0.16258	2	244.80395	14.39605	12.68636	0.1655 493	0.10506 734	0.0363 261	0.00386 29	82.128702	85.01973
1240.00 104	208.20174	94.42774	1.08413	0.16258	2	244.75670	14.44330	12.73361	0.1661 66	0.10568 395	0.0365 474	0.00390 95	82.633891	85.5028
1239.99 37	208.68481	94.40782	1.08716	0.16258	2	244.70507	14.49493	12.78525	0.1668 397	0.10635 773	0.0367 894	0.00396 08	83.186242	85.98587
1240.00 504	209.16787	94.38971	1.09038	0.16258	2	244.65813	14.54187	12.83219	0.1674 523	0.10697 028	0.0370 096	0.00400 77	83.688703	86.46893
1240.00 514	209.65094	94.37011	1.09433	0.16258	2	244.60733	14.59267	12.88299	0.1681 152	0.10763 323	0.0372 479	0.00405 89	84.232825	86.952
1239.99 772	210.13401	94.34914	1.09723	0.16258	2	244.55297	14.64703	12.93735	0.1688 245	0.10834 252	0.0375 031	0.00411 39	84.815348	87.43507
1239.99 981	210.61707	94.33001	1.10062	0.16258	2	244.50339	14.69661	12.98693	0.1694 716	0.10898 958	0.0377 359	0.00416 45	85.347092	87.91813
1239.99 334	211.10014	94.31154	1.10457	0.16258	2	244.45551	14.74449	13.03481	0.1700 963	0.10961 43	0.0379 609	0.00421 37	85.860793	88.4012
1239.99 419	211.58321	94.29245	1.10695	0.16258	2	244.40603	14.79397	13.08429	0.1707 42	0.11026 001	0.0381 935	0.00426 48	86.39205	88.88427
1240.00 297	212.06627	94.2726	1.11012	0.16258	2	244.35458	14.84542	13.13574	0.1714 134	0.11093 141	0.0384 355	0.00431 83	86.944795	89.36733
1240.00 516	212.54934	94.25179	1.11373	0.16258	2	244.30064	14.89936	13.18968	0.1721 173	0.11163 529	0.0386 893	0.00437 48	87.524641	89.8504
1240.00 272	213.03241	94.23127	1.11733	0.16258	2	244.24745	14.95255	13.24286	0.1728 114	0.11232 936	0.0389 397	0.00443 08	88.096778	90.33347
1239.99 915	213.51547	94.21115	1.12091	0.16258	2	244.19530	15.00470	13.29502	0.1734 919	0.11300 99	0.0391 854	0.00448 62	88.65812	90.81653
1240.00 108	213.99854	94.19094	1.12435	0.16258	2	244.14292	15.05708	13.34740	0.1741 755	0.11369 348	0.0394 323	0.00454 21	89.22233	91.2996
1240.01 173	214.48161	94.17077	1.12722	0.16258	2	244.09064	15.10936	13.39968	0.1748 577	0.11437 571	0.0396 788	0.00459 83	89.785781	91.78267
1240.01 471	214.96467	94.15053	1.13075	0.16258	2	244.03817	15.16183	13.45214	0.1755 423	0.11506 031	0.0399 263	0.00465 5	90.351547	92.26573
1240.00 029	215.44774	94.1305	1.13358	0.16258	2	243.98626	15.21374	13.50406	0.1762 198	0.11573 781	0.0401 714	0.00471 16	90.911798	92.7488
1240.00 022	215.93081	94.1095	1.13675	0.16258	2	243.93182	15.26818	13.55849	0.1769 301	0.11644 811	0.0404 285	0.00477 12	91.49956	93.23187
1240.00 262	216.41387	94.09022	1.14057	0.16258	2	243.88185	15.31815	13.60847	0.1775 822	0.11710 024	0.0406 646	0.00482 63	92.039524	93.71493
1239.98 891	216.89694	94.07077	1.14349	0.16258	2	243.83144	15.36856	13.65888	0.1782 401	0.11775 812	0.0409 029	0.00488 23	92.584582	94.198
1240.00 024	217.38001	94.04985	1.14685	0.16258	2	243.77721	15.42279	13.71311	0.1789 477	0.11846 571	0.0411 594	0.00494 28	93.171208	94.68107
1240.00 531	217.86307	94.02899	1.15034	0.16258	2	243.72314	15.47686	13.76717	0.1796 533	0.11917 128	0.0414 153	0.00500 36	93.756537	95.16413

1239.99 195	218.34614	94.00731	1.15431	0.16258	2	243.66695	15.53305	13.82337	0.1803 866	0.11990 459	0.0416 814	0.00506 72	94.365285	95.6472
1240.01 02	218.82921	93.98664	1.15751	0.16258	2	243.61337	15.58663	13.87695	0.1810 857	0.12060 373	0.0419 352	0.00512 82	94.946061	96.13027
1240.01 097	219.31227	93.96658	1.16157	0.16258	2	243.56138	15.63862	13.92894	0.1817 642	0.12128 224	0.0421 817	0.00518 78	95.510061	96.61333
1239.99 391	219.79534	93.94631	1.16448	0.16258	2	243.50884	15.69116	13.98148	0.1824 499	0.12196 785	0.0424 309	0.00524 84	96.080329	97.0964
1239.99 926	220.27841	93.92602	1.16695	0.16258	2	243.45624	15.74376	14.03407	0.1831 361	0.12265 414	0.0426 804	0.00530 94	96.651527	97.57947
1239.99 142	220.76147	93.90206	1.17112	0.16258	2	243.39414	15.80586	14.09618	0.1839 466	0.12346 457	0.0429 753	0.00538 19	97.326514	98.06253
1240.00 117	221.24454	93.88218	1.17402	0.16258	2	243.34261	15.85739	14.14771	0.1846 19	0.12413 699	0.0432 201	0.00544 25	97.886951	98.5456
1240.00 83	221.72761	93.86213	1.17748	0.16258	2	243.29064	15.90936	14.19968	0.1852 972	0.12481 516	0.0434 671	0.00550 39	98.452539	99.02867
1239.99 454	222.21067	93.84087	1.18143	0.16258	2	243.23554	15.96446	14.25478	0.1860 163	0.12553 426	0.0437 291	0.00556 95	99.052653	99.51173
1239.98 151	222.69374	93.82024	1.18399	0.16259	2	243.18206	16.01794	14.30825	0.1867 141	0.12623 205	0.0439 835	0.00563 35	99.635372	99.9948
1239.99 982	223.17681	93.79722	1.18632	0.16258	2	243.12239	16.07761	14.36792	0.1874 927	0.12701 068	0.0442 676	0.00570 54	100.28605	100.4778 7
1239.99 693	223.65987	93.77523	1.19011	0.16258	2	243.06540	16.13460	14.42492	0.1882 365	0.12775 447	0.0445 391	0.00577 45	100.90806	100.9609 3
1240.00 691	224.14294	93.75219	1.19377	0.16258	2	243.00568	16.19432	14.48464	0.1890 158	0.12853 378	0.0448 237	0.00584 74	101.56024	101.444
1240.00 13	224.62601	93.73012	1.19794	0.16258	2	242.94847	16.25153	14.54185	0.1897 623	0.12928 027	0.0450 966	0.00591 77	102.1854	101.9270 7
1240.00 074	225.10907	93.70784	1.20118	0.16258	2	242.89072	16.30928	14.59960	0.1905 159	0.13003 387	0.0453 721	0.00598 91	102.81697	102.4101 3
1239.99 638	225.59214	93.68525	1.20353	0.16258	2	242.83217	16.36783	14.65815	0.1912 8	0.13079 796	0.0456 517	0.00606 19	103.45778	102.8932
1240.00 843	226.07521	93.66279	1.2068	0.16258	2	242.77395	16.42605	14.71637	0.1920 396	0.13155 764	0.0459 298	0.00613 49	104.09536	103.3762 7
1239.99 46	226.55827	93.63973	1.20999	0.16258	2	242.71418	16.48582	14.77614	0.1928 196	0.13233 763	0.0462 155	0.00621 02	104.75045	103.8593 3
1239.99 892	227.04134	93.61559	1.21343	0.16258	2	242.65161	16.54839	14.83871	0.1936 361	0.13315 414	0.0465 148	0.00628 96	105.43673	104.3424
1240.00 817	227.52441	93.59331	1.21655	0.16258	2	242.59386	16.60614	14.89646	0.1943 897	0.13390 774	0.0467 912	0.00636 34	106.07061	104.8254 7
1240.00 434	228.00747	93.57267	1.22036	0.16258	2	242.54036	16.65964	14.94996	0.1950 879	0.13460 586	0.0470 474	0.00643 21	106.65823	105.3085 3
1240.00 622	228.49054	93.54825	1.22369	0.16258	2	242.47706	16.72294	15.01325	0.1959 138	0.13543 185	0.0473 506	0.00651 39	107.35397	105.7916
1239.99 906	228.97361	93.52462	1.22748	0.16258	2	242.41582	16.78418	15.07450	0.1967 131	0.13623 111	0.0476 443	0.00659 36	108.02773	106.2746 7
1240.00 124	229.45667	93.50135	1.23048	0.16258	2	242.35550	16.84450	15.13482	0.1975 002	0.13701 819	0.0479 337	0.00667 26	108.69171	106.7577 3
1240.01 075	229.93974	93.47874	1.23418	0.16258	2	242.29689	16.90311	15.19342	0.1982 65	0.13778 296	0.0482 15	0.00674 99	109.33734	107.2408
1239.99 597	230.42281	93.45615	1.23793	0.16258	2	242.23834	16.96166	15.25198	0.1990 29	0.13854 704	0.0484 962	0.00682 75	109.98287	107.7238 7
1240.00 474	230.90587	93.43397	1.24168	0.16258	2	242.18085	17.01915	15.30947	0.1997 793	0.13929 726	0.0487 725	0.00690 42	110.61714	108.2069 3
1240.00 228	231.38894	93.4077	1.24502	0.16258	2	242.11276	17.08724	15.37756	0.2006 678	0.14018 582	0.0491	0.00699 57	111.36895	108.69
1240.00 76	231.87201	93.3853	1.2481	0.16258	2	242.05470	17.14530	15.43562	0.2014 255	0.14094 347	0.0493 793	0.00707 42	112.01051	109.1730 7
1240.00 288	232.35507	93.36398	1.25139	0.16258	2	241.99944	17.20056	15.49088	0.2021 466	0.14166 46	0.0496 454	0.00714 93	112.62157	109.6561 3
1239.99 915	232.83814	93.33907	1.25487	0.16258	2	241.93487	17.26513	15.55545	0.2029 892	0.14250 716	0.0499 565	0.00723 76	113.33605	110.1392
1239.99 661	233.32121	93.31796	1.25867	0.16258	2	241.88015	17.31985	15.61016	0.2037 032	0.14322 118	0.0502 202	0.00731 29	113.94199	110.6222 7
1239.99 155	233.80427	93.29344	1.26236	0.16258	2	241.81660	17.38340	15.67372	0.2045 325	0.14405 055	0.0505 268	0.00740 09	114.64633	111.1053 3
1240.00	234.28734	93.2699	1.26565	0.16258	2	241.75558	17.44442	15.73474	0.2053	0.14484	0.0508	0.00748	115.32304	111.5884

307									288	677	213	59		
1240.00 442	234.77041	93.24675	1.26894	0.16258	2	241.69558	17.50442	15.79474	0.2061 118	0.14562 979	0.0511 111	0.00757	115.98904	112.0714 7
1240.00 264	235.25347	93.22194	1.27225	0.16258	2	241.63127	17.56873	15.85905	0.2069 51	0.14646 897	0.0514 219	0.00766 07	116.70336	112.5545 3
1240.01 152	235.73654	93.19783	1.27548	0.16258	2	241.56878	17.63122	15.92154	0.2077 665	0.14728 446	0.0517 241	0.00774 94	117.39807	113.0376
1240.00 789	236.21961	93.17306	1.27901	0.16258	2	241.50457	17.69543	15.98575	0.2086 043	0.14812 229	0.0520 347	0.00784 11	118.11236	113.5206 7
1239.99 433	236.70267	93.14811	1.28293	0.16258	2	241.43990	17.76010	16.05042	0.2094 482	0.14896 619	0.0523 479	0.00793 4	118.83242	114.0037 3
1239.99 952	237.18574	93.12486	1.28553	0.16258	2	241.37964	17.82036	16.11068	0.2102 346	0.14975 26	0.0526 399	0.00802 11	119.50395	114.4868
1240.00 477	237.66881	93.09924	1.28896	0.16258	2	241.31323	17.88677	16.17709	0.2111 012	0.15061 917	0.0529 618	0.00811 78	120.24451	114.9698 7
1240.00 72	238.15187	93.0766	1.29231	0.16258	2	241.25455	17.94545	16.23577	0.2118 67	0.15138 495	0.0532 465	0.00820 36	120.89945	115.4529 3
1239.99 454	238.63494	93.05341	1.29594	0.16258	2	241.19444	18.00556	16.29588	0.2126 513	0.15216 933	0.0535 383	0.00829 21	121.5708	115.936
1239.98 884	239.11801	93.02781	1.2993	0.16258	2	241.12808	18.07192	16.36223	0.2135 172	0.15303 523	0.0538 606	0.00839 04	122.31251	116.4190 7
1239.99 697	239.60107	93.00297	1.30314	0.16258	2	241.06370	18.13630	16.42662	0.2143 574	0.15387 541	0.0541 736	0.00848 64	123.03279	116.9021 3
1239.98 996	240.08414	92.97657	1.3066	0.16258	2	240.99527	18.20473	16.49505	0.2152 504	0.15476 837	0.0545 064	0.00858 9	123.79895	117.3852
1240.00 184	240.56721	92.95246	1.31003	0.16258	2	240.93278	18.26722	16.55754	0.2160 659	0.15558 387	0.0548 106	0.00868 33	124.49922	117.8682 7
1240.00 196	241.05027	92.92763	1.31348	0.16258	2	240.86842	18.33158	16.62190	0.2169 057	0.15642 372	0.0551 241	0.00878 1	125.22098	118.3513 3
1240.00 598	241.53334	92.90123	1.31632	0.16258	2	240.79999	18.40001	16.69033	0.2177 987	0.15731 667	0.0554 576	0.00888 55	125.98903	118.8344

APPENDIX 4: Data for the reactivity of Argentine coke at 1290°C.

Temp./-	Time/ min	Mass/%	DTA/(mW /mg)	Sensit./( $\Delta$ V/mW)	Segm ent	mg change	mg evolved	mg CO evolved	%R\ X	bouyancy			ti(model)	ti(exp)
										%R(adj)	lf(X)	Pf(X)		
1290.485 33	129.42 974	96.87726	0.58248	0.14663	2	250.8152 3	8.08477	6.64480	0.0000 0	0	0	0	0	0
1290.393 1	129.92 375	96.81277	0.58955	0.14666	2	250.6482 6	8.25174	6.81176	0.0005 6	0.003051 9	0.0010 183	3.109E-06	0.343792 2	0.49401
1290.313 34	130.41 776	96.74853	0.59536	0.14668	2	250.4819 4	8.41806	6.97808	0.0027 3	0.010435 18	0.0034 906	3.647E-05	1.180122 6	0.98802
1290.274 72	130.91 176	96.68572	0.60169	0.14669	2	250.3193 3	8.58067	7.14070	0.0048 6	0.016284 75	0.0054 58	8.904E-05	1.847399 2	1.48202
1290.210 73	131.40 577	96.62086	0.60755	0.14671	2	250.1514 1	8.74859	7.30862	0.0070 6	0.021726 03	0.0072 951	0.0001589	2.471849 6	1.97603
1290.174 5	131.89 978	96.55536	0.61442	0.14673	2	249.9818 3	8.91817	7.47820	0.0092 8	0.026837 86	0.0090 272	0.000243	3.061809 6	2.47004
1290.145 95	132.39 378	96.49248	0.61963	0.14674	2	249.8190 3	9.08097	7.64099	0.0114 1	0.031487 47	0.0106 08	0.0003352	3.601240 4	2.96404
1290.113 06	132.88 779	96.4282	0.62542	0.14675	2	249.6526 1	9.24739	7.80741	0.0135 8	0.036040 17	0.0121 607	0.00044	4.132045 7	3.45805
1290.090 36	133.38 18	96.36558	0.63161	0.14675	2	249.4904 9	9.40951	7.96954	0.0157 0	0.040317 88	0.0136 241	0.0005518	4.633167 2	3.95206
1290.075 85	133.87 58	96.30281	0.63694	0.14676	2	249.3279 8	9.57202	8.13205	0.0178 3	0.044475 8	0.0150 507	0.0006727	5.122477 7	4.44606
1290.059 19	134.36 981	96.23959	0.64266	0.14676	2	249.1643 0	9.73570	8.29573	0.0199 7	0.048551 03	0.0164 529	0.0008032	5.604198 8	4.94007
1290.048 01	134.86 382	96.17482	0.64812	0.14677	2	248.9966 1	9.90339	8.46342	0.0221 6	0.052624 44	0.0178 585	0.0009454	6.087836 9	5.43408
1290.038 94	135.35 782	96.11347	0.65366	0.14677	2	248.8377 7	10.06223	8.62225	0.0242 4	0.056398 98	0.0191 646	0.0010878	6.537905 8	5.92808
1290.029 41	135.85 183	96.05124	0.65895	0.14677	2	248.6766 6	10.22334	8.78336	0.0263 5	0.060153 3	0.0204 671	0.0012396	6.987401 8	6.42209
1290.030 96	136.34 584	95.98881	0.66398	0.14677	2	248.5150 3	10.38497	8.94500	0.0284 6	0.063851 73	0.0217 537	0.0013991	7.432010 8	6.9161
1290.021 07	136.83 984	95.92767	0.66928	0.14677	2	248.3567 4	10.54326	9.10329	0.0305 3	0.067413 71	0.0229 96	0.0015621	7.861918 7	7.4101
1290.007 88	137.33 385	95.86494	0.67385	0.14678	2	248.1943 3	10.70567	9.26569	0.0326 6	0.071011 75	0.0242 541	0.0017362	8.297886 5	7.90411
1290.006 53	137.82 786	95.80288	0.67972	0.14678	2	248.0336 6	10.86634	9.42637	0.0347 6	0.074519 4	0.0254 837	0.0019152	8.724563 6	8.39812
1289.999 07	138.32 186	95.73832	0.68574	0.14678	2	247.8665 1	11.03349	9.59351	0.0369 5	0.078117 63	0.0267 483	0.0021081	9.163972	8.89212
1289.996 45	138.81 587	95.67571	0.69047	0.14678	2	247.7044 1	11.19559	9.75561	0.0390 7	0.081561 25	0.0279 616	0.0023018	9.586135 5	9.38613
1290.001 98	139.30 988	95.61482	0.69516	0.14678	2	247.5467 7	11.35323	9.91326	0.0411 3	0.084869 77	0.0291 303	0.0024963	9.993252 6	9.88014
1290.007 06	139.80 388	95.55418	0.6999	0.14678	2	247.3897 7	11.51023	10.07025	0.0431 8	0.088127 48	0.0302 837	0.0026958	10.39557 6	10.37414
1290.005 59	140.29 789	95.49154	0.70531	0.14678	2	247.2276 0	11.67240	10.23243	0.0453 1	0.091455 9	0.0314 65	0.0029078	10.80813 7	10.86815
1289.997 6	140.79 19	95.43033	0.71073	0.14678	2	247.0691 2	11.83088	10.39090	0.0473 8	0.094674 32	0.0326 1	0.0031209	11.20851 5	11.36216
1289.990 29	141.28 59	95.37072	0.71537	0.14678	2	246.9147 9	11.98521	10.54523	0.0494 0	0.097778 02	0.0337 167	0.0033338	11.59598 2	11.85616
1289.993 85	141.77 991	95.31054	0.72066	0.14678	2	246.7589 9	12.14101	10.70104	0.0514 4	0.100882 31	0.0348 262	0.0035541	11.98486 8	12.35017
1290.003 71	142.27 392	95.2494	0.72514	0.14678	2	246.6007 0	12.29930	10.85933	0.0535 1	0.104007 65	0.0359 458	0.0037834	12.37775 6	12.84418
1289.997 26	142.76 792	95.18869	0.73013	0.14678	2	246.4435 2	12.45648	11.01651	0.0555 6	0.107083 95	0.0370 504	0.0040165	12.76582 3	13.33818
1289.996 08	143.26 193	95.12929	0.73582	0.14678	2	246.2897 3	12.61027	11.17029	0.0575 8	0.110068 96	0.0381 247	0.0042496	13.14365 6	13.83219
1290.002 27	143.75 594	95.06596	0.74092	0.14678	2	246.1257 7	12.77423	11.33425	0.0597 2	0.113225 49	0.0392 633	0.0045038	13.54458 1	14.3262
1289.993	144.24	95.00441	0.74659	0.14678	2	245.9664	12.93358	11.49361	0.0618	0.116268	0.0403	0.0047561	13.93246	14.8202

12	994					2			1	73	635		7	
1290.003 61	144.74 395	94.94554	0.75068	0.14678	2	245.8140 0	13.08600	11.64602	0.0638 0	0.119157 73	0.0414 104	0.0050024	14.30192 8	15.31421
1290.004 1	145.23 796	94.88518	0.75566	0.14678	2	245.6577 3	13.24227	11.80229	0.0658 4	0.122098 65	0.0424 784	0.0052599	14.67926 9	15.80822
1289.993 78	145.73 196	94.82235	0.76075	0.14678	2	245.4950 6	13.40494	11.96496	0.0679 7	0.125137 98	0.0435 847	0.0055333	15.07055 9	16.30222
1289.985 15	146.22 597	94.7581	0.7664	0.14679	2	245.3287 2	13.57128	12.13130	0.0701 5	0.128223 74	0.0447 105	0.0058183	15.46921	16.79623
1289.999 14	146.71 998	94.69843	0.77174	0.14678	2	245.1742 4	13.72576	12.28579	0.0721 7	0.131070 12	0.0457 513	0.006088	15.83817 6	17.29024
1290.003 39	147.21 398	94.63562	0.77651	0.14678	2	245.0116 2	13.88838	12.44840	0.0743 0	0.134046 82	0.0468 422	0.006377	16.22531 5	17.78424
1289.994 56	147.70 799	94.57417	0.782	0.14678	2	244.8525 3	14.04747	12.60750	0.0763 8	0.136940 38	0.0479 05	0.0066648	16.60290 5	18.27825
1290.000 53	148.20 2	94.51112	0.78674	0.14678	2	244.6892 9	14.21071	12.77073	0.0785 1	0.139890 75	0.0489 912	0.0069652	16.98919 4	18.77226
1290.004 3	148.69 6	94.45185	0.79165	0.14678	2	244.5358 4	14.36416	12.92418	0.0805 2	0.142647 66	0.0500 084	0.0072524	17.35133 6	19.26626

APPENDIX 5: Data for the reactivity of Argentine coke 1340°C.

Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\bar{t}$ V/mW)	Segment	mg change	mg evolved	mg CO evolved	%R/X	%R(adj)
1340.53098	133.56176	95.65665	0.53855	0.13102	2	248.611633	11.288367	9.970882	0	0
1340.41726	134.06577	95.48934	0.54414	0.13105	2	248.176795	11.723205	10.405720	0.0053669	0.00111851
1340.3314	134.56978	95.32513	0.5511	0.13108	2	247.750013	12.149987	10.832502	0.0109222	0.00281712
1340.26353	135.07378	95.15814	0.55767	0.1311	2	247.316006	12.583994	11.266509	0.0165717	0.00484368
1340.19672	135.57779	94.99253	0.56445	0.13112	2	246.885585	13.014415	11.696929	0.0221744	0.00707306
1340.15315	136.0818	94.82755	0.57272	0.13113	2	246.456802	13.443198	12.125712	0.0277558	0.00947021
1340.1332	136.5858	94.66417	0.58182	0.13114	2	246.032178	13.867822	12.550337	0.0332831	0.01199197
1340.09567	137.08981	94.5008	0.59003	0.13115	2	245.607579	14.292421	12.974936	0.03881	0.0146429
1340.06997	137.59382	94.3377	0.59842	0.13116	2	245.183682	14.716318	13.398833	0.0443278	0.01740522
1340.05225	138.09782	94.17061	0.60776	0.13116	2	244.749415	15.150585	13.833100	0.0499806	0.02034428
1340.04428	138.60183	94.00148	0.6203	0.13117	2	244.309847	15.590153	14.272668	0.0557024	0.02342267
1340.03448	139.10584	93.83155	0.63209	0.13117	2	243.868198	16.031802	14.714316	0.0614513	0.0266128
1340.03302	139.60984	93.65954	0.64279	0.13117	2	243.421144	16.478856	15.161370	0.0672706	0.02993454
1340.02629	140.11385	93.4876	0.65507	0.13117	2	242.974272	16.925728	15.608243	0.0730874	0.0333423
1340.01258	140.61786	93.31179	0.67101	0.13118	2	242.517342	17.382658	16.065173	0.0790352	0.03691195
1340.00695	141.12186	93.13327	0.68433	0.13118	2	242.053369	17.846631	16.529146	0.0850747	0.04062007
1340.01064	141.62587	92.95216	0.69925	0.13118	2	241.582664	18.317336	16.999851	0.0912018	0.04446359
1340.00164	142.12988	92.76607	0.71534	0.13118	2	241.099016	18.800984	17.483499	0.0974974	0.04849433
1340.01165	142.63388	92.57751	0.73163	0.13118	2	240.608948	19.291052	17.973566	0.1038765	0.05265901
1339.9947	143.13789	92.38658	0.7498	0.13118	2	240.112721	19.787279	18.469794	0.1103359	0.05695498
1340.00293	143.6419	92.19193	0.76766	0.13118	2	239.606826	20.293174	18.975689	0.116921	0.06141302
1339.99472	144.1459	91.9907	0.78285	0.13118	2	239.083829	20.816171	19.498686	0.1237288	0.06610162
1340.0018	144.64991	91.78779	0.79855	0.13118	2	238.556466	21.343534	20.026049	0.1305934	0.07090841
1339.99823	145.15392	91.58202	0.81412	0.13118	2	238.021670	21.878330	20.560845	0.1375548	0.07586099
1339.99609	145.65792	91.37548	0.83007	0.13118	2	237.484873	22.415127	21.097642	0.1445422	0.08090831
1339.99791	146.16193	91.16666	0.84577	0.13118	2	236.942149	22.957851	21.640366	0.1516068	0.08608633
1339.99747	146.66594	90.95274	0.86021	0.13118	2	236.386171	23.513829	22.196344	0.1588439	0.0914664
1340.00737	147.16994	90.73745	0.87581	0.13118	2	235.826633	24.073367	22.755882	0.1661273	0.0969557
1339.99509	147.67395	90.51709	0.88854	0.13118	2	235.253917	24.646083	23.328598	0.1735823	0.10264954
1339.99993	148.17796	90.29782	0.89954	0.13118	2	234.684034	25.215966	23.898481	0.1810004	0.10838852
1340.00167	148.68196	90.07594	0.91019	0.13118	2	234.107368	25.792632	24.475147	0.1885068	0.11426809
1339.99916	149.18597	89.85564	0.92077	0.13118	2	233.534808	26.365192	25.047707	0.1959597	0.12017573
1340.01264	149.68998	89.6328	0.93	0.13118	2	232.955647	26.944353	25.626868	0.2034986	0.12622045
1340.00091	150.19398	89.415	0.93868	0.13118	2	232.389585	27.510415	26.192930	0.2108669	0.13219376
1340.0064	150.69799	89.19253	0.94624	0.13118	2	231.811385	28.088615	26.771129	0.2183933	0.13836014
1340.00905	151.202	88.96789	0.9535	0.13118	2	231.227546	28.672454	27.354969	0.225993	0.14465169
1340	151.706	88.74403	0.96158	0.13118	2	230.645734	29.254266	27.936781	0.2335664	0.15098488
1340.00874	152.21001	88.52057	0.9684	0.13118	2	230.064961	29.835039	28.517553	0.2411262	0.15736849
1340.00239	152.71402	88.30138	0.97505	0.13118	2	229.495287	30.404713	29.087228	0.2485416	0.16368875
1339.99471	153.21802	88.07709	0.98142	0.13118	2	228.912357	30.987643	29.670158	0.2561295	0.17021489
1340.00413	153.72203	87.85364	0.98595	0.13118	2	228.331610	31.568390	30.250905	0.263689	0.17677452
1339.98643	154.22604	87.63196	0.99085	0.13118	2	227.755464	32.144536	30.827051	0.2711886	0.1833382
1340.00522	154.73004	87.41323	0.99472	0.13118	2	227.186985	32.713015	31.395530	0.2785885	0.18986813
1339.99799	155.23405	87.19344	0.99874	0.13118	2	226.615751	33.284249	31.966764	0.2860241	0.19648234
1339.99167	155.73806	86.97239	1.00173	0.13118	2	226.041242	33.858758	32.541273	0.2935025	0.20318669

1339.99296	156.24206	86.75509	1.00543	0.13118	2	225.476479	34.423521	33.106036	0.3008539	0.20982746
1339.99837	156.74607	86.53793	1.00898	0.13118	2	224.912080	34.987920	33.670435	0.3082006	0.21651278
1339.99763	157.25008	86.32246	1.01253	0.13118	2	224.352074	35.547926	34.230441	0.3154901	0.22319349
1339.98422	157.75408	86.10722	1.01489	0.13118	2	223.792665	36.107335	34.789850	0.3227719	0.22991346
1339.99672	158.25809	85.89106	1.01654	0.13118	2	223.230865	36.669135	35.351650	0.3300848	0.2367081
1339.99106	158.7621	85.67812	1.02019	0.13118	2	222.677434	37.222566	35.905081	0.3372887	0.24344582
1339.99931	159.2661	85.4686	1.02269	0.13118	2	222.132891	37.767109	36.449624	0.3443769	0.25011761

APPENDIX 6: Data for the reactivity of Argentine at 1390°C.

Temp./-C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\Delta$ V/mW)	Segment	mg change	mg evolved	mg CO evolved	bouyancy				ti(model)	ti(exp)
									%R /X	%R(adj)	lf(X)	Pf(X)		
1387.2570	136.7258	93.2274	0.9469	0.1169	1	242.6265	15.6735	14.1799	0.0000	0.0000	0.0000	0.00000000	0.0000	0.0000
1390.7423	137.2398	92.8122	1.0056	0.1158	2	242.4315	15.8685	14.3749	0.0002	0.0002	0.0001	0.00000001	0.0106	0.5140
1390.7774	137.7538	92.3465	1.1661	0.1158	2	242.4108	15.8892	14.3956	0.0004	0.0004	0.0001	0.00000006	0.0277	1.0280
1390.4393	138.2678	91.9395	1.3327	0.1159	2	242.3819	15.9181	14.4245	0.0008	0.0008	0.0003	0.00000022	0.0514	1.5420
1390.3608	138.7818	91.5014	1.3654	0.1159	2	242.3378	15.9622	14.4686	0.0014	0.0014	0.0005	0.00000065	0.0876	2.0560
1390.2660	139.2958	91.0411	1.4145	0.1160	2	242.2749	16.0251	14.5315	0.0022	0.0022	0.0007	0.000000164	0.1393	2.5700
1390.1924	139.8098	90.5301	1.4570	0.1160	2	242.1830	16.1170	14.6234	0.0034	0.0034	0.0011	0.000000391	0.2149	3.0840
1390.1456	140.3238	90.0441	1.4958	0.1160	2	242.0720	16.2280	14.7345	0.0049	0.0049	0.0016	0.000000794	0.3064	3.5981
1390.1153	140.8378	89.5616	1.5300	0.1160	2	241.9368	16.3632	14.8696	0.0066	0.0066	0.0022	0.000001476	0.4179	4.1120
1390.0872	141.3518	89.0716	1.5595	0.1160	2	241.7724	16.5276	15.0340	0.0088	0.0088	0.0029	0.000002590	0.5537	4.6261
1390.0561	141.8658	88.5935	1.5820	0.1160	2	241.5838	16.7162	15.2226	0.0113	0.0113	0.0038	0.000004252	0.7099	5.1401
1390.0418	142.3798	88.1124	1.6006	0.1160	2	241.3642	16.9358	15.4422	0.0141	0.0141	0.0047	0.000006706	0.8921	5.6541
1390.0360	142.8939	87.5932	1.6147	0.1160	2	241.0919	17.2081	15.7145	0.0177	0.0177	0.0059	0.000010530	1.1187	6.1681
1390.0286	143.4079	87.1370	1.6207	0.1160	2	240.8209	17.4791	15.9855	0.0213	0.0213	0.0071	0.000015198	1.3450	6.6821
1390.0179	143.9219	86.6259	1.6232	0.1160	2	240.4802	17.8198	16.3262	0.0257	0.0257	0.0086	0.000022289	1.6304	7.1961
1390.0219	144.4359	86.1407	1.6211	0.1160	2	240.1191	18.1809	16.6873	0.0304	0.0304	0.0103	0.000031304	1.9341	7.7101
1390.0083	144.9499	85.6671	1.6182	0.1160	2	239.7298	18.5702	17.0766	0.0355	0.0355	0.0120	0.000042760	2.2629	8.2241
1390.0151	145.4639	85.1622	1.6109	0.1160	2	239.2733	19.0267	17.5332	0.0415	0.0415	0.0140	0.000058514	2.6506	8.7381
1390.0112	145.9779	84.7387	1.6015	0.1160	2	238.8561	19.4439	17.9503	0.0470	0.0470	0.0159	0.000075110	3.0066	9.2521
1390.0124	146.4919	84.2888	1.5922	0.1160	2	238.3776	19.9224	18.4288	0.0532	0.0532	0.0181	0.000096753	3.4170	9.7661
1390.0038	147.0059	83.8302	1.5817	0.1160	2	237.8515	20.4485	18.9549	0.0601	0.0601	0.0205	0.000123799	3.8710	10.2801
1390.0100	147.5199	83.3862	1.5708	0.1160	2	237.3041	20.9959	19.5023	0.0673	0.0673	0.0229	0.000155586	4.3463	10.7941
1390.0000	148.0339	82.9456	1.5594	0.1160	2	236.7229	21.5771	20.0835	0.0749	0.0749	0.0256	0.000193446	4.8545	11.3082
1390.0090	148.5479	82.5153	1.5480	0.1160	2	236.1178	22.1822	20.6886	0.0828	0.0828	0.0284	0.000237411	5.3873	11.8222
1390.0006	149.0619	82.0868	1.5377	0.1160	2	235.4777	22.8223	21.3287	0.0912	0.0912	0.0314	0.000289028	5.9552	12.3362
1390.0119	149.5759	81.6736	1.5243	0.1160	2	234.8240	23.4760	21.9824	0.0997	0.0997	0.0344	0.000347231	6.5397	12.8502
1390.0036	150.0899	81.2531	1.5116	0.1160	2	234.1214	24.1786	22.6850	0.1089	0.1089	0.0377	0.000416046	7.1732	13.3642
1390.0071	150.6040	80.8274	1.4981	0.1160	2	233.3710	24.9290	23.4354	0.1188	0.1188	0.0413	0.000496810	7.8559	13.8782
1389.9906	151.1180	80.4675	1.4849	0.1160	2	232.7051	25.5949	24.1013	0.1275	0.1275	0.0444	0.000574845	8.4670	14.3922
1389.9916	151.6320	80.0722	1.4712	0.1160	2	231.9401	26.3599	24.8663	0.1375	0.1375	0.0481	0.000672003	9.1754	14.9062
1390.0018	152.14	79.697	1.4579	0.1160	2	231.181	27.1182	25.6246	0.1474	0.1474	0.0518	0.000776	9.8845	15.4202



	60	5				8			4			346		
1389.9932	152.66 00	79.323 2	1.4443	0.1160	2	230.391 3	27.9087	26.4151	0.157 8	0.1578	0.0556	0.0089	10.6309	15.9342
1390.0073	153.17 40	78.958 2	1.4295	0.1160	2	229.588 9	28.7111	27.2175	0.168 3	0.1683	0.0596	0.0102	11.3965	16.4482
1390.0086	153.68 80	78.601 8	1.4159	0.1160	2	228.774 1	29.5259	28.0323	0.178 9	0.1789	0.0636	0.0116	12.1820	16.9622
1390.0003	154.20 20	78.251 5	1.4002	0.1160	2	227.943 0	30.3570	28.8634	0.189 8	0.1898	0.0678	0.0132	12.9920	17.4762
1390.0094	154.71 60	77.909 4	1.3850	0.1160	2	227.102 2	31.1978	29.7042	0.200 8	0.2008	0.0720	0.0148	13.8206	17.9902
1389.9913	155.23 00	77.578 0	1.3704	0.1160	2	226.259 7	32.0403	30.5467	0.211 8	0.2118	0.0763	0.0166	14.6603	18.5042
1389.9985	155.74 40	77.253 0	1.3563	0.1160	2	225.406 4	32.8936	31.4000	0.223 0	0.2230	0.0807	0.0185	15.5206	19.0183
1390.0043	156.25 80	76.935 4	1.3404	0.1160	2	224.546 3	33.7537	32.2601	0.234 3	0.2343	0.0851	0.0205	16.3979	19.5323
1390.0001	156.77 20	76.627 9	1.3255	0.1160	2	223.688 5	34.6115	33.1179	0.245 5	0.2455	0.0896	0.0227	17.2835	20.0463
1389.9939	157.28 60	76.324 6	1.3099	0.1160	2	222.818 2	35.4818	33.9882	0.256 9	0.2569	0.0942	0.0250	18.1928	20.5603
1389.9985	157.80 00	76.031 6	1.2955	0.1160	2	221.954 3	36.3457	34.8521	0.268 2	0.2682	0.0988	0.0274	19.1066	21.0743
1390.0005	158.31 41	75.748 9	1.2819	0.1160	2	221.098 8	37.2012	35.7076	0.279 4	0.2794	0.1035	0.0299	20.0228	21.5883
1390.0010	158.82 81	75.470 7	1.2683	0.1160	2	220.236 0	38.0640	36.5704	0.290 7	0.2907	0.1082	0.0326	20.9585	22.1023
1390.0062	159.34 21	75.199 9	1.2538	0.1160	2	219.375 5	38.9245	37.4309	0.301 9	0.3019	0.1129	0.0354	21.9035	22.6163
1390.0014	159.85 61	74.938 0	1.2420	0.1160	2	218.524 5	39.7755	38.2819	0.313 1	0.3131	0.1177	0.0383	22.8502	23.1303
1390.0033	160.37 01	74.686 4	1.2308	0.1160	2	217.688 7	40.6113	39.1177	0.324 0	0.3240	0.1224	0.0413	23.7918	23.6443
1390.0011	160.88 41	74.440 1	1.2202	0.1160	2	216.853 2	41.4468	39.9532	0.335 0	0.3350	0.1271	0.0444	24.7452	24.1583
1389.9949	161.39 81	74.202 8	1.2111	0.1160	2	216.032 4	42.2676	40.7740	0.345 7	0.3457	0.1319	0.0476	25.6940	24.6723
1389.9960	161.91 21	73.971 6	1.2018	0.1160	2	215.217 0	43.0830	41.5894	0.356 4	0.3564	0.1366	0.0509	26.6487	25.1863
1389.9959	162.42 61	73.748 7	1.1944	0.1160	2	214.416 8	43.8832	42.3896	0.366 8	0.3668	0.1413	0.0543	27.5978	25.7003
1389.9980	162.94 01	73.533 2	1.1881	0.1160	2	213.629 0	44.6710	43.1774	0.377 2	0.3772	0.1460	0.0577	28.5441	26.2143
1389.9973	163.45 41	73.324 6	1.1821	0.1160	2	212.854 3	45.4457	43.9521	0.387 3	0.3873	0.1507	0.0613	29.4868	26.7284

APPENDIX 7: Data for the reactivity of Springlake anthracite.

Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\Delta$ V/mW)	mg change	mg evolved	CO evolved	%R	%R
891.98845	87.22077	97.71758	6.53E-02	0.25733	253.2839674	5.91603264			
897.12061	87.73383	97.68581	6.31E-02	0.25629	253.2016195	5.99838048	0	0	0
902.24108	88.2469	97.6607	6.60E-02	0.25525	253.1365344	6.0634656	0.06508512	0.0008493	0.0008493
907.40562	88.75996	97.63426	6.83E-02	0.25419	253.0680019	6.13199808	0.1336176	0.0017436	0.0017436
912.53548	89.27302	97.6031	7.28E-02	0.25312	252.9872352	6.2127648	0.21438432	0.0027976	0.0027976
917.6638	89.78609	97.57394	7.38E-02	0.25203	252.9116525	6.28834752	0.28996704	0.0037839	0.0037839
922.79619	90.29915	97.5478	7.69E-02	0.25093	252.8438976	6.3561024	0.35772192	0.0046681	0.0046681
927.9306	90.81221	97.51687	7.89E-02	0.24982	252.763727	6.43627296	0.43789248	0.0057142	0.0057142
933.05433	91.32528	97.48902	8.15E-02	0.2487	252.6915398	6.50846016	0.51007968	0.0066562	0.0066562
938.18194	91.83834	97.45535	8.23E-02	0.24757	252.6042672	6.5957328	0.59735232	0.0077951	0.0077951
943.29992	92.3514	97.42903	8.23E-02	0.24642	252.5360458	6.66395424	0.66557376	0.0086853	0.0086853
948.43261	92.86447	97.40198	8.25E-02	0.24526	252.4659322	6.73406784	0.73568736	0.0096003	0.0096003
953.55647	93.37753	97.37589	8.26E-02	0.24408	252.3983069	6.80169312	0.80331264	0.0104827	0.0104827
958.6966	93.89059	97.34254	8.31E-02	0.24289	252.3118637	6.88813632	0.88975584	0.0116108	0.0116108
963.83313	94.40366	97.30647	8.40E-02	0.24169	252.2183702	6.98162976	0.98324928	0.0128308	0.0128308
968.96295	94.91672	97.28853	8.51E-02	0.24048	252.1718698	7.02813024	1.02974976	0.0134376	0.0134376
974.09786	95.42978	97.26081	8.52E-02	0.23925	252.1000195	7.09998048	1.1016	0.0143752	0.0143752
979.22031	95.94285	97.23593	8.44E-02	0.23802	252.0355306	7.16446944	1.16608896	0.0152168	0.0152168
984.36751	96.45591	97.20933	8.38E-02	0.23676	251.9665834	7.23341664	1.23503616	0.0161165	0.0161165
989.51559	96.96897	97.18828	8.38E-02	0.23549	251.9120218	7.28797824	1.28959776	0.0168285	0.0168285
994.66111	97.48204	97.16486	8.46E-02	0.23421	251.8513171	7.34868288	1.3503024	0.0176206	0.0176206
999.80061	97.9951	97.1435	8.41E-02	0.23293	251.795952	7.404048	1.40566752	0.0183431	0.0183431
1004.93206	98.50816	97.12273	8.34E-02	0.23163	251.7421162	7.45788384	1.45950336	0.0190456	0.0190456
1010.08035	99.02123	97.10408	8.42E-02	0.23031	251.6937754	7.50622464	1.50784416	0.0196765	0.0196765
1015.20895	99.53429	97.08108	8.38E-02	0.22899	251.6341594	7.56584064	1.56746016	0.0204544	0.0204544
1020.32667	100.04735	97.06633	8.46E-02	0.22766	251.5959274	7.60407264	1.60569216	0.0209533	0.0209533
1025.47555	100.56042	97.04859	8.32E-02	0.22631	251.5499453	7.65005472	1.65167424	0.0215533	0.0215533
1030.59602	101.07348	97.03215	8.32E-02	0.22495	251.5073328	7.6926672	1.69428672	0.0221094	0.0221094
1035.73224	101.58654	97.01466	8.20E-02	0.22358	251.4619987	7.73800128	1.7396208	0.022701	0.022701
1040.86289	102.09961	97.00077	8.20E-02	0.2222	251.4259958	7.77400416	1.77562368	0.0231708	0.0231708
1046.00614	102.61267	96.98538	8.13E-02	0.22081	251.386105	7.81389504	1.81551456	0.0236914	0.0236914
1051.12772	103.12573	96.96898	8.04E-02	0.21941	251.3435962	7.85640384	1.85802336	0.0242461	0.0242461
1056.26333	103.6388	96.95138	7.86E-02	0.218	251.297977	7.90202304	1.90364256	0.0248414	0.0248414
1061.39621	104.15186	96.93981	7.71E-02	0.21658	251.2679875	7.93201248	1.933632	0.0252327	0.0252327
1066.52524	104.66492	96.92473	7.61E-02	0.21515	251.2289002	7.97109984	1.97271936	0.0257428	0.0257428
1071.63303	105.17799	96.90818	7.39E-02	0.21371	251.1860026	8.01399744	2.01561696	0.0263026	0.0263026
1076.7838	105.69105	96.89194	7.19E-02	0.21226	251.1439085	8.05609152	2.05771104	0.0268519	0.0268519
1081.91659	106.20411	96.87871	6.99E-02	0.2108	251.1096163	8.09038368	2.0920032	0.0272994	0.0272994
1087.04525	106.71718	96.86491	6.82E-02	0.20933	251.0738467	8.12615328	2.1277728	0.0277661	0.0277661
1092.18053	107.23024	96.84874	6.64E-02	0.20785	251.0319341	8.16806592	2.16968544	0.0283131	0.0283131
1097.30827	107.7433	96.83699	6.35E-02	0.20637	251.0014781	8.19852192	2.20014144	0.0287105	0.0287105
1102.43875	108.25637	96.81552	6.23E-02	0.20487	250.9458278	8.25417216	2.25579168	0.0294367	0.0294367
1107.58304	108.76943	96.80326	6.00E-02	0.20337	250.9140499	8.28595008	2.2875696	0.0298514	0.0298514
1112.70183	109.28249	96.7877	5.81E-02	0.20186	250.8737184	8.3262816	2.32790112	0.0303777	0.0303777
1117.83412	109.79556	96.77273	5.65E-02	0.20034	250.8349162	8.36508384	2.36670336	0.030884	0.030884

1122.97624	110.30862	96.75772	5.38E-02	0.19881	250.7960102	8.40398976	2.40560928	0.0313917	0.0313917
1128.09908	110.82168	96.73835	5.14E-02	0.19728	250.7458032	8.4541968	2.45581632	0.0320469	0.0320469
1133.23675	111.33475	96.72217	4.83E-02	0.19574	250.7038646	8.49613536	2.49775488	0.0325942	0.0325942
1138.41143	111.84781	96.70218	6.84E-02	0.19418	250.6520506	8.54794944	2.54956896	0.0332703	0.0332703
1143.51324	112.36087	96.6844	6.89E-02	0.19263	250.6059648	8.5940352	2.59565472	0.0338717	0.0338717

APPENDIX 8: Data for the reactivity of Springlake anthracite at 1190°C.

Temp./ -C	Time/ min	Mass/%	DTA/(mW /mg)	Sensit./( $\Delta$ V/mW)	Segm ent	mg change	mg evolved	mg CO evolved	%R/X	bouyancy		Pf(X)	ti(model)	ti(exp)
										%R(adj)/X	lf(X)			
1190.2 4758	122.99 213	96.16029	0.63952	0.17823	2	248.9589 9	9.94101	3.81349	0	0	0	0	0	0
1190.2 0877	123.46 518	96.14398	0.64518	0.17825	2	248.9167 6	9.98324	3.85572	0.0372 405	0.000147 53	4.91802E -05	7.25585E -09	0.2577845	0.47305
1190.1 7482	123.93 823	96.12731	0.65049	0.17825	2	248.8736 1	10.02639	3.89888	0.0376 574	0.000564 38	0.000188 163	1.06202E -07	0.9882078	0.9461
1190.1 4703	124.41 127	96.11248	0.65591	0.17826	2	248.8352 1	10.06479	3.93727	0.0380 282	0.000935 22	0.000311 837	2.91666E -07	1.6405748	1.41914
1190.1 2788	124.88 432	96.10052	0.66101	0.17827	2	248.8042 5	10.09575	3.96824	0.0383 273	0.001234 29	0.000411 599	5.08103E -07	2.1684525	1.89219
1190.1 1175	125.35 737	96.08725	0.66584	0.17827	2	248.7698 9	10.13011	4.00259	0.0386 591	0.001566 12	0.000522 312	8.18145E -07	2.7559907	2.36524
1190.0 8487	125.83 041	96.07273	0.67115	0.17828	2	248.7323 0	10.16770	4.04019	0.0390 222	0.001929 2	0.000643 482	1.24167E -06	3.4010933	2.83828
1190.0 6946	126.30 346	96.05825	0.67641	0.17829	2	248.6948 1	10.20519	4.07768	0.0393 843	0.002291 29	0.000764 347	1.75179E -06	4.0467301	3.31133
1190.0 6693	126.77 651	96.04527	0.68088	0.17829	2	248.6612 0	10.23880	4.11128	0.0397 089	0.002615 87	0.000872 717	2.28357E -06	4.6274473	3.78438
1190.0 5067	127.24 955	96.03168	0.68578	0.17829	2	248.6260 2	10.27398	4.14646	0.0400 487	0.002955 7	0.000986 204	2.91588E -06	5.2374449	4.25742
1190.0 3697	127.72 26	96.01876	0.69032	0.1783	2	248.5925 7	10.30743	4.17991	0.0403 718	0.003278 77	0.001094 121	3.58868E -06	5.8192569	4.73047
1190.0 2903	128.19 565	96.00623	0.69526	0.1783	2	248.5601 3	10.33987	4.21235	0.0406 851	0.003592 1	0.001198 802	4.30793E -06	6.3852648	5.20352
1190.0 111	128.66 869	95.99499	0.70022	0.17831	2	248.5310 3	10.36897	4.24146	0.0409 662	0.003873 16	0.001292 724	5.00909E -06	6.8944743	5.67656
1190.0 1638	129.14 174	95.98346	0.70467	0.1783	2	248.5011 8	10.39882	4.27131	0.0412 545	0.004161 48	0.001389 089	5.78334E -06	7.4182707	6.14961
1190.0 1659	129.61 479	95.97071	0.71049	0.1783	2	248.4681 7	10.43183	4.30432	0.0415 733	0.004480 31	0.001495 671	6.7044E -06	7.9991996	6.62266
1189.9 9347	130.08 783	95.95736	0.71715	0.17831	2	248.4336 1	10.46639	4.33888	0.0419 071	0.004814 13	0.001607 293	7.74187E -06	8.6093908	7.0957
1190.0 0332	130.56 088	95.94485	0.72103	0.17831	2	248.4012 2	10.49878	4.37127	0.0422 2	0.005126 96	0.001711 915	8.78192E -06	9.1829756	7.56875
1190.0 0663	131.03 393	95.93165	0.72502	0.17831	2	248.3670 4	10.53296	4.40544	0.0425 5	0.005457 04	0.001822 331	9.95057E -06	9.790073	8.0418
1189.9 968	131.50 697	95.921	0.73033	0.17831	2	248.3394 7	10.56053	4.43302	0.0428 163	0.005723 35	0.001911 434	1.09468E -05	10.281295	8.51484
1189.9 9912	131.98 002	95.90876	0.73582	0.17831	2	248.3077 8	10.59222	4.46470	0.0431 224	0.006029 42	0.002013 86	1.21506E -05	10.847404	8.98789
1190.0 0002	132.45 307	95.89862	0.74002	0.17831	2	248.2815 3	10.61847	4.49096	0.0433 76	0.006282 98	0.002098 728	1.31955E -05	11.317643	9.46094
1189.9 9371	132.92 611	95.88924	0.7454	0.17831	2	248.2572 4	10.64276	4.51524	0.0436 105	0.006517 54	0.002177 249	1.42006E -05	11.753651	9.93398
1190.0 0095	133.39 916	95.87762	0.75088	0.17831	2	248.2271 6	10.67284	4.54533	0.0439 011	0.006808 1	0.002274 538	1.5497E -05	12.295132	10.40703
1190.0 0759	133.87 221	95.86623	0.75664	0.17831	2	248.1976 7	10.70233	4.57481	0.0441 859	0.007092 92	0.002369 919	1.68229E -05	12.827347	10.88008
1189.9 9817	134.34 525	95.85488	0.76209	0.17831	2	248.1682 8	10.73172	4.60420	0.0444 697	0.007376 74	0.002464 984	1.81985E -05	13.359123	11.35312
1189.9 968	134.81 83	95.84428	0.76694	0.17831	2	248.1408 4	10.75916	4.63164	0.0447 348	0.007641 8	0.002553 783	1.95321E -05	13.857051	11.82617
1189.9 9367	135.29 135	95.83357	0.7716	0.17831	2	248.1131 1	10.78689	4.65937	0.0450 026	0.007909 61	0.002643 52	2.09276E -05	14.361411	12.29922
1189.9 9199	135.76 439	95.82303	0.77621	0.17831	2	248.0858 2	10.81418	4.68666	0.0452 662	0.008173 18	0.002731 848	2.23482E -05	14.859009	12.77226
1189.9 9299	136.23 744	95.81392	0.78073	0.17831	2	248.0622 4	10.83776	4.71025	0.0454 94	0.008400 98	0.002808 205	2.36138E -05	15.290089	13.24531
1189.9 8974	136.71 049	95.80307	0.78476	0.17831	2	248.0341 5	10.86585	4.73834	0.0457 653	0.008672 29	0.002899 162	2.51667E -05	15.804708	13.71836
1189.9	137.18	95.79013	0.79054	0.17831	2	248.0006	10.89935	4.77184	0.0460	0.008995	0.003007	2.70836E	16.420166	14.1914

8472	353					5			889	87	66	-05		
1189.9 8646	137.65 658	95.77958	0.79564	0.17831	2	247.9733 3	10.92667	4.79915	0.0463 527	0.009259 68	0.003096 137	2.86988E -05	16.923328	14.66445
1190.0 0496	138.12 963	95.77043	0.80083	0.17831	2	247.9496 4	10.95036	4.82284	0.0465 815	0.009488 49	0.003172 885	3.01377E -05	17.360721	15.1375
1189.9 8597	138.60 267	95.759	0.80662	0.17831	2	247.9200 5	10.97995	4.85243	0.0468 673	0.009774 3	0.003268 775	3.19848E -05	17.908412	15.61054
1190.0 0463	139.07 572	95.74757	0.81132	0.17831	2	247.8904 6	11.00954	4.88203	0.0471 531	0.010060 12	0.003364 682	3.38871E -05	18.457556	16.08359
1190.0 1139	139.54 877	95.73763	0.81634	0.17831	2	247.8647 2	11.03528	4.90776	0.0474 017	0.010308 68	0.003448 102	3.55862E -05	18.936297	16.55664
1189.9 9231	140.02 181	95.72856	0.82141	0.17831	2	247.8412 4	11.05876	4.93124	0.0476 285	0.010535 48	0.003524 233	3.71731E -05	19.374096	17.02968
1189.9 9611	140.49 486	95.71712	0.82644	0.17831	2	247.8116 2	11.08838	4.96086	0.0479 146	0.010821 55	0.003620 274	3.92243E -05	19.927599	17.50273
1189.9 8669	140.96 791	95.70796	0.83153	0.17831	2	247.7879 1	11.11209	4.98458	0.0481 436	0.011050 61	0.003697 187	4.09065E -05	20.37184	17.97578
1190.0 0846	141.44 095	95.69724	0.83568	0.17831	2	247.7601 5	11.13985	5.01233	0.0484 117	0.011318 67	0.003787 214	4.29203E -05	20.892925	18.44882
1190.0 0714	141.91 4	95.68957	0.84092	0.17831	2	247.7403 0	11.15970	5.03219	0.0486 035	0.011510 46	0.003851 637	4.4391E -05	21.26654	18.92187
1190.0 0022	142.38 705	95.6786	0.84677	0.17831	2	247.7119 0	11.18810	5.06059	0.0488 778	0.011784 78	0.003943 792	4.65378E -05	21.802043	19.39492
1189.9 9884	142.86 009	95.66679	0.85175	0.17831	2	247.6813 2	11.21868	5.09116	0.0491 731	0.012080 1	0.004043 023	4.89059E -05	22.380051	19.86796
1189.9 9089	143.33 314	95.65842	0.85682	0.17831	2	247.6596 5	11.24035	5.11283	0.0493 824	0.012289 4	0.004113 362	5.06201E -05	22.79064	20.34101
1190.0 0125	143.80 619	95.64759	0.86151	0.17831	2	247.6316 1	11.26839	5.14087	0.0496 532	0.012560 21	0.004204 389	5.2882E -05	23.323065	20.81406
1190.0 0254	144.27 923	95.64197	0.86581	0.17831	2	247.6170 6	11.28294	5.15542	0.0497 937	0.012700 74	0.004251 632	5.40754E -05	23.599872	21.2871
1189.9 9189	144.75 228	95.63155	0.87063	0.17831	2	247.5900 8	11.30992	5.18240	0.0500 543	0.012961 31	0.004339 237	5.63235E -05	24.114031	21.76015
1189.9 8644	145.22 533	95.62106	0.87613	0.17831	2	247.5629 2	11.33708	5.20956	0.0503 166	0.013223 62	0.004427 446	5.86333E -05	24.63287	22.2332
1189.9 9505	145.69 837	95.61183	0.88118	0.17831	2	247.5390 3	11.36097	5.23346	0.0505 474	0.013454 42	0.004505 073	6.07042E -05	25.090407	22.70624
1190.0 0456	146.17 142	95.60349	0.88612	0.17831	2	247.5174 4	11.38256	5.25505	0.0507 56	0.013662 97	0.004575 224	6.26065E -05	25.504645	23.17929
1189.9 8755	146.64 447	95.59346	0.89118	0.17831	2	247.4914 7	11.40853	5.28102	0.0510 068	0.013913 78	0.004659 605	6.49334E -05	26.003853	23.65234
1189.9 8848	147.11 751	95.58188	0.89625	0.17831	2	247.4614 9	11.43851	5.31100	0.0512 963	0.014203 35	0.004757 043	6.76731E -05	26.581608	24.12538

APPENDIX 9: Data for the reactivity of Springlake anthracite at 1240°C.

Temp./ -C	Time/mi n	Mass/%	DTA/(mW /mg)	Sensit./( $\Delta$ V/mW)	Segm ent	mg change	mg evolved	CO evolved	%R	buoyancy		Pf(X)	ti(model)	ti(exp)
										%R(adj)	lf(X)			
1241.2 4629	122.215 02	95.90075	0.3436	0.16219	2	248.287 0	10.6130	4.2186	0	0	0	0	0	0
1241.3 9752	122.698 08	95.8543	0.47848	0.16214	2	248.166 8	10.7332	4.3389	0.0031 73	0.0031730 18	0.0010 588	3.361E-06	1.771353 6	0.4830 6
1241.0 0456	123.181 15	95.80988	0.61121	0.16226	2	248.051 8	10.8482	4.4539	0.0046 798	0.0046797 66	0.0015 624	7.315E-06	2.614557 1	0.9661 3
1240.8 11	123.664 21	95.76885	0.61599	0.16232	2	247.945 6	10.9544	4.5601	0.0060 715	0.0060715 24	0.0020 28	1.232E-05	3.394588 4	1.4491 9
1240.6 9222	124.147 27	95.72915	0.63207	0.16236	2	247.842 8	11.0572	4.6629	0.0074 182	0.0074181 68	0.0024 789	1.84E-05	4.150414 4	1.9322 5
1240.5 8621	124.630 34	95.6905	0.64023	0.1624	2	247.742 7	11.1573	4.7630	0.0087 292	0.0087291 95	0.0029 182	2.55E-05	4.887272 4	2.4153 2
1240.4 9842	125.113 4	95.65381	0.64566	0.16242	2	247.647 7	11.2523	4.8579	0.0099 737	0.0099737 38	0.0033 357	3.331E-05	5.587698 2	2.8983 8
1240.4 1858	125.596 46	95.61934	0.65086	0.16245	2	247.558 5	11.3415	4.9472	0.0111 43	0.0111429 77	0.0037 282	4.159E-05	6.246574 7	3.3814 4
1240.3 4114	126.079 53	95.58588	0.65646	0.16247	2	247.471 8	11.4282	5.0338	0.0122 78	0.0122779 57	0.0041 095	5.053E-05	6.886917 4	3.8645 1
1240.2 7517	126.562 59	95.55331	0.66221	0.16249	2	247.387 5	11.5125	5.1181	0.0133 827	0.0133827 48	0.0044 81	6.006E-05	7.510959 2	4.3475 7
1240.2 5001	127.045 65	95.52109	0.667	0.1625	2	247.304 1	11.5959	5.2016	0.0144 757	0.0144756 66	0.0048 487	7.03E-05	8.129006 3	4.8306 3
1240.2 0374	127.528 72	95.49148	0.67291	0.16252	2	247.227 4	11.6726	5.2782	0.0154 801	0.0154800 52	0.0051 869	8.043E-05	8.697613 1	5.3137 1
1240.1 5416	128.011 78	95.46204	0.67892	0.16253	2	247.151 2	11.7488	5.3544	0.0164 787	0.0164786 71	0.0055 233	9.118E-05	9.263549 6	5.7967 6
1240.1 2236	128.494 84	95.43206	0.68308	0.16254	2	247.073 6	11.8264	5.4321	0.0174 956	0.0174956 08	0.0058 662	0.0001028	9.840476 8	6.2798 2
1240.1 0609	128.977 91	95.4046	0.68778	0.16255	2	247.002 5	11.8975	5.5032	0.0184 271	0.0184270 64	0.0061 805	0.0001141	10.36945 1	6.7628 9
1240.0 919	129.460 97	95.37604	0.69331	0.16255	2	246.928 6	11.9714	5.5771	0.0193 958	0.0193958 34	0.0065 075	0.0001265	10.92016 4	7.2459 5
1240.0 6536	129.944 03	95.34736	0.6986	0.16256	2	246.854 3	12.0457	5.6513	0.0203 687	0.0203686 73	0.0068 362	0.0001396	11.47375 6	7.7290 1
1240.0 6177	130.427 1	95.31824	0.70349	0.16256	2	246.778 9	12.1211	5.7267	0.0213 564	0.0213564 38	0.0071 701	0.0001535	12.03642 6	8.2120 8
1240.0 4929	130.910 16	95.29101	0.70881	0.16256	2	246.708 4	12.1916	5.7972	0.0222 801	0.0222800 93	0.0074 825	0.0001671	12.56309 5	8.6951 4
1240.0 3269	131.393 22	95.26374	0.714	0.16257	2	246.637 8	12.2622	5.8678	0.0232 051	0.0232051 05	0.0077 956	0.0001814	13.09105 8	9.1782 8
1240.0 2263	131.876 29	95.23634	0.71964	0.16257	2	246.566 9	12.3331	5.9388	0.0241 345	0.0241345 27	0.0081 104	0.0001963	13.62205 5	9.6612 7
1240.0 1955	132.359 35	95.2108	0.72413	0.16257	2	246.500 8	12.3992	6.0049	0.0250 009	0.0250008 56	0.0084 04	0.0002107	14.11747 6	10.144 33
1240.0 2393	132.842 41	95.18347	0.72865	0.16257	2	246.430 0	12.4700	6.0757	0.0259 279	0.0259279 03	0.0087 184	0.0002267	14.64812 6	10.627 39
1240.0 1276	133.325 48	95.15754	0.73457	0.16258	2	246.362 9	12.5371	6.1428	0.0268 075	0.0268074 62	0.0090 169	0.0002424	15.15206 1	11.110 46
1240.0 0025	133.808 54	95.13009	0.73948	0.16258	2	246.291 8	12.6082	6.2139	0.0277 386	0.0277385 79	0.0093 33	0.0002597	15.68605 3	11.593 52
1240.0 0475	134.291 6	95.10492	0.74372	0.16258	2	246.226 6	12.6734	6.2790	0.0285 924	0.0285923 58	0.0096 231	0.000276	16.17615 3	12.076 58
1240.0 0366	134.774 67	95.0805	0.74856	0.16258	2	246.163 4	12.7366	6.3422	0.0294 207	0.0294206 97	0.0099 047	0.0002924	16.65207 3	12.559 65
1240.0 0568	135.257 73	95.05546	0.75423	0.16258	2	246.098 6	12.8014	6.4071	0.0302 701	0.0302700 66	0.0101 936	0.0003096	17.14050 8	13.042 71
1239.9 9624	135.740 79	95.03142	0.75869	0.16258	2	246.036 3	12.8637	6.4693	0.0310 855	0.0310855 14	0.0104 711	0.0003266	17.60985 8	13.525 77
1239.9 9465	136.223 86	95.00488	0.76299	0.16258	2	245.967 6	12.9324	6.5380	0.0319 858	0.0319857 64	0.0107 777	0.000346	18.12847 1	14.008 84
1239.9	136.706	94.98137	0.7684	0.16258	2	245.906	12.9932	6.5989	0.0327	0.0327832	0.0110	0.0003636	18.58829	14.491

9571	92					8			832	35	494		5	9
1239.9 9737	137.189 98	94.95615	0.77396	0.16258	2	245.841 5	13.0585	6.6642	0.0336 387	0.0336387 1	0.0113 41	0.0003829	19.08199 6	14.974 96
1239.9 9568	137.673 05	94.93228	0.77866	0.16258	2	245.779 7	13.1203	6.7260	0.0344 484	0.0344483 92	0.0116 172	0.0004017	19.54968 3	15.458 03
1239.9 969	138.156 11	94.90763	0.78358	0.16258	2	245.715 9	13.1841	6.7898	0.0352 845	0.0352845 33	0.0119 026	0.0004216	20.03307 3	15.941 09
1239.9 9376	138.639 17	94.88447	0.78859	0.16258	2	245.655 9	13.2441	6.8498	0.0360 701	0.0360701 31	0.0121 709	0.0004408	20.48763 5	16.424 15
1239.9 9102	139.122 24	94.86142	0.79306	0.16258	2	245.596 2	13.3038	6.9094	0.0368 52	0.0368519 99	0.0124 381	0.0004603	20.94041 4	16.907 22
1239.9 973	139.605 3	94.83768	0.79716	0.16258	2	245.534 8	13.3652	6.9709	0.0376 573	0.0376572 71	0.0127 134	0.0004808	21.40714 4	17.390 28
1239.9 952	140.088 36	94.81384	0.80172	0.16258	2	245.473 0	13.4270	7.0326	0.0384 659	0.0384659 36	0.0129 9	0.0005018	21.87623 4	17.873 34
1239.9 9503	140.571 43	94.79034	0.80719	0.16258	2	245.412 2	13.4878	7.0935	0.0392 631	0.0392630 67	0.0132 628	0.000523	22.33903 2	18.356 41
1239.9 8567	141.054 49	94.76629	0.81223	0.16258	2	245.349 9	13.5501	7.1557	0.0400 789	0.0400788 55	0.0135 422	0.0005452	22.81306 7	18.839 47
1239.9 8722	141.537 55	94.74381	0.81834	0.16258	2	245.291 7	13.6083	7.2139	0.0408 414	0.0408413 88	0.0138 035	0.0005663	23.25652 9	19.322 53
1239.9 911	142.020 62	94.72175	0.82185	0.16258	2	245.234 6	13.6654	7.2711	0.0415 897	0.0415896 74	0.0140 6	0.0005875	23.69205 6	19.805 6
1239.9 9752	142.503 68	94.69857	0.82693	0.16258	2	245.174 6	13.7254	7.3311	0.0423 76	0.0423759 51	0.0143 297	0.0006101	24.15006 8	20.288 66
1239.9 9053	142.986 74	94.67514	0.83258	0.16258	2	245.113 9	13.7861	7.3917	0.0431 707	0.0431707 08	0.0146 024	0.0006335	24.61341 2	20.771 72
1239.9 9173	143.469 81	94.65238	0.83615	0.16258	2	245.055 0	13.8450	7.4507	0.0439 427	0.0439427 39	0.0148 675	0.0006566	25.06387 7	21.254 79
1239.9 9445	143.952 87	94.62995	0.84119	0.16258	2	244.996 9	13.9031	7.5087	0.0447 036	0.0447035 75	0.0151 289	0.0006797	25.50817 6	21.737 85
1239.9 9437	144.435 93	94.60683	0.8453	0.16258	2	244.937 1	13.9629	7.5686	0.0454 878	0.0454878 17	0.0153 985	0.000704	25.96652 1	22.220 91
1239.9 9142	144.919	94.58341	0.85068	0.16258	2	244.876 4	14.0236	7.6292	0.0462 822	0.0462822 35	0.0156 717	0.0007291	26.43120 2	22.703 98
1239.9 9889	145.402 06	94.56061	0.85556	0.16258	2	244.817 4	14.0826	7.6882	0.0470 556	0.0470556 23	0.0159 379	0.000754	26.88396 1	23.187 04
1239.9 9345	145.885 12	94.53869	0.8598	0.16258	2	244.760 7	14.1393	7.7450	0.0477 992	0.0477991 6	0.0161 939	0.0007782	27.31959 7	23.670 1
1239.9 9192	146.368 19	94.51699	0.86448	0.16258	2	244.704 5	14.1955	7.8012	0.0485 352	0.0485352 35	0.0164 474	0.0008027	27.75120 2	24.153 17

APPENDIX 10: Data for the reactivity of Springlake anthracite at 1290°C.

Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\mu$ V/mW)	mg change	mg evolved	CO evolved	%R	%R(adj)
1289.99697	137.56002	94.03215	0.63681	0.14678	242.6029	15.3971	6.1824	0	0
1289.999	138.05307	93.97403	0.64178	0.14678	242.4530	15.5470	6.3324	0.0006447	0.0030829
1289.99395	138.54611	93.91855	0.64731	0.14678	242.3099	15.6901	6.4755	0.0025172	0.00900591
1289.99968	139.03916	93.8683	0.65162	0.14678	242.1802	15.8198	6.6052	0.0042133	0.0135075
1290.00228	139.53221	93.81302	0.65641	0.14678	242.0376	15.9624	6.7478	0.0060791	0.01802517
1289.99583	140.02525	93.75861	0.6612	0.14678	241.8972	16.1028	6.8882	0.0079155	0.02218719
1290.00248	140.5183	93.7063	0.66566	0.14678	241.7623	16.2377	7.0231	0.0096811	0.02599687
1289.98501	141.01135	93.65021	0.6699	0.14679	241.6175	16.3825	7.1678	0.0115742	0.02992038
1289.99347	141.50439	93.5995	0.67482	0.14678	241.4867	16.5133	7.2987	0.0132857	0.03335067
1289.99885	141.99744	93.54689	0.67907	0.14678	241.3510	16.6490	7.4344	0.0150614	0.03681125
1290.0014	142.49049	93.49487	0.684	0.14678	241.2168	16.7832	7.5686	0.0168172	0.04014837
1289.99353	142.98353	93.4416	0.68922	0.14678	241.0793	16.9207	7.7060	0.0186151	0.04348955
1290.00073	143.47658	93.38706	0.69399	0.14678	240.9386	17.0614	7.8468	0.020456	0.04683984
1289.99603	143.96963	93.33181	0.70012	0.14678	240.7961	17.2039	7.9893	0.0223208	0.05016882
1289.9883	144.46267	93.27793	0.70388	0.14678	240.6571	17.3429	8.1283	0.0241393	0.05335858
1289.99365	144.95572	93.2231	0.70963	0.14678	240.5156	17.4844	8.2698	0.0259899	0.05655244
1289.98917	145.44877	93.16967	0.71539	0.14678	240.3777	17.6223	8.4076	0.0277933	0.05961842
1289.99051	145.94181	93.11448	0.71957	0.14678	240.2354	17.7646	8.5500	0.029656	0.06274121
1289.98833	146.43486	93.0636	0.72447	0.14678	240.1041	17.8959	8.6813	0.0313733	0.06558327
1289.98796	146.92791	93.01054	0.73052	0.14678	239.9672	18.0328	8.8182	0.0331642	0.06851202
1289.99219	147.42095	92.95602	0.73552	0.14678	239.8265	18.1735	8.9588	0.0350043	0.07148647
1289.99651	147.914	92.90291	0.73984	0.14678	239.6895	18.3105	9.0959	0.0367969	0.07435212
1290.00334	148.40705	92.84993	0.74401	0.14678	239.5528	18.4472	9.2326	0.0385851	0.07718126
1290.00725	148.90009	92.79682	0.74974	0.14678	239.4158	18.5842	9.3696	0.0403776	0.07998945
1289.99739	149.39314	92.7414	0.75589	0.14678	239.2728	18.7272	9.5126	0.0422481	0.08289161
1290.00844	149.88619	92.68491	0.76143	0.14678	239.1271	18.8729	9.6583	0.0441548	0.08582176
1290.00281	150.37923	92.63078	0.7656	0.14678	238.9874	19.0126	9.7980	0.0459818	0.08860431
1289.99842	150.87228	92.57421	0.77081	0.14678	238.8415	19.1585	9.9439	0.0478911	0.09148724
1290.00586	151.36533	92.51781	0.77593	0.14678	238.6959	19.3041	10.0894	0.0497947	0.09433722
1289.99432	151.85837	92.46294	0.781	0.14678	238.5544	19.4456	10.2310	0.0516467	0.0970877
1289.99288	152.35142	92.4064	0.78592	0.14678	238.4085	19.5915	10.3769	0.053555	0.0999
1289.99746	152.84447	92.34635	0.79108	0.14678	238.2536	19.7464	10.5318	0.0555818	0.10286362
1289.99956	153.33751	92.29303	0.79625	0.14678	238.1160	19.8840	10.6694	0.0573814	0.10547584
1289.99223	153.83056	92.23793	0.80183	0.14678	237.9739	20.0261	10.8115	0.0592411	0.108157
1289.9982	154.32361	92.17991	0.80638	0.14678	237.8242	20.1758	10.9612	0.0611994	0.11096094
1290.00575	154.81665	92.12169	0.81205	0.14678	237.6740	20.3260	11.1114	0.0631644	0.1137554
1290.00523	155.3097	92.06516	0.81536	0.14678	237.5281	20.4719	11.2573	0.0650724	0.11645107
1289.99403	155.80274	92.00627	0.82249	0.14678	237.3762	20.6238	11.4092	0.0670601	0.11924144
1289.9952	156.29579	91.94817	0.82713	0.14678	237.2263	20.7737	11.5591	0.0690211	0.12197716
1290.00323	156.78884	91.8917	0.83154	0.14678	237.0806	20.9194	11.7048	0.070927	0.12462031
1289.99936	157.28188	91.83487	0.83899	0.14678	236.9340	21.0660	11.8514	0.0728451	0.12726507
1289.99132	157.77493	91.77351	0.84511	0.14678	236.7757	21.2243	12.0097	0.0749161	0.13010406
1289.99041	158.26798	91.71597	0.84888	0.14678	236.6272	21.3728	12.1582	0.0768582	0.13275115
1289.99883	158.76102	91.65983	0.85364	0.14678	236.4824	21.5176	12.3030	0.078753	0.13532013
1290.00243	159.25407	91.5985	0.85806	0.14678	236.3241	21.6759	12.4612	0.080823	0.13811161



1289.99348	159.74712	91.53729	0.86366	0.14678	236.1662	21.8338	12.6192	0.082889	0.14088248
1290.0034	160.24016	91.47843	0.86918	0.14678	236.0143	21.9857	12.7710	0.0848756	0.14353313
1290.00261	160.73321	91.41563	0.87359	0.14678	235.8523	22.1477	12.9330	0.0869952	0.14634669
1289.99756	161.22626	91.35497	0.8788	0.14678	235.6958	22.3042	13.0896	0.0890426	0.14905053
1289.9984	161.7193	91.29321	0.88424	0.14678	235.5365	22.4635	13.2489	0.0911271	0.15178984
1290.00685	162.21235	91.23402	0.88962	0.14678	235.3838	22.6162	13.4016	0.0931249	0.15440265
1289.9979	162.7054	91.17125	0.89472	0.14678	235.2218	22.7782	13.5636	0.0952435	0.15716049

APPENDIX 11: Data for the reactivity of Springlake anthracite at 1340°C.

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Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\nabla$ V/mW)	mg change	mg evolved	CO evolved	%R	%R(adj)
1340.6308	132.30565	93.95457	-2.63007	0.13099	244.56375	15.73625	9.40214	0	0
1341.00875	132.80872	93.71517	1.14889	0.13087	243.94059	16.35941	10.02530	0.0053801	0.005380143
1340.55801	133.31178	93.56273	0.43253	0.13101	243.54379	16.75621	10.42210	0.0105842	0.010584167
1340.47249	133.81484	93.39548	0.61748	0.13103	243.10843	17.19157	10.85745	0.0162938	0.016293777
1340.36494	134.31791	93.23214	0.58657	0.13107	242.68326	17.61674	11.28263	0.0218699	0.021869907
1340.29439	134.82097	93.0645	0.60749	0.13109	242.24689	18.05311	11.71899	0.0275928	0.027592831
1340.21966	135.32403	92.89925	0.61993	0.13111	241.81675	18.48325	12.14914	0.0332342	0.033234165
1340.17863	135.8271	92.73206	0.63129	0.13113	241.38155	18.91845	12.58433	0.0389417	0.038941727
1340.13917	136.33016	92.56216	0.64554	0.13114	240.93930	19.36070	13.02658	0.0447418	0.044741803
1340.10092	136.83322	92.39539	0.66041	0.13115	240.50520	19.79480	13.46069	0.050435	0.050435027
1340.08078	137.33629	92.22454	0.6729	0.13116	240.06048	20.23952	13.90541	0.0562675	0.056267534
1340.05188	137.83935	92.05154	0.68626	0.13116	239.61016	20.68984	14.35573	0.0621734	0.062173439
1340.03838	138.34241	91.87253	0.69929	0.13117	239.14420	21.15580	14.82169	0.0682845	0.068284514
1340.03387	138.84548	91.69434	0.71613	0.13117	238.68037	21.61963	15.28552	0.0743676	0.074367596
1340.02896	139.34854	91.51365	0.73078	0.13117	238.21003	22.08997	15.75585	0.080536	0.080536024
1340.02267	139.8516	91.33161	0.74389	0.13117	237.73618	22.56382	16.22971	0.0867505	0.086750537
1340.01903	140.35467	91.14453	0.75861	0.13117	237.24921	23.05079	16.71667	0.0931371	0.093137108
1340.00506	140.85773	90.95545	0.77446	0.13118	236.75704	23.54296	17.20885	0.099592	0.099591954
1340.00755	141.36079	90.76384	0.78722	0.13118	236.25828	24.04172	17.70761	0.1061332	0.10613317
1340.00265	141.86386	90.56802	0.80093	0.13118	235.74856	24.55144	18.21733	0.1128181	0.112818108
1340.00262	142.36692	90.37219	0.81534	0.13118	235.23881	25.06119	18.72708	0.1195034	0.119503388
1339.99921	142.86998	90.1742	0.82892	0.13118	234.72344	25.57656	19.24244	0.1262624	0.126262406
1339.99545	143.37305	89.97425	0.84103	0.13118	234.20297	26.09703	19.76291	0.1330883	0.133088334
1339.98947	143.87611	89.76792	0.85357	0.13118	233.66590	26.63410	20.29999	0.1401321	0.140132064
1339.99082	144.37917	89.56212	0.86416	0.13118	233.13020	27.16980	20.83569	0.1471577	0.147157701
1339.99322	144.88224	89.35885	0.87494	0.13118	232.60109	27.69891	21.36480	0.154097	0.154096969
1340.002	145.3853	89.15143	0.88623	0.13118	232.06117	28.23883	21.90471	0.1611779	0.161177909
1340.00494	145.88836	88.94469	0.89771	0.13118	231.52303	28.77697	22.44286	0.1682356	0.168235636
1340.00432	146.39143	88.73156	0.90672	0.13118	230.96825	29.33175	22.99764	0.1755115	0.175511506
1339.993	146.89449	88.52207	0.91475	0.13118	230.42295	29.87705	23.54294	0.1826631	0.182663113
1339.99555	147.39755	88.31188	0.92206	0.13118	229.87582	30.42418	24.09006	0.1898386	0.189838616
1340.00262	147.90062	88.10168	0.92996	0.13118	229.32867	30.97133	24.63721	0.1970145	0.197014461
1339.9954	148.40368	87.89064	0.93629	0.13118	228.77934	31.52066	25.18655	0.204219	0.204218982
1340.00119	148.90674	87.67971	0.94253	0.13118	228.23029	32.06971	25.73560	0.2114197	0.211419748
1339.99261	149.40981	87.47004	0.94894	0.13118	227.68451	32.61549	26.28137	0.2185775	0.2185775
1339.9963	149.91287	87.26263	0.95457	0.13118	227.14463	33.15537	26.82126	0.2256581	0.225658099
1339.99253	150.41593	87.0541	0.9597	0.13118	226.60182	33.69818	27.36406	0.2327769	0.232776933
1339.98901	150.919	86.84376	0.96446	0.13118	226.05431	34.24569	27.91158	0.2399576	0.239957558
1339.99634	151.42206	86.6357	0.96947	0.13118	225.51273	34.78727	28.45316	0.2470603	0.247060347
1340.00391	151.92512	86.43052	0.9746	0.13118	224.97864	35.32136	28.98724	0.2540648	0.254064818
1339.99704	152.42819	86.22628	0.97897	0.13118	224.44701	35.85299	29.51888	0.2610372	0.2610372
1340.00007	152.93125	86.02057	0.9818	0.13118	223.91154	36.38846	30.05434	0.2680598	0.268059764
1340.00672	153.43431	85.8158	0.98572	0.13118	223.37853	36.92147	30.58736	0.2750502	0.275050239
1340.00182	153.93738	85.61251	0.98901	0.13118	222.84936	37.45064	31.11652	0.2819902	0.281990189

1340.00394	154.44044	85.41188	0.99291	0.13118	222.32712	37.97288	31.63876	0.2888393	0.288839331
1339.99637	154.9435	85.2129	0.99551	0.13118	221.80918	38.49082	32.15671	0.2956321	0.295632146
1339.99228	155.44657	85.01466	0.9993	0.13118	221.29316	39.00684	32.67273	0.3023997	0.302399698
1339.99852	155.94963	84.81658	1.00347	0.13118	220.77756	39.52244	33.18833	0.3091618	0.309161789
1339.99902	156.45269	84.61972	1.00737	0.13118	220.26513	40.03487	33.70075	0.3158822	0.31588223
1339.99915	156.95576	84.42787	1.01082	0.13118	219.76575	40.53425	34.20014	0.3224316	0.32243164
1339.99507	157.45882	84.23544	1.01363	0.13118	219.26485	41.03515	34.70104	0.3290008	0.329000849
1340.00286	157.96188	84.04394	1.01604	0.13118	218.76638	41.53362	35.19951	0.3355383	0.33553831

APPENDIX 12: Data for the reactivity of Springlake anthracite at 1390°C.

Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\mu$ V/mW)	mg change	mg evolved	CO evolved	%R	%R(adj)
1389.84799	136.98792	91.67852	0.45134	0.11608	237.6307	21.5693	15.5709	0	0
1390.94362	137.50098	91.24361	0.54673	0.11575	236.5034	22.6966	16.6982	0.0290722	0.01432758
1390.53942	138.01404	90.86278	0.75607	0.11587	235.5163	23.6837	17.6853	0.0419534	0.02224949
1390.40045	138.52711	90.41708	0.79295	0.11591	234.3611	24.8389	18.8405	0.0570287	0.03215973
1390.30054	139.04017	90.02676	0.81783	0.11594	233.3494	25.8506	19.8523	0.0702309	0.04128897
1390.22166	139.55323	89.62384	0.84087	0.11596	232.3050	26.8950	20.8966	0.0838593	0.05108125
1390.17141	140.0663	89.2031	0.86145	0.11598	231.2144	27.9856	21.9872	0.0980904	0.06165268
1390.11738	140.57936	88.77595	0.87674	0.116	230.1073	29.0927	23.0944	0.1125384	0.0727044
1390.10741	141.09242	88.36283	0.89024	0.116	229.0365	30.1635	24.1652	0.1265117	0.08366754
1390.08024	141.60549	87.90553	0.90169	0.11601	227.8511	31.3489	25.3505	0.1419795	0.09608833
1390.05209	142.11855	87.49561	0.90979	0.11602	226.7886	32.4114	26.4130	0.1558446	0.10745588
1390.04499	142.63161	87.0656	0.91642	0.11602	225.6740	33.5260	27.5276	0.1703893	0.11959988
1390.03824	143.14468	86.6764	0.92031	0.11602	224.6652	34.5348	28.5364	0.1835536	0.13077222
1390.02253	143.65774	86.27694	0.92392	0.11602	223.6298	35.5702	29.5718	0.1970649	0.14240697
1390.01112	144.1708	85.86056	0.92588	0.11603	222.5506	36.6494	30.6510	0.2111486	0.15470553
1390.01112	144.68387	85.45663	0.92358	0.11603	221.5036	37.6964	31.6980	0.2248111	0.16679437
1390.00133	145.19693	85.0566	0.92329	0.11603	220.4667	38.7333	32.7349	0.2383418	0.17891229
1390.01316	145.70999	84.64312	0.92036	0.11603	219.3950	39.8050	33.8067	0.2523273	0.19158307
1389.99042	146.22306	84.27874	0.91688	0.11603	218.4505	40.7495	34.7511	0.2646521	0.20286655
1389.99441	146.73612	83.89447	0.91266	0.11603	217.4545	41.7455	35.7472	0.2776497	0.21488031
1390.00479	147.24918	83.52889	0.90962	0.11603	216.5069	42.6931	36.6947	0.2900151	0.22641473
1390.01049	147.76225	83.15937	0.9046	0.11603	215.5491	43.6509	37.6525	0.3025137	0.23817386
1390.00688	148.27531	82.80715	0.90002	0.11603	214.6361	44.5639	38.5655	0.3144272	0.24947335
1390.00198	148.78837	82.4224	0.8951	0.11603	213.6389	45.5611	39.5628	0.327441	0.26191459
1390.00522	149.30144	82.08473	0.89002	0.11603	212.7636	46.4364	40.4380	0.3388624	0.27291539
1389.99943	149.8145	81.7748	0.88515	0.11603	211.9603	47.2397	41.2413	0.3493455	0.283078
1389.99157	150.32756	81.44331	0.88035	0.11603	211.1011	48.0989	42.1006	0.3605578	0.29401525
1389.99752	150.84063	81.11393	0.8755	0.11603	210.2473	48.9527	42.9543	0.3716987	0.30495047
1389.99349	151.35369	80.79764	0.87028	0.11603	209.4275	49.7725	43.7741	0.3823969	0.31551303
1389.99494	151.86675	80.48484	0.86599	0.11603	208.6167	50.5833	44.5849	0.3929771	0.32601734
1389.99188	152.37982	80.18351	0.86207	0.11603	207.8357	51.3643	45.3660	0.4031693	0.33619012
1389.99249	152.89288	79.88464	0.85738	0.11603	207.0610	52.1390	46.1406	0.4132783	0.34633079
1390.0006	153.40594	79.59274	0.85408	0.11603	206.3044	52.8956	46.8972	0.4231515	0.35628299
1389.99609	153.91901	79.29748	0.8512	0.11603	205.5391	53.6609	47.6626	0.4331384	0.3663971
1389.99172	154.43207	79.0223	0.84779	0.11603	204.8258	54.3742	48.3758	0.4424461	0.37586548
1389.99886	154.94513	78.74912	0.84512	0.11603	204.1177	55.0823	49.0839	0.4516861	0.38530454
1390.00517	155.4582	78.47596	0.84259	0.11603	203.4097	55.7903	49.7919	0.4609255	0.3947816
1390.00001	155.97126	78.21763	0.83975	0.11603	202.7401	56.4599	50.4615	0.4696633	0.40377918
1390.00269	156.48432	77.95541	0.83714	0.11603	202.0604	57.1396	51.1412	0.4785326	0.41294656
1390.01351	156.99739	77.69848	0.8344	0.11603	201.3945	57.8055	51.8072	0.487223	0.42196202
1390.00551	157.51045	77.45274	0.83299	0.11603	200.7575	58.4425	52.4441	0.4955349	0.43061498
1389.99985	158.02351	77.20761	0.83094	0.11603	200.1221	59.0779	53.0795	0.5038262	0.43927544
1389.99636	158.53658	76.96571	0.83045	0.11603	199.4951	59.7049	53.7065	0.5120083	0.44784977
1390.00492	159.04964	76.72948	0.82762	0.11603	198.8828	60.3172	54.3188	0.5199985	0.45624962
1389.99609	159.5627	76.50318	0.82689	0.11603	198.2962	60.9038	54.9054	0.5276529	0.46432063

1389.99825	160.07577	76.2756	0.82558	0.11603	197.7064	61.4936	55.4953	0.5353506	0.47246094
1389.99743	160.58883	76.05071	0.82352	0.11603	197.1234	62.0766	56.0782	0.5429572	0.48052806
1390.00151	161.10189	75.836	0.82251	0.11603	196.5669	62.6331	56.6347	0.5502196	0.48825114
1390.01386	161.61496	75.61232	0.82228	0.11603	195.9871	63.2129	57.2145	0.5577854	0.49631858

APPENDIX 13: Data for the reactivity of China nuts coke.

Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\Delta$ V/mW)	mg change	mg evolved	CO evolved	%R
888.50086	86.86712	99.62897	0.19934	0.25802	249.7698278	0.93017221		
893.63769	87.38113	99.61628	0.20289	0.257	249.738014	0.96198604		
898.78054	87.89514	99.6055	0.20591	0.25596	249.7109885	0.9890115	0	0
903.92066	88.40914	99.59391	0.2089	0.25491	249.6819324	1.01806763	0.02905613	0.0003801
909.05539	88.92315	99.58253	0.21185	0.25384	249.6534027	1.04659729	0.05758579	0.0007533
914.22441	89.43716	99.56998	0.21476	0.25276	249.6219399	1.07806014	0.08904864	0.0011649
919.36328	89.95116	99.55885	0.21918	0.25167	249.594037	1.10596305	0.11695155	0.00153
924.49704	90.46517	99.54777	0.22294	0.25057	249.5662594	1.13374061	0.14472911	0.0018934
929.64312	90.97918	99.53413	0.22583	0.24945	249.5320639	1.16793609	0.17892459	0.0023407
934.78124	91.49318	99.52227	0.22865	0.24832	249.5023309	1.19766911	0.20865761	0.0027297
939.92369	92.00719	99.50877	0.2315	0.24718	249.4684864	1.23151361	0.24250211	0.0031724
945.058	92.5212	99.49578	0.23384	0.24602	249.4359205	1.26407954	0.27506804	0.0035985
950.19373	93.0352	99.48104	0.2366	0.24486	249.3989673	1.30103272	0.31202122	0.0040819
955.33461	93.54921	99.46789	0.23888	0.24367	249.3660002	1.33399977	0.34498827	0.0045132
960.48116	94.06322	99.45252	0.2415	0.24248	249.3274676	1.37253236	0.38352086	0.0050173
965.61235	94.57722	99.43778	0.24518	0.24127	249.2905145	1.40948554	0.42047404	0.0055007
970.7568	95.09123	99.42404	0.2483	0.24005	249.2560683	1.44393172	0.45492022	0.0059513
975.8936	95.60524	99.40885	0.25161	0.23882	249.217987	1.48201305	0.49300155	0.0064495
981.04162	96.11924	99.39288	0.25444	0.23757	249.1779502	1.52204984	0.53303834	0.0069733
986.19511	96.63325	99.37777	0.25633	0.23631	249.1400694	1.55993061	0.57091911	0.0074688
991.332	97.14726	99.36093	0.25945	0.23504	249.0978515	1.60214849	0.61313699	0.0080211
996.4918	97.66126	99.34417	0.26116	0.23376	249.0558342	1.64416581	0.65515431	0.0085708
1001.64711	98.17527	99.328	0.26393	0.23246	249.015296	1.684704	0.6956925	0.0091011
1006.78582	98.68928	99.31151	0.26826	0.23115	248.9739556	1.72604443	0.73703293	0.0096419
1011.93392	99.20328	99.2906	0.27094	0.22983	248.9215342	1.7784658	0.7894543	0.0103277
1017.08778	99.71729	99.27237	0.27409	0.2285	248.8758316	1.82416841	0.83515691	0.0109256
1022.23132	100.2313	99.25246	0.27668	0.22716	248.8259172	1.87408278	0.88507128	0.0115786
1027.37106	100.7453	99.2314	0.27795	0.22581	248.7731198	1.9268802	0.9378687	0.0122693
1032.51656	101.25931	99.20631	0.27994	0.22444	248.7102192	1.98978083	1.00076933	0.0130921
1037.65286	101.77332	99.18306	0.28115	0.22307	248.6519314	2.04806858	1.05905708	0.0138547
1042.80388	102.28732	99.15844	0.28294	0.22168	248.5902091	2.10979092	1.12077942	0.0146621
1047.93609	102.80133	99.13026	0.2835	0.22028	248.5195618	2.18043818	1.19142668	0.0155863
1053.07995	103.31534	99.10038	0.28422	0.21888	248.4446527	2.25534734	1.26633584	0.0165663
1058.22794	103.82934	99.06979	0.28524	0.21746	248.3679635	2.33203647	1.34302497	0.0175696
1063.35938	104.34335	99.03704	0.286	0.21603	248.2858593	2.41414072	1.42512922	0.0186437
1068.50551	104.85736	99.00155	0.28658	0.2146	248.1968859	2.50311415	1.51410265	0.0198076
1073.64467	105.37136	98.96289	0.28698	0.21315	248.0999652	2.60003477	1.61102327	0.0210755
1078.78234	105.88537	98.92383	0.28683	0.21169	248.0020418	2.69795819	1.70894669	0.0223566
1083.92779	106.39938	98.88319	0.28769	0.21022	247.9001573	2.79984267	1.81083117	0.0236894
1089.06467	106.91338	98.84001	0.28886	0.20875	247.7919051	2.90809493	1.91908343	0.0251056
1094.2117	107.42739	98.79499	0.28952	0.20726	247.6790399	3.02096007	2.03194857	0.0265821
1099.34906	107.9414	98.74805	0.29174	0.20577	247.5613614	3.13863865	2.14962715	0.0281216
1104.4934	108.4554	98.70032	0.29252	0.20427	247.4417022	3.25829776	2.26928626	0.029687
1109.63477	108.96941	98.6534	0.29507	0.20276	247.3240738	3.3759262	2.3869147	0.0312258
1114.76717	109.48342	98.60669	0.29695	0.20125	247.2069718	3.49302817	2.50401667	0.0327578

1119.91521	109.99742	98.56019	0.29919	0.19972	247.0903963	3.60960367	2.62059217	0.0342828
1125.05993	110.51143	98.51691	0.29974	0.19819	246.9818934	3.71810663	2.72909513	0.0357022
1130.19843	111.02544	98.47454	0.30132	0.19665	246.8756718	3.82432822	2.83531672	0.0370918
1135.33733	111.53944	98.43562	0.3017	0.1951	246.7780993	3.92190066	2.93288916	0.0383683
1140.48218	112.05345	98.3993	0.30485	0.19355	246.6870451	4.0129549	3.0239434	0.0395595
1145.62011	112.56746	98.36597	0.30628	0.19199	246.6034868	4.09651321	3.10750171	0.0406526
1150.7695	113.08146	98.33332	0.30648	0.19042	246.5216332	4.17836676	3.18935526	0.0417234

APPENDIX 14: Data for the reactivity of China nuts coke at 1190°C.

Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./(V/mW)	Segment	mg change	mg evolved	CO evolved	%R
1190.96383	117.31557	98.09555	0.54446	0.17801	2	246.71031	4.78969	3.80990	0
1191.72335	117.78862	98.06881	0.69757	0.17777	2	246.64306	4.85694	3.87715	0.010347927
1191.12515	118.26167	98.0511	0.81785	0.17796	2	246.59852	4.90148	3.92169	0.010928575
1190.9944	118.73471	98.03394	0.82976	0.178	2	246.55536	4.94464	3.96485	0.011491191
1190.86069	119.20776	98.01662	0.83429	0.17804	2	246.51180	4.98820	4.00841	0.012059052
1190.74869	119.68081	97.99974	0.84097	0.17808	2	246.46935	5.03065	4.05086	0.012612488
1190.63309	120.15385	97.98393	0.84752	0.17811	2	246.42958	5.07042	4.09062	0.013130842
1190.54331	120.6269	97.96774	0.85376	0.17814	2	246.38887	5.11113	4.13134	0.013661654
1190.4592	121.09995	97.95191	0.85931	0.17817	2	246.34905	5.15095	4.17115	0.014180664
1190.3973	121.57299	97.93785	0.86451	0.17818	2	246.31369	5.18631	4.20651	0.014641642
1190.34732	122.04604	97.9227	0.87042	0.1782	2	246.27559	5.22441	4.24462	0.015138356
1190.2829	122.51909	97.90811	0.87628	0.17822	2	246.23890	5.26110	4.28131	0.015616711
1190.23705	122.99213	97.89468	0.88221	0.17823	2	246.20512	5.29488	4.31509	0.016057033
1190.2119	123.46518	97.88056	0.88791	0.17824	2	246.16961	5.33039	4.35060	0.016519978
1190.1872	123.93823	97.86829	0.89304	0.17825	2	246.13875	5.36125	4.38146	0.016922267
1190.15131	124.41127	97.85572	0.89941	0.17826	2	246.10714	5.39286	4.41307	0.017334393
1190.12224	124.88432	97.84336	0.90607	0.17827	2	246.07605	5.42395	4.44416	0.017739634
1190.10717	125.35737	97.83181	0.91091	0.17828	2	246.04700	5.45300	4.47320	0.018118317
1190.08895	125.83041	97.818	0.91656	0.17828	2	246.01227	5.48773	4.50794	0.018571098
1190.07449	126.30346	97.8054	0.9225	0.17829	2	245.98058	5.51942	4.53963	0.018984208
1190.06024	126.77651	97.79351	0.92808	0.17829	2	245.95068	5.54932	4.56953	0.019374038
1190.04497	127.24955	97.78094	0.93334	0.17829	2	245.91906	5.58094	4.60114	0.019786164
1190.04242	127.7226	97.76992	0.9387	0.1783	2	245.89135	5.60865	4.62886	0.020147471
1190.02422	128.19565	97.75935	0.94447	0.1783	2	245.86477	5.63523	4.65544	0.020494024
1190.01387	128.66869	97.74762	0.9502	0.1783	2	245.83526	5.66474	4.68494	0.020878609
1190.01195	129.14174	97.73676	0.95568	0.17831	2	245.80795	5.69205	4.71225	0.02123467
1190.0034	129.61479	97.72582	0.96155	0.17831	2	245.78044	5.71956	4.73977	0.021593354
1190.00304	130.08783	97.71462	0.96782	0.17831	2	245.75227	5.74773	4.76794	0.021960562
1190.00166	130.56088	97.70299	0.97346	0.17831	2	245.72302	5.77698	4.79719	0.022341868
1190.01729	131.03393	97.69198	0.9785	0.1783	2	245.69533	5.80467	4.82488	0.022702847
1189.99726	131.50697	97.68006	0.98468	0.17831	2	245.66535	5.83465	4.85486	0.023093662
1190.00432	131.98002	97.66857	0.99075	0.17831	2	245.63645	5.86355	4.88375	0.023470378
1190.00338	132.45307	97.6586	0.99709	0.17831	2	245.61138	5.88862	4.90883	0.023797259
1189.99768	132.92611	97.64805	1.00272	0.17831	2	245.58485	5.91515	4.93536	0.024143156
1189.99631	133.39916	97.63656	1.0083	0.17831	2	245.55595	5.94405	4.96426	0.024519873
1190.0048	133.87221	97.6271	1.01518	0.17831	2	245.53216	5.96784	4.98805	0.024830033
1189.99363	134.34525	97.61623	1.0215	0.17831	2	245.50482	5.99518	5.01539	0.025186421
1189.99273	134.8183	97.60662	1.0269	0.17831	2	245.48065	6.01935	5.03956	0.025501499
1190.00018	135.29135	97.59406	1.0322	0.17831	2	245.44906	6.05094	5.07115	0.025913297
1189.99675	135.76439	97.58401	1.03776	0.17831	2	245.42379	6.07621	5.09642	0.026242801
1189.99328	136.23744	97.57293	1.04323	0.17831	2	245.39592	6.10408	5.12429	0.026606075
1189.98422	136.71049	97.56205	1.04898	0.17831	2	245.36856	6.13144	5.15165	0.026962791
1189.99729	137.18353	97.55267	1.05492	0.17831	2	245.34497	6.15503	5.17524	0.027270328
1189.99485	137.65658	97.54246	1.06038	0.17831	2	245.31929	6.18071	5.20092	0.027605078



1189.9919	138.12963	97.53226	1.06709	0.17831	2	245.29363	6.20637	5.22657	0.0279395
1189.99096	138.60267	97.52049	1.07271	0.17831	2	245.26403	6.23597	5.25617	0.028325397
1189.99802	139.07572	97.51029	1.07815	0.17831	2	245.23838	6.26162	5.28183	0.028659818
1189.99319	139.54877	97.5009	1.08441	0.17831	2	245.21476	6.28524	5.30544	0.028967683
1189.99297	140.02181	97.49073	1.09059	0.17831	2	245.18919	6.31081	5.33102	0.029301121
1189.99397	140.49486	97.48052	1.09664	0.17831	2	245.16351	6.33649	5.35670	0.029635871
1189.9925	140.96791	97.4704	1.1029	0.17831	2	245.13806	6.36194	5.38215	0.02996767
1189.98545	141.44095	97.45933	1.10783	0.17831	2	245.11021	6.38979	5.40999	0.030330616
1189.99962	141.914	97.45066	1.11316	0.17831	2	245.08841	6.41159	5.43180	0.030614875
1189.9895	142.38705	97.43995	1.11973	0.17831	2	245.06147	6.43853	5.45873	0.030966018
1190.00186	142.86009	97.42881	1.12525	0.17831	2	245.03346	6.46654	5.48675	0.031331259
1190.0062	143.33314	97.41922	1.13101	0.17831	2	245.00934	6.49066	5.51087	0.031645681
1189.9978	143.80619	97.41004	1.13668	0.17831	2	244.98625	6.51375	5.53396	0.031946661
1190.0074	144.27923	97.39899	1.14194	0.17831	2	244.95846	6.54154	5.56175	0.032308951
1189.99724	144.75228	97.3903	1.14834	0.17831	2	244.93660	6.56340	5.58360	0.032593865
1189.99146	145.22533	97.37891	1.15331	0.17831	2	244.90796	6.59204	5.61225	0.032967303

APPENDIX 15: Data for the reactivity of China nuts coke at 1240°C.

Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\nabla$ V/mW)	Segment	mg change	mg evolved	CO evolved	%R
1239.6783	121.96926	97.72279	0.3132	0.16268	1	244.60014	5.69986	4.57386	0
1241.47755	122.45327	97.6858	0.36019	0.16211	2	244.50756	5.79244	4.66644	0.0022728
1241.22025	122.93727	97.64844	0.55725	0.16219	2	244.41405	5.88595	4.75996	0.0034961
1240.89449	123.42128	97.61628	0.59887	0.1623	2	244.33355	5.96645	4.84045	0.0045492
1240.76319	123.90528	97.58407	0.6106	0.16234	2	244.25293	6.04707	4.92107	0.0056039
1240.64464	124.38929	97.55101	0.62084	0.16238	2	244.17018	6.12982	5.00382	0.0066864
1240.55186	124.87329	97.52112	0.62744	0.16241	2	244.09536	6.20464	5.07864	0.0076651
1240.45588	125.3573	97.49213	0.63294	0.16244	2	244.02280	6.27720	5.15120	0.0086144
1240.38116	125.8413	97.46232	0.63774	0.16246	2	243.94819	6.35181	5.22581	0.0095905
1240.31466	126.32531	97.43492	0.64457	0.16248	2	243.87960	6.42040	5.29440	0.0104877
1240.2743	126.80931	97.4059	0.65036	0.16249	2	243.80697	6.49303	5.36703	0.011438
1240.21712	127.29332	97.37776	0.65595	0.16251	2	243.73653	6.56347	5.43747	0.0123594
1240.19193	127.77732	97.3528	0.66213	0.16252	2	243.67406	6.62594	5.49994	0.0131767
1240.14658	128.26133	97.32613	0.66808	0.16253	2	243.60730	6.69270	5.56670	0.01405
1240.12595	128.74533	97.29881	0.67279	0.16254	2	243.53892	6.76108	5.63508	0.0149446
1240.09855	129.22934	97.27296	0.67837	0.16255	2	243.47422	6.82578	5.69978	0.015791
1240.08022	129.71334	97.24478	0.68381	0.16256	2	243.40368	6.89632	5.77032	0.0167138
1240.0655	130.19735	97.21908	0.68941	0.16256	2	243.33936	6.96064	5.83464	0.0175553
1240.04522	130.68135	97.19241	0.69524	0.16257	2	243.27260	7.02740	5.90140	0.0184286
1240.04232	131.16536	97.16588	0.70055	0.16257	2	243.20620	7.09380	5.96780	0.0192973
1240.03021	131.64936	97.14018	0.70662	0.16257	2	243.14187	7.15813	6.03213	0.0201388
1240.02636	132.13337	97.11525	0.71411	0.16257	2	243.07947	7.22053	6.09453	0.0209551
1240.01975	132.61737	97.09022	0.71929	0.16257	2	243.01682	7.28318	6.15718	0.0217747
1240.01824	133.10138	97.06429	0.72483	0.16257	2	242.95192	7.34808	6.22208	0.0226238
1240.0123	133.58538	97.03777	0.72995	0.16258	2	242.88554	7.41446	6.28846	0.0234922
1240.01759	134.06939	97.01196	0.73548	0.16257	2	242.82094	7.47906	6.35306	0.0243373
1240.00337	134.55339	96.98653	0.74135	0.16258	2	242.75728	7.54272	6.41672	0.02517
1239.99436	135.0374	96.96294	0.74701	0.16258	2	242.69824	7.60176	6.47576	0.0259424
1240.00765	135.5214	96.93611	0.75243	0.16258	2	242.63108	7.66892	6.54292	0.026821
1240.01261	136.00541	96.90944	0.75789	0.16258	2	242.56433	7.73567	6.60967	0.0276943
1239.99341	136.48941	96.88215	0.76281	0.16258	2	242.49602	7.80398	6.67798	0.0285879
1239.98717	136.97342	96.85668	0.7666	0.16258	2	242.43227	7.86773	6.74173	0.0294219
1239.99793	137.45742	96.83159	0.77144	0.16258	2	242.36947	7.93053	6.80453	0.0302434
1239.99028	137.94143	96.80578	0.77709	0.16258	2	242.30487	7.99513	6.86913	0.0310886
1239.99123	138.42543	96.77983	0.78289	0.16258	2	242.23991	8.06009	6.93409	0.0319383
1240.01048	138.90944	96.75333	0.78781	0.16258	2	242.17358	8.12642	7.00042	0.032806
1239.99609	139.39344	96.72758	0.79308	0.16258	2	242.10913	8.19087	7.06487	0.0336492
1239.99898	139.87745	96.70204	0.79826	0.16258	2	242.04521	8.25479	7.12879	0.0344855
1239.99978	140.36145	96.67671	0.80237	0.16258	2	241.98181	8.31819	7.19220	0.0353149
1239.98483	140.84546	96.65034	0.80815	0.16259	2	241.91580	8.38420	7.25820	0.0361784
1240.00056	141.32946	96.6254	0.81316	0.16258	2	241.85338	8.44662	7.32062	0.036995
1239.99531	141.81347	96.59943	0.8183	0.16258	2	241.78837	8.51163	7.38563	0.0378454
1239.99056	142.29747	96.57389	0.8227	0.16258	2	241.72445	8.57555	7.44955	0.0386817
1240.00639	142.78148	96.54894	0.82866	0.16258	2	241.66200	8.63800	7.51200	0.0394987

1240.01281	143.26548	96.52415	0.83324	0.16258	2	241.59995	8.70005	7.57405	0.0403104
1239.99466	143.74949	96.50006	0.83788	0.16258	2	241.53965	8.76035	7.63435	0.0410992
1239.99659	144.23349	96.47588	0.84322	0.16258	2	241.47913	8.82087	7.69487	0.041891
1239.99859	144.7175	96.44981	0.84794	0.16258	2	241.41387	8.88613	7.76013	0.0427446
1239.99274	145.2015	96.42355	0.85315	0.16258	2	241.34815	8.95185	7.82585	0.0436045
1239.99047	145.68551	96.39996	0.858	0.16258	2	241.28910	9.01090	7.88490	0.0443769
1239.99111	146.16951	96.37367	0.86319	0.16258	2	241.22330	9.07670	7.95070	0.0452378
1239.98721	146.65352	96.34852	0.86888	0.16258	2	241.16035	9.13965	8.01365	0.0460613
1239.99458	147.13752	96.32444	0.87358	0.16258	2	241.10007	9.19993	8.07393	0.0468498
1239.99985	147.62153	96.29844	0.87867	0.16258	2	241.03500	9.26500	8.13901	0.0477011
1239.99194	148.10553	96.27317	0.88333	0.16258	2	240.97174	9.32826	8.20226	0.0485286
1239.99067	148.58954	96.24882	0.88809	0.16258	2	240.91080	9.38920	8.26320	0.0493259
1239.99212	149.07354	96.22265	0.8928	0.16258	2	240.84529	9.45471	8.32871	0.0501828
1239.99434	149.55755	96.19907	0.8978	0.16258	2	240.78627	9.51373	8.38773	0.050955
1239.99132	150.04155	96.1761	0.90348	0.16258	2	240.72878	9.57122	8.44522	0.0517071
1239.99661	150.52556	96.15321	0.90869	0.16258	2	240.67148	9.62852	8.50252	0.0524566
1239.99422	151.00956	96.13016	0.91308	0.16258	2	240.61379	9.68621	8.56021	0.0532114
1239.98512	151.49357	96.10733	0.91865	0.16259	2	240.55665	9.74335	8.61735	0.0539589
1239.99785	151.97757	96.08401	0.92344	0.16258	2	240.49828	9.80172	8.67572	0.0547225
1239.99828	152.46158	96.05989	0.92818	0.16258	2	240.43790	9.86210	8.73610	0.0555123

APPENDIX 16: Data for the reactivity of China nuts coke at 1290°C.

Temp./- C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\bar{t}$ V/mW)	mg change	mg evolved	CO evolved	%R	%R(adj)
1290.65495	128.68648	96.93445	0.65008	0.14657	243.20854	7.69146	6.66293	0	0
1290.54667	129.17954	96.85167	0.65608	0.14661	243.00084	7.89916	6.87062	0.002528	0.008982387
1290.43885	129.67259	96.77002	0.66252	0.14664	242.79598	8.10402	7.07548	0.005208	0.015875886
1290.36234	130.16564	96.6922	0.66896	0.14667	242.60073	8.29927	7.27073	0.0077623	0.02174265
1290.29631	130.65869	96.61245	0.6747	0.14669	242.40064	8.49936	7.47082	0.0103799	0.027337652
1290.23283	131.15174	96.53205	0.67933	0.14671	242.19891	8.70109	7.67255	0.0130189	0.032680178
1290.20203	131.64479	96.45232	0.68443	0.14672	241.99887	8.90113	7.87259	0.0156359	0.03775445
1290.15302	132.13785	96.37343	0.68978	0.14673	241.80094	9.09906	8.07052	0.0182253	0.042600148
1290.12861	132.6309	96.29549	0.69501	0.14674	241.60538	9.29462	8.26608	0.0207835	0.047245688
1290.10049	133.12395	96.21765	0.69934	0.14675	241.41008	9.48992	8.46138	0.0233384	0.051765503
1290.08038	133.617	96.14054	0.70414	0.14676	241.21661	9.68339	8.65485	0.0258694	0.05614043
1290.07894	134.11005	96.0635	0.70885	0.14676	241.02332	9.87668	8.84814	0.0283981	0.06042154
1290.05133	134.6031	95.98736	0.71334	0.14676	240.83229	10.06771	9.03917	0.0308972	0.064573831
1290.04042	135.09616	95.91025	0.71723	0.14677	240.63882	10.26118	9.23264	0.0334282	0.068707012
1290.03317	135.58921	95.83632	0.72308	0.14677	240.45333	10.44667	9.41813	0.0358548	0.072607804
1290.02669	136.08226	95.76111	0.72795	0.14677	240.26462	10.63538	9.60684	0.0383234	0.076519092
1290.03156	136.57531	95.68731	0.7327	0.14677	240.07946	10.82054	9.79200	0.0407458	0.080305421
1290.0114	137.06836	95.61284	0.73715	0.14678	239.89262	11.00738	9.97884	0.0431901	0.084078036
1290.01296	137.56141	95.53911	0.74203	0.14678	239.70763	11.19237	10.16383	0.0456101	0.087768801
1290.00082	138.05447	95.46621	0.74763	0.14678	239.52472	11.37528	10.34674	0.0480029	0.091377399
1290.0035	138.54752	95.39094	0.75312	0.14678	239.33587	11.56413	10.53559	0.0504735	0.095063518
1290.01216	139.04057	95.31894	0.75855	0.14678	239.15522	11.74478	10.71624	0.0528367	0.098553844
1290.0072	139.53362	95.24609	0.764	0.14678	238.97244	11.92756	10.89902	0.0552279	0.102051845
1289.99936	140.02667	95.17387	0.76932	0.14678	238.79124	12.10876	11.08022	0.0575984	0.105488032
1289.99653	140.51972	95.09927	0.77406	0.14678	238.60407	12.29593	11.26739	0.060047	0.109006124
1289.99524	141.01278	95.0257	0.77979	0.14678	238.41948	12.48052	11.45198	0.0624617	0.112445968
1289.99677	141.50583	94.95194	0.78542	0.14678	238.23442	12.66558	11.63704	0.0648828	0.115866502
1289.99683	141.99888	94.87843	0.79113	0.14678	238.04998	12.85002	11.82148	0.0672956	0.11924862
1290.00147	142.49193	94.80555	0.79629	0.14678	237.86712	13.03288	12.00434	0.0696877	0.122576462
1289.99693	142.98498	94.733	0.80223	0.14678	237.68510	13.21490	12.18636	0.072069	0.125865263
1290.00002	143.47803	94.66037	0.80745	0.14678	237.50287	13.39713	12.36859	0.0744529	0.12913469
1290.00562	143.97109	94.58554	0.81447	0.14678	237.31512	13.58488	12.55634	0.0769091	0.132480022
1289.98911	144.46414	94.5133	0.82075	0.14678	237.13387	13.76613	12.73759	0.0792802	0.135688138
1289.99232	144.95719	94.44012	0.82542	0.14678	236.95026	13.94974	12.92120	0.0816822	0.138917324
1289.99898	145.45024	94.36505	0.83165	0.14678	236.76191	14.13809	13.10955	0.0841462	0.14220906
1289.99246	145.94329	94.29101	0.83714	0.14678	236.57614	14.32386	13.29532	0.0865764	0.14543567
1289.99752	146.43634	94.21565	0.84208	0.14678	236.38707	14.51293	13.48439	0.08905	0.148700148
1289.99803	146.9294	94.14155	0.84845	0.14678	236.20115	14.69885	13.67031	0.0914821	0.151891349
1289.9906	147.42245	94.06292	0.85502	0.14678	236.00387	14.89613	13.86759	0.094063	0.155258035
1289.9929	147.9155	93.9856	0.8604	0.14678	235.80987	15.09013	14.06159	0.0966009	0.158549585
1289.9944	148.40855	93.91021	0.86667	0.14678	235.62072	15.27928	14.25074	0.0990754	0.161741363
1290.00611	148.9016	93.83044	0.87355	0.14678	235.42057	15.47943	14.45089	0.1016937	0.165100233
1290.00189	149.39465	93.75301	0.87991	0.14678	235.22630	15.67370	14.64516	0.1042352	0.168343078
1289.99574	149.88771	93.6752	0.88479	0.14678	235.03108	15.86892	14.84038	0.1067891	0.171584994
1289.99806	150.38076	93.59841	0.89114	0.14678	234.83841	16.06159	15.03305	0.1093096	0.174768334

1289.99748	150.87381	93.52009	0.89804	0.14678	234.64191	16.25809	15.22955	0.1118803	0.177999112
1289.99513	151.36686	93.44032	0.90458	0.14678	234.44176	16.45824	15.42970	0.1144986	0.181273566
1289.99762	151.85991	93.36172	0.91138	0.14678	234.24456	16.65544	15.62691	0.1170785	0.184484502
1290.00537	152.35296	93.28188	0.91755	0.14678	234.04424	16.85576	15.82722	0.119699	0.187730772
1290.00956	152.84602	93.20079	0.9253	0.14678	233.84078	17.05922	16.03068	0.1223607	0.191012482
1289.99245	153.33907	93.12001	0.93168	0.14678	233.63811	17.26189	16.23336	0.1250121	0.194266631
1289.99515	153.83212	93.03577	0.93865	0.14678	233.42675	17.47325	16.44471	0.1277771	0.197644618
1289.99696	154.32517	92.95453	0.94604	0.14678	233.22292	17.67708	16.64854	0.1304436	0.200887655
1289.99808	154.81822	92.87047	0.95224	0.14678	233.01201	17.88799	16.85945	0.1332027	0.204228504
1289.99597	155.31127	92.78528	0.95848	0.14678	232.79827	18.10173	17.07319	0.1359989	0.20759933
1289.99998	155.80433	92.70093	0.96599	0.14678	232.58663	18.31337	17.28483	0.1387675	0.210922471
1290.00402	156.29738	92.6166	0.97344	0.14678	232.37505	18.52495	17.49641	0.1415355	0.214230802
1290.00084	156.79043	92.53227	0.98071	0.14678	232.16347	18.73653	17.70800	0.1443035	0.217525444

APPENDIX 17: Data for the reactivity of China nuts coke at 1340°C.

Temp./ -C	Time/mi n	Mass/ %	DTA(mW /mg)	Sensit./(† V/mW)	Segment	mg change	mg evolved	CO evolved	%R	%R(adj)	If(X)	Pf(X)	ti(model)	ti(exp)
1340.21 202	132.049 74	95.846 59	0.38192	0.13111	2	240.479 09	10.4209 1	9.51887	0	0	0	0	0	0
1341.14 728	132.553 75	95.635 49	0.41699	0.13083	2	239.949 44	10.9505 6	10.0485 2	0.0028 62	0.000419 231	0.0001 398	5.8596E-08	0.032805 8	0.5040 1
1340.67 102	133.057 76	95.442 23	0.62133	0.13097	2	239.464 56	11.4354 4	10.5334 1	0.0091 99	0.001976 274	0.0006 592	1.303E-06	0.154787 9	1.0080 2
1340.53 028	133.561 76	95.248 55	0.63048	0.13102	2	238.978 61	11.9213 9	11.0193 5	0.0155 498	0.003968 348	0.0013 245	5.2585E-06	0.311173 1	1.5120 2
1340.42 883	134.065 77	95.059 77	0.6352	0.13105	2	238.504 96	12.3950 4	11.4930 0	0.0217 399	0.006192 668	0.0020 685	1.2818E-05	0.486218 7	2.0160 3
1340.33 382	134.569 78	94.872 2	0.64407	0.13108	2	238.034 35	12.8656 5	11.9636 1	0.0278 903	0.008621 095	0.0028 82	2.487E-05	0.677844 5	2.5200 4
1340.26 444	135.073 78	94.683 36	0.65424	0.1311	2	237.560 55	13.3394 5	12.4374 1	0.0340 824	0.011251 235	0.0037 646	4.2409E-05	0.885999 1	3.0240 4
1340.20 824	135.577 79	94.494 66	0.66372	0.13112	2	237.087 10	13.8129 0	12.9108 6	0.0402 699	0.014041 521	0.0047 026	6.6135E-05	1.107526 3	3.5280 5
1340.15 709	136.081 8	94.305 54	0.67519	0.13113	2	236.612 60	14.2874 0	13.3853 6	0.0464 712	0.016983 207	0.0056 934	9.6876E-05	1.341855 4	4.0320 6
1340.12 934	136.585 8	94.115 91	0.68759	0.13114	2	236.136 82	14.7631 8	13.8611 5	0.0526 891	0.020065 301	0.0067 337	0.00013542	1.588234	4.5360 6
1340.09 347	137.089 81	93.926 1	0.70047	0.13115	2	235.660 58	15.2394 2	14.3373 8	0.0589 13	0.023272 375	0.0078 184	0.00018243	1.845547 3	5.0400 7
1340.08 108	137.593 82	93.733 68	0.71298	0.13116	2	235.177 80	15.7222 0	14.8201 6	0.0652 225	0.026639 116	0.0089 597	0.00023939	2.116712 4	5.5440 8
1340.06 577	138.097 82	93.538 46	0.72744	0.13116	2	234.688 00	16.2120 0	15.3099 7	0.0716 238	0.030165 882	0.0101 581	0.00030747	2.401916 4	6.0480 8
1340.04 205	138.601 83	93.337 51	0.74218	0.13117	2	234.183 81	16.7161 9	15.8141 5	0.0782 13	0.033905 806	0.0114 321	0.00038909	2.705649 6	6.5520 9
1340.04 362	139.105 84	93.137 88	0.75817	0.13117	2	233.682 94	17.2170 6	16.3150 2	0.0847 588	0.037725 036	0.0127 365	0.00048253	3.017204 9	7.0561
1340.02 462	139.609 84	92.935 99	0.77353	0.13117	2	233.176 40	17.7236 0	16.8215 7	0.0913 788	0.041687 22	0.0140 934	0.00059028	3.341905 4	7.5601
1340.01 183	140.113 85	92.732 12	0.78864	0.13118	2	232.664 89	18.2351 1	17.3330 8	0.0980 637	0.045785 003	0.0155 007	0.00071337	3.679317 7	8.0641 1
1340.01 691	140.617 86	92.522 45	0.80354	0.13117	2	232.138 83	18.7611 7	17.8591 4	0.1049 388	0.050096 036	0.0169 856	0.00085573	4.036056 1	8.5681 2
1340.01 294	141.121 86	92.309 91	0.82031	0.13118	2	231.605 56	19.2944 4	18.3924 0	0.1119 08	0.054561 692	0.0185 284	0.00101718	4.407513 4	9.0721 2
1340.01 492	141.625 87	92.093 93	0.83503	0.13118	2	231.063 67	19.8363 3	18.9342 9	0.1189 901	0.059194 062	0.0201 34	0.00119981	4.794921 6	9.5761 3
1340.00 864	142.129 88	91.877 15	0.85	0.13118	2	230.519 77	20.3802 3	19.4781 9	0.1260 983	0.063935 46	0.0217 829	0.00140281	5.193661 8	10.080 14
1340.00 938	142.633 88	91.657 98	0.86564	0.13118	2	229.969 87	20.9301 3	20.0280 9	0.1332 849	0.068819 111	0.0234 87	0.00162901	5.606724 4	10.584 14
1340.00 428	143.137 89	91.433 47	0.87812	0.13118	2	229.406 58	21.4934 2	20.5913 9	0.1406 466	0.073912 11	0.0252 706	0.00188353	6.040064 9	11.088 15
1339.99 653	143.641 9	91.209 83	0.89116	0.13118	2	228.845 46	22.0545 4	21.1525 0	0.1479 798	0.079073 09	0.0270 847	0.002161	6.481889 7	11.592 16
1340.00 388	144.145 9	90.982 87	0.90375	0.13118	2	228.276 02	22.6239 8	21.7219 4	0.1554 218	0.084397 168	0.0289 632	0.002468	6.940549 7	12.096 16
1339.99 742	144.649 91	90.754 47	0.91629	0.13118	2	227.702 97	23.1970 3	22.2950 0	0.1629 111	0.089840 13	0.0308 911	0.00280383	7.412494	12.600 17
1340.00 505	145.153 92	90.524 73	0.92643	0.13118	2	227.126 55	23.7734 5	22.8714 2	0.1704 443	0.095398 467	0.0328 68	0.00316989	7.897646	13.104 18
1339.99 457	145.657 92	90.293 07	0.93812	0.13118	2	226.545 31	24.3546 9	23.4526 5	0.1780 404	0.101085 458	0.0348 989	0.00356879	8.397409 5	13.608 18
1339.99 494	146.161 93	90.063 83	0.94971	0.13118	2	225.970 15	24.9298 5	24.0278 1	0.1855 572	0.106791 962	0.0369 455	0.00399405	8.902359 3	14.112 19
1340.00 42	146.665 94	89.833	0.95927	0.13118	2	225.391 00	25.5090 0	24.6069 7	0.1931 261	0.112615 184	0.0390 429	0.00445402	9.421257 2	14.616 2
1340.00 869	147.169 94	89.601 98	0.96685	0.13118	2	224.811 37	26.0886 3	25.1866 0	0.2007 013	0.118518 647	0.0411 786	0.00494738	9.951075 5	15.120 2

1339.99	147.673	89.371	0.97428	0.13118	2	224.232	26.6670	25.7649	0.2082	0.124482	0.0433	0.00547373	10.49022	15.624
861	95	46				99	1	7	601	65	459		1	21
1340.00	148.177	89.140	0.98212	0.13118	2	223.652	27.2474	26.3454	0.2158	0.130540	0.0455	0.00603731	11.04187	16.128
228	96	1				51	9	5	464	211	574		3	22
1339.99	148.681	88.906	0.98806	0.13118	2	223.066	27.8331	26.9310	0.2234	0.136722	0.0478	0.00664291	11.60914	16.632
28	96	69				89	1	8	999	626	25		6	22
1339.99	149.185	88.681	0.99484	0.13118	2	222.500	28.3992	27.4971	0.2308	0.142765	0.0500	0.00726478	12.1678	17.136
706	97	06				78	2	8	984	376	519			23
1339.99	149.689	88.453	1.00182	0.13118	2	221.929	28.9703	28.0683	0.2383	0.148926	0.0523	0.00792961	12.74170	17.640
909	98	43				66	4	1	624	39	331		5	24
1340.01	150.193	88.225	1.00576	0.13118	2	221.357	29.5420	28.6399	0.2458	0.155157	0.0546	0.00863386	13.32658	18.144
055	98	58				98	2	8	336	064	514			24
1339.99	150.697	87.997	1.0109	0.13118	2	220.784	30.1153	29.2132	0.2533	0.161467	0.0570	0.00938021	13.92363	18.648
108	99	09				70	0	7	258	929	111			25
1340.00	151.202	87.771	1.01564	0.13118	2	220.219	30.6805	29.7784	0.2607	0.167750	0.0593	0.01015652	14.52266	19.152
805		82				50	0	7	124	095	72		3	26
1339.99	151.706	87.549	1.02077	0.13118	2	219.660	31.2390	30.3370	0.2680	0.174016	0.0617	0.01096433	15.12489	19.656
065		19				92	8	5	125	275	386		4	26
1340.00	152.210	87.326	1.02468	0.13118	2	219.102	31.7979	30.8959	0.2753	0.180341	0.0641	0.01181405	15.73767	20.160
053	01	45				06	4	0	161	831	399		2	27
1339.99	152.714	87.103	1.02789	0.13118	2	218.541	32.3582	31.4562	0.2826	0.186739	0.0665	0.01270882	16.36242	20.664
668	02	13				75	5	1	388	359	811		8	28
1340.00	153.218	86.882	1.03246	0.13118	2	217.988	32.9113	32.0092	0.2898	0.193107	0.0690	0.01363519	16.98938	21.168
433	02	7				69	1	7	667	648	239		7	28
1340.00	153.722	86.664	1.03619	0.13118	2	217.441	33.4587	32.5566	0.2970	0.199462	0.0714	0.01459548	17.62010	21.672
633	03	52				28	2	8	209	441	744		9	29
1340.00	154.226	86.447	1.03895	0.13118	2	216.895	34.0042	33.1022	0.3041	0.205845	0.0739	0.01559656	18.25885	22.176
107	04	08				72	8	4	508	834	489		4	3
1340.01	154.730	86.230	1.04088	0.13118	2	216.352	34.5471	33.6451	0.3112	0.212247	0.0764	0.01663752	18.90466	22.680
083	04	7				83	7	4	459	024	438		1	3
1340.00	155.234	86.016	1.04358	0.13118	2	215.815	35.0842	34.1821	0.3182	0.218626	0.0789	0.01771227	19.55358	23.184
205	05	66				80	0	6	643	26	435			31
1340.00	155.738	85.804	1.04571	0.13118	2	215.282	35.6172	34.7152	0.3252	0.225004	0.0814	0.01882448	20.20775	23.688
111	06	2				74	6	3	309	209	564		2	32
1339.99	156.242	85.594	1.04755	0.13118	2	214.757	36.1430	35.2409	0.3321	0.231338	0.0839	0.01996679	20.86284	24.192
845	06	66				00	0	6	017	551	658		5	32
1340.00	156.746	85.386	1.05	0.13118	2	214.234	36.6658	35.7638	0.3389	0.237680	0.0864	0.02114862	21.52422	24.696
747	07	27				15	5	1	348	91	922		2	33
1340.00	157.250	85.178	1.05205	0.13118	2	213.713	37.1865	36.2845	0.3457	0.244039	0.0890	0.02237213	22.19284	25.200
733	08	72				41	9	6	404	531	392		3	34
1340.00	157.754	84.973	1.05403	0.13118	2	213.197	37.7022	36.8002	0.3524	0.250376	0.0915	0.02363049	22.86482	25.704
022	08	19				73	7	3	798	858	919		6	34
1339.99	158.258	84.767	1.05486	0.13118	2	212.681	38.2187	37.3167	0.3592	0.256764	0.0941	0.02493866	23.54788	26.208
387	09	32				21	9	6	302	637	795		8	35
1340.00	158.762	84.565	1.05664	0.13118	2	212.176	38.7239	37.8219	0.3658	0.263049	0.0967	0.02626524	24.22566	26.712
628	1	99				07	3	0	319	749	401		2	36
1339.99	159.266	84.367	1.05811	0.13118	2	211.677	39.2224	38.3203	0.3723	0.269288	0.0992	0.0276212	24.90411	27.216
755	1	31				58	2	8	466	716	963		3	36
1339.99	159.770	84.170	1.05842	0.13118	2	211.183	39.7160	38.8139	0.3787	0.275501	0.1018	0.02901073	25.58542	27.720
032	11	58				99	1	8	974	832	564		6	37
1340.00	160.274	83.972	1.06048	0.13118	2	210.686	40.2137	39.3116	0.3853	0.281801	0.1044	0.03046012	26.28213	28.224
652	12	21				27	3	9	02	982	674		9	38

APPENDIX 18: Data for the reactivity of China coke nuts at 1390°C.

Temp./ -C	Time/mi n	Mass/%	DTA/(mW /mg)	Sensit./( $\frac{t}{V/mW}$ )	Segm ent	mg change	mg evolved	CO evolved	%R	%R(adj)	If(X)	Pf(X)	ti(model)	ti(exp)
1390.6 2365	137.239 78	92.9358	0.94274	0.11585	2	232.990 05	17.7099 5	16.7209 4	0	0	0	0	0	0
1390.8 1729	137.753 78	92.4943 3	1.15724	0.11579	2	231.883 29	18.8167 1	17.8277 0	0.0485 955	0.001455 62	0.0004 8544	7.067E-07	0.1019816	0.514
1390.4 4146	138.267 79	92.0412 5	1.30583	0.1159	2	230.747 41	19.9525 9	18.9635 7	0.0634 551	0.002590 16	0.0008 6413	2.239E-06	0.1815913	1.02801
1390.3 5539	138.781 8	91.5814 1	1.33109	0.11593	2	229.594 59	21.1054 1	20.1163 9	0.0785 363	0.004105 37	0.0013 7033	5.628E-06	0.2880797	1.54202
1390.2 6652	139.295 8	91.1152 9	1.37011	0.11595	2	228.426 03	22.2739 7	21.2849 6	0.0938 236	0.006028 28	0.0020 1348	1.215E-05	0.4234987	2.05602
1390.2 0194	139.809 81	90.6420 1	1.4032	0.11597	2	227.239 52	23.4604 8	22.4714 7	0.1093 456	0.008390 95	0.0028 0484	2.356E-05	0.5903125	2.57003
1390.1 5008	140.323 82	90.1671	1.42881	0.11599	2	226.048 92	24.6510 8	23.6620 7	0.1249 211	0.011187 51	0.0037 4317	4.193E-05	0.7883708	3.08404
1390.1 1532	140.837 82	89.6576 6	1.44818	0.116	2	224.771 75	25.9282 5	24.9392 3	0.1416 291	0.014672 01	0.0049 1479	7.223E-05	1.0360775	3.59804
1390.0 8652	141.351 83	89.1666 8	1.46437	0.116	2	223.540 87	27.1591 3	26.1701 2	0.1577 317	0.018514 2	0.0062 0988	0.0001152	1.310412	4.11205
1390.0 6089	141.865 84	88.7136 4	1.47597	0.11601	2	222.405 10	28.2949 0	27.3058 9	0.1725 899	0.022488 14	0.0075 5295	0.0001703	1.5954847	4.62606
1390.0 4184	142.379 84	88.2566 2	1.48312	0.11602	2	221.259 35	29.4406 5	28.4516 4	0.1875 787	0.026920 09	0.0090 5511	0.0002445	1.9150211	5.14006
1390.0 3659	142.893 85	87.7847 6	1.4878	0.11602	2	220.076 39	30.6236 1	29.6346 0	0.2030 542	0.031947 88	0.0107 6476	0.0003451	2.2795817	5.65407
1390.0 254	143.407 86	87.3213 7	1.48668	0.11602	2	218.914 67	31.7853 3	30.7963 1	0.2182 519	0.037337 86	0.0126 0415	0.0004726	2.6728642	6.16808
1390.0 1977	143.921 86	86.8325 6	1.48456	0.11602	2	217.689 23	33.0107 7	32.0217 6	0.2342 833	0.043515 24	0.0147 2072	0.0006437	3.1267547	6.68208
1390.0 1612	144.435 87	86.3705 8	1.47966	0.11603	2	216.531 04	34.1689 6	33.1799 4	0.2494 348	0.049822 68	0.0168 9127	0.0008463	3.5937136	7.19609
1390.0 0188	144.949 88	85.9517 4	1.47444	0.11603	2	215.481 01	35.2189 9	34.2299 8	0.2631 714	0.055939 1	0.0190 0528	0.0010699	4.0499518	7.7101
1390.0 0692	145.463 88	85.5011 2	1.46797	0.11603	2	214.351 31	36.3486 9	35.3596 8	0.2779 503	0.062946 11	0.0214 3836	0.0013591	4.5768055	8.2241
1390.0 224	145.977 89	85.0630 8	1.46033	0.11602	2	213.253 14	37.4468 6	36.4578 5	0.2923 166	0.070184 86	0.0239 6467	0.0016954	5.125827	8.73811
1390.0 068	146.491 9	84.6364 2	1.45208	0.11603	2	212.183 50	38.5165 0	37.5274 8	0.3063 096	0.077643 85	0.0265 816	0.0020822	5.6966566	9.25212
1390.0 0432	147.005 9	84.2131	1.44387	0.11603	2	211.122 24	39.5777 6	38.5887 5	0.3201 932	0.085445 67	0.0293 3396	0.002531	6.299334	9.76612
1390.0 0383	147.519 91	83.8019 6	1.43355	0.11603	2	210.091 51	40.6084 9	39.6194 7	0.3336 772	0.093408 29	0.0321 5923	0.0030361	6.9204247	10.2801 3
1390.0 1093	148.033 92	83.3995	1.42311	0.11603	2	209.082 55	41.6174 5	40.6284 4	0.3468 766	0.101572 96	0.0350 7342	0.0036041	7.5636452	10.7941 4
1390.0 0449	148.547 92	82.9975	1.41233	0.11603	2	208.074 73	42.6252 7	41.6362 6	0.3600 609	0.110096 16	0.0381 3447	0.0042518	8.2420886	11.3081 4
1389.9 9808	149.061 93	82.611	1.40105	0.11603	2	207.105 78	43.5942 2	42.6052 1	0.3727 369	0.118639 46	0.0412 2242	0.0049578	8.9293864	11.8221 5
1390.0 0607	149.575 94	82.2267 7	1.39002	0.11603	2	206.142 51	44.5574 9	43.5684 8	0.3853 384	0.127473 34	0.0444 3646	0.0057483	9.6478145	12.3361 6
1390.0 0765	150.089 94	81.8569 1	1.37742	0.11603	2	205.215 27	45.4847 3	44.4957 2	0.3974 686	0.136299 47	0.0476 6942	0.0066005	10.373605	12.8501 6
1389.9 9195	150.603 95	81.4944 9	1.36443	0.11603	2	204.306 69	46.3933 1	45.4043 0	0.4093 548	0.145256 59	0.0509 7296	0.0075298	11.118463	13.3641 7
1389.9 9568	151.117 96	81.1329 4	1.35167	0.11603	2	203.400 28	47.2997 2	46.3107 1	0.4212 125	0.154497 95	0.0544 0561	0.0085578	11.895858	13.8781 8
1390.0 0985	151.631 96	80.7853 6	1.33967	0.11603	2	202.528 90	48.1711 0	47.1820 9	0.4326 12	0.163671 45	0.0578 3788	0.0096487	12.676632	14.3921 8
1390.0 0802	152.145 97	80.4487 7	1.32788	0.11603	2	201.685 07	49.0149 3	48.0259 2	0.4436 511	0.172826 26	0.0612 8827	0.0108083	13.464994	14.9061 9



1390.0 0294	152.659 98	80.1164 7	1.31513	0.11603	2	200.851 99	49.8480 1	48.8590 0	0.4545 495	0.182127 39	0.0648 1998	0.0120602	14.275505	15.4202
1389.9 9571	153.173 98	79.7913 5	1.30312	0.11603	2	200.036 91	50.6630 9	49.6740 7	0.4652 123	0.191481 43	0.0683 9888	0.0133952	15.100503	15.9342
1390.0 1265	153.687 99	79.4783 1	1.28997	0.11603	2	199.252 12	51.4478 8	50.4588 7	0.4754 79	0.200726 07	0.0719 6316	0.0147907	15.925755	16.4482 1
1390.0 0865	154.202	79.1691 8	1.27846	0.11603	2	198.477 13	52.2228 7	51.2338 5	0.4856 175	0.210085 36	0.0755 9975	0.0162818	16.771447	16.9622 2
1389.9 9906	154.716	78.8694 7	1.26621	0.11603	2	197.725 76	52.9742 4	51.9852 3	0.4954 47	0.219378 48	0.0792 3916	0.0178415	17.621505	17.4762 2
1390.0 0292	155.230 01	78.5794 3	1.25449	0.11603	2	196.998 63	53.7013 7	52.7123 6	0.5049 594	0.228577 77	0.0828 7039	0.0194643	18.473316	17.9902 3
1390.0 0498	155.744 02	78.2959	1.2439	0.11603	2	196.287 82	54.4121 8	53.4231 7	0.5142 583	0.237767 02	0.0865 2658	0.0211649	19.334654	18.5042 4
1389.9 9987	156.258 02	78.0203	1.23343	0.11603	2	195.596 89	55.1031 1	54.1141 0	0.5232 971	0.246885 94	0.0901 8397	0.0229325	20.19992	19.0182 4
1389.9 8872	156.772 03	77.7512 5	1.22459	0.11603	2	194.922 38	55.7776 2	54.7886 0	0.5321 211	0.255966 16	0.0938 5528	0.0247729	21.072121	19.5322 5
1390.0 0066	157.286 04	77.4931 8	1.21386	0.11603	2	194.275 40	56.4246 0	55.4355 9	0.5405 849	0.264841 53	0.0974 7275	0.0266506	21.935064	20.0462 6
1390.0 0758	157.800 04	77.2383 9	1.20536	0.11603	2	193.636 64	57.0633 6	56.0743 4	0.5489 412	0.273763 67	0.1011 3875	0.028618	22.81313	20.5602 6
1389.9 8564	158.314 05	76.992	1.19883	0.11603	2	193.018 94	57.6810 6	56.6920 4	0.5570 22	0.282542 83	0.1047 7543	0.0306332	23.687669	21.0742 7
1390.0 0199	158.828 06	76.7522 1	1.19021	0.11603	2	192.417 79	58.2822 1	57.2932 0	0.5648 864	0.291229 88	0.1084 0327	0.0327061	24.56352	21.5882 8
1390.0 0211	159.342 06	76.5216 5	1.18334	0.11603	2	191.839 78	58.8602 2	57.8712 1	0.5724 48	0.299715 92	0.1119 759	0.0348078	25.429367	22.1022 8
1390.0 0307	159.856 07	76.2963 3	1.17774	0.11603	2	191.274 90	59.4251 0	58.4360 9	0.5798 377	0.308135 69	0.1155 4928	0.0369694	26.298663	22.6162 9
1389.9 9733	160.370 08	76.0780 2	1.17046	0.11603	2	190.727 60	59.9724 0	58.9833 9	0.5869 976	0.316413 12	0.1190 9061	0.0391697	27.163361	23.1303
1389.9 9552	160.884 08	75.8628 8	1.16482	0.11603	2	190.188 24	60.5117 6	59.5227 5	0.5940 535	0.324685 75	0.1226 5857	0.0414445	28.03775	23.6443
1390.0 1269	161.398 09	75.6584 8	1.16054	0.11603	2	189.675 81	61.0241 9	60.0351 8	0.6007 572	0.332651 72	0.1261 2191	0.0437078	28.889533	24.1583 1
1389.9 9597	161.912 1	75.4641 3	1.1557	0.11603	2	189.188 57	61.5114 3	60.5224 1	0.6071 312	0.340322 26	0.1294 8296	0.0459557	29.718987	24.6723 2

APPENDIX 19: Data for the reactivity of Vietnamese anthracite.

Temp./-C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./( $\mu$ V/mW)	Segment	mg change	mg evolved	CO evolved	%R	(T-900) $\circ$ C	%R
898.75174	87.89799	98.35543	0.18597	0.25596	1	243.03627	4.06373	0	0	0	0
903.89476	88.41201	98.32926	0.18766	0.25491	1	242.97160	4.12840	0.064666	0.0008468	3.895	0.0008468
909.02432	88.92603	98.30273	0.18992	0.25385	1	242.90605	4.19395	0.130222	0.0017053	9.024	0.0017053
914.18055	89.44006	98.27357	0.19105	0.25277	1	242.83399	4.26601	0.202276	0.0026488	14.181	0.0026488
919.31678	89.95408	98.24461	0.19429	0.25168	1	242.76243	4.33757	0.273836	0.0035859	19.317	0.0035859
924.46977	90.4681	98.21522	0.19613	0.25057	1	242.68981	4.41019	0.346459	0.004537	24.470	0.004537
929.59874	90.98213	98.18276	0.19753	0.24946	1	242.60960	4.49040	0.426668	0.0055873	29.599	0.0055873
934.75585	91.49615	98.14955	0.19924	0.24833	1	242.52754	4.57246	0.508729	0.0066619	34.756	0.0066619
939.87568	92.01017	98.11818	0.20081	0.24719	1	242.45002	4.64998	0.586245	0.007677	39.876	0.007677
945.02795	92.5242	98.08293	0.20155	0.24603	1	242.36292	4.73708	0.673347	0.0088176	45.028	0.0088176
950.16854	93.03822	98.0479	0.20285	0.24486	1	242.27636	4.82364	0.759907	0.0099511	50.169	0.0099511
955.31258	93.55224	98.01587	0.2046	0.24368	1	242.19721	4.90279	0.839053	0.0109876	55.313	0.0109876
960.43662	94.06627	97.97672	0.20659	0.24249	1	242.10048	4.99952	0.935792	0.0122544	60.437	0.0122544
965.60915	94.58029	97.94008	0.20788	0.24128	1	242.00994	5.09006	1.026330	0.01344	65.609	0.01344
970.73526	95.09431	97.90404	0.21029	0.24006	1	241.92088	5.17912	1.115385	0.0146062	70.735	0.0146062
975.88466	95.60834	97.86912	0.21164	0.23882	1	241.83460	5.26540	1.201672	0.0157361	75.885	0.0157361
981.055	96.12236	97.83394	0.21345	0.23757	1	241.74767	5.35233	1.288602	0.0168745	81.055	0.0168745
986.17699	96.63638	97.79868	0.2157	0.23632	1	241.66054	5.43946	1.375729	0.0180155	86.177	0.0180155
991.33703	97.15041	97.76767	0.2169	0.23504	1	241.58391	5.51609	1.452355	0.0190189	91.337	0.0190189
996.48337	97.66443	97.73364	0.21921	0.23376	1	241.49982	5.60018	1.536443	0.02012	96.483	0.02012
1001.65637	98.17845	97.70307	0.22114	0.23246	1	241.42429	5.67571	1.611982	0.0211092	101.656	0.0211092
1006.77561	98.69248	97.6762	0.2235	0.23116	1	241.35789	5.74211	1.678377	0.0219787	106.776	0.0219787
1011.91096	99.2065	97.64966	0.22504	0.22984	1	241.29231	5.80769	1.743958	0.0228375	111.911	0.0228375
1017.07137	99.72052	97.62276	0.2267	0.2285	1	241.22584	5.87416	1.810428	0.0237079	117.071	0.0237079
1022.21577	100.23455	97.59916	0.22864	0.22716	1	241.16752	5.93248	1.868743	0.0244716	122.216	0.0244716
1027.36171	100.74857	97.5742	0.22917	0.22581	1	241.10585	5.99415	1.930419	0.0252792	127.362	0.0252792
1032.50423	101.26259	97.55218	0.2307	0.22445	1	241.05144	6.04856	1.984831	0.0259918	132.504	0.0259918
1037.6481	101.77662	97.52977	0.23177	0.22307	1	240.99606	6.10394	2.040206	0.0267169	137.648	0.0267169
1042.79266	102.29064	97.50702	0.23287	0.22168	1	240.93985	6.16015	2.096421	0.0274531	142.793	0.0274531
1047.92116	102.80466	97.48612	0.23257	0.22029	1	240.88820	6.21180	2.148065	0.0281293	147.921	0.0281293
1053.06113	103.31869	97.46578	0.23276	0.21888	1	240.83794	6.26206	2.198325	0.0287875	153.061	0.0287875
1058.2039	103.83271	97.44738	0.23252	0.21747	1	240.79248	6.30752	2.243792	0.0293829	158.204	0.0293829
1063.3427	104.34673	97.42684	0.23141	0.21604	1	240.74172	6.35828	2.294546	0.03004	163.343	0.0300475

7									75			
1068.48549	104.86076	97.40752	0.23077	0.2146	1	240.69398	6.40602	2.342286	0.0306727		168.485	0.0306727
1073.6214	105.37478	97.38899	0.22886	0.21315	1	240.64819	6.45181	2.388073	0.0312723		173.621	0.0312723
1078.77004	105.8888	97.37206	0.22641	0.2117	1	240.60636	6.49364	2.429907	0.0318201		178.770	0.0318201
1083.90286	106.40283	97.35717	0.22654	0.21023	1	240.56957	6.53043	2.466700	0.0323019		183.903	0.0323019
1089.05547	106.91685	97.34377	0.22574	0.20875	1	240.53646	6.56354	2.499812	0.0327355		189.055	0.0327355
1094.18663	107.43087	97.32898	0.2237	0.20727	1	240.49991	6.60009	2.536358	0.0332141		194.187	0.0332141
1099.3361	107.9449	97.31339	0.22287	0.20578	1	240.46139	6.63861	2.574881	0.0337186		199.336	0.0337186
1104.48033	108.45892	97.30154	0.22201	0.20427	1	240.43211	6.66789	2.604162	0.034102		204.480	0.034102
1109.61612	108.97294	97.28593	0.22133	0.20277	1	240.39353	6.70647	2.642735	0.0346071		209.616	0.0346071
1114.76216	109.48697	97.27416	0.22154	0.20125	1	240.36445	6.73555	2.671818	0.034988		214.762	0.034988
1119.89215	110.00099	97.25943	0.2209	0.19973	1	240.32805	6.77195	2.708216	0.0354646		219.892	0.0354646
1125.0356	110.51501	97.24602	0.21944	0.19819	1	240.29492	6.80508	2.741352	0.0358986		225.036	0.0358986
1130.15947	111.02904	97.23119	0.21981	0.19666	1	240.25827	6.84173	2.777997	0.0363784		230.159	0.0363784
1135.32043	111.54306	97.21872	0.21887	0.19511	1	240.22746	6.87254	2.808810	0.0367819		235.320	0.0367819
1140.45134	112.05708	97.20525	0.21912	0.19356	1	240.19417	6.90583	2.842095	0.0372178		240.451	0.0372178

APPENDIX 20: Data for the reactivity of Vietnamese anthracite at 1190°C.

Temp./-C	Time/min	Mass/%	DTA/(mW/mg)	Sensit./(t V/mW)	Segment	mg change	mg evolved	CO evolved	%R	%R(adj)	lf(X)	Pf(X)	ti(model)	ti(exp)
1188.38 726	116.84 212	96.916 89	0.38806	0.17881	1	241.22614	7.67386	3.34459	0	0	0	0	0	0
1190.99 293	117.31 516	96.898 93	0.39851	0.178	2	241.18144	7.71856	3.38930	0.0033 193	0.000134 826	4.494 E-05	6.06E-09	0.2230385	0.47304
1191.74 938	117.78 821	96.875 88	0.55758	0.17776	2	241.12407	7.77593	3.44667	0.0040 679	0.000829 585	0.0002 766	2.295E-07	1.392048	0.94609
1191.13 201	118.26 125	96.859 37	0.68526	0.17796	2	241.08297	7.81703	3.48776	0.0046 042	0.001327 219	0.0004 426	5.875E-07	2.2496566	1.41913
1190.98 109	118.73 43	96.842 44	0.69673	0.178	2	241.04083	7.85917	3.52990	0.0051 541	0.001837 513	0.0006 129	1.126E-06	3.1466769	1.89218
1190.84 893	119.20 734	96.827 95	0.7004	0.17804	2	241.00477	7.89523	3.56597	0.0056 247	0.002274 261	0.0007 587	1.726E-06	3.9285746	2.36522
1190.75 292	119.68 039	96.813 07	0.70708	0.17807	2	240.96773	7.93227	3.60300	0.0061 08	0.002722 765	0.0009 084	2.474E-06	4.7451168	2.83827
1190.63 161	120.15 343	96.799 23	0.71301	0.17811	2	240.93328	7.96672	3.63745	0.0065 575	0.003139 922	0.0010 477	3.291E-06	5.516965	3.31131
1190.54 622	120.62 648	96.787 28	0.71764	0.17814	2	240.90354	7.99646	3.66719	0.0069 456	0.003500 112	0.0011 681	4.09E-06	6.1930104	3.78436
1190.47 401	121.09 952	96.775 31	0.72288	0.17816	2	240.87375	8.02625	3.69699	0.0073 344	0.003860 904	0.0012 886	4.977E-06	6.8791117	4.2574
1190.39 295	121.57 257	96.763 91	0.72809	0.17819	2	240.84537	8.05463	3.72536	0.0077 047	0.004204 516	0.0014 035	5.904E-06	7.5408496	4.73045
1190.33 12	122.04 561	96.752 57	0.73369	0.17821	2	240.81715	8.08285	3.75359	0.0080 73	0.004546 319	0.0015 177	6.904E-06	8.2071499	5.20349
1190.29 48	122.51 866	96.740 33	0.73826	0.17822	2	240.78668	8.11332	3.78405	0.0084 706	0.004915 25	0.0016 411	8.071E-06	8.9353402	5.67654
1190.25 193	122.99 17	96.729 69	0.74345	0.17823	2	240.76020	8.13980	3.81053	0.0088 162	0.005235 954	0.0017 484	9.16E-06	9.5759444	6.14958
1190.20 118	123.46 475	96.720 2	0.74954	0.17825	2	240.73658	8.16342	3.83416	0.0091 244	0.005521 996	0.0018 441	1.019E-05	10.153279	6.62263
1190.17 604	123.93 779	96.711 61	0.75406	0.17825	2	240.71520	8.18480	3.85554	0.0094 034	0.005780 91	0.0019 307	1.117E-05	10.680714	7.09567
1190.15 628	124.41 084	96.702 69	0.75988	0.17826	2	240.69300	8.20700	3.87774	0.0096 931	0.006049 771	0.0020 207	1.223E-05	11.233296	7.56872
1190.12 725	124.88 388	96.692 81	0.76536	0.17827	2	240.66840	8.23160	3.90233	0.0100 14	0.006347 568	0.0021 203	1.347E-05	11.851157	8.04176
1190.10 362	125.35 693	96.684 06	0.76947	0.17828	2	240.64663	8.25337	3.92411	0.0102 982	0.006611 305	0.0022 086	1.461E-05	12.403453	8.51481
1190.09 384	125.82 997	96.674 31	0.77502	0.17828	2	240.62236	8.27764	3.94838	0.0106 149	0.006905 184	0.0023 07	1.594E-05	13.024514	8.98785
1190.06 997	126.30 302	96.665 24	0.78112	0.17829	2	240.59978	8.30022	3.97095	0.0109 095	0.007178 566	0.0023 986	1.723E-05	13.607605	9.4609
1190.06 011	126.77 606	96.656 2	0.78608	0.17829	2	240.57728	8.32272	3.99345	0.0112 031	0.007451 044	0.0024 899	1.857E-05	14.193895	9.93394
1190.04 85	127.24 911	96.647 11	0.79089	0.17829	2	240.55466	8.34534	4.01608	0.0114 984	0.007725 03	0.0025 817	1.996E-05	14.788593	10.40699
1190.03 84	127.72 215	96.639 39	0.79578	0.1783	2	240.53544	8.36456	4.03529	0.0117 491	0.007957 721	0.0026 596	2.118E-05	15.297728	10.88003
1190.03 001	128.19 52	96.631 42	0.80166	0.1783	2	240.51560	8.38440	4.05513	0.0120 08	0.008197 948	0.0027 402	2.248E-05	15.827272	11.35308
1190.01 486	128.66 824	96.623 51	0.80685	0.1783	2	240.49592	8.40408	4.07482	0.0122 649	0.008436 366	0.0028 201	2.381E-05	16.35677	11.82612
1190.03 245	129.14 129	96.615 61	0.81073	0.1783	2	240.47625	8.42375	4.09448	0.0125 215	0.008674 483	0.0028 999	2.518E-05	16.889517	12.29917
1190.01 708	129.61 433	96.607 61	0.81659	0.1783	2	240.45634	8.44366	4.11439	0.0127 813	0.008915 614	0.0029 807	2.66E-05	17.433001	12.77221
1189.99 956	130.08 738	96.600 03	0.82179	0.17831	2	240.43747	8.46253	4.13326	0.0130 275	0.009144 086	0.0030 574	2.799E-05	17.951659	13.24526
1190.00 546	130.56 042	96.593 95	0.82718	0.17831	2	240.42234	8.47766	4.14839	0.0132 25	0.009327 346	0.0031 188	2.912E-05	18.370289	13.7183
1190.00 901	131.03 347	96.587 22	0.83209	0.17831	2	240.40559	8.49441	4.16514	0.0134 436	0.009530 197	0.0031 869	3.04E-05	18.836382	14.19135

1190.00 515	131.50 651	96.579 26	0.83736	0.17831	2	240.38578	8.51422	4.18495	0.0137 021	0.009770 123	0.0032 674	3.196E-05	19.391335	14.66439
1189.99 733	131.97 956	96.572 43	0.8431	0.17831	2	240.36878	8.53122	4.20195	0.0139 24	0.009975 988	0.0033 364	3.332E-05	19.870682	15.13744
1190.00 796	132.45 26	96.565 97	0.84846	0.17831	2	240.35270	8.54730	4.21803	0.0141 338	0.010170 702	0.0034 018	3.464E-05	20.326761	15.61048
1190.00 109	132.92 565	96.558 91	0.85383	0.17831	2	240.33513	8.56487	4.23561	0.0143 631	0.010383 5	0.0034 732	3.611E-05	20.828202	16.08353
1190.00 095	133.39 869	96.552 55	0.85893	0.17831	2	240.31930	8.58070	4.25144	0.0145 697	0.010575 199	0.0035 376	3.745E-05	21.28261	16.55657
1189.98 291	133.87 174	96.545 36	0.86462	0.17831	2	240.30140	8.59860	4.26933	0.0148 032	0.010791 915	0.0036 103	3.901E-05	21.799386	17.02962
1189.98 907	134.34 478	96.538 2	0.87002	0.17831	2	240.28358	8.61642	4.28715	0.0150 357	0.011007 728	0.0036 828	4.059E-05	22.31724	17.50266
1189.99 192	134.81 783	96.531 24	0.8753	0.17831	2	240.26626	8.63374	4.30448	0.0152 618	0.011217 512	0.0037 532	4.215E-05	22.823723	17.97571
1189.98 964	135.29 087	96.525 7	0.88061	0.17831	2	240.25247	8.64753	4.31827	0.0154 417	0.011384 495	0.0038 093	4.342E-05	23.229053	18.44875
1189.99 198	135.76 392	96.519 39	0.88541	0.17831	2	240.23676	8.66324	4.33397	0.0156 467	0.011574 687	0.0038 732	4.489E-05	23.693075	18.9218
1190.00 415	136.23 696	96.513 79	0.88983	0.17831	2	240.22282	8.67718	4.34791	0.0158 286	0.011743 479	0.0039 299	4.621E-05	24.106987	19.39484
1189.99 436	136.71 001	96.506 65	0.89538	0.17831	2	240.20505	8.69495	4.36568	0.0160 605	0.011958 689	0.0040 022	4.793E-05	24.637591	19.86789
1189.99 459	137.18 305	96.501 18	0.90081	0.17831	2	240.19144	8.70856	4.37930	0.0162 382	0.012123 562	0.0040 576	4.926E-05	25.046265	20.34093
1190.00 577	137.65 61	96.495 61	0.90613	0.17831	2	240.17757	8.72243	4.39316	0.0164 191	0.012291 449	0.0041 141	5.064E-05	25.46435	20.81398
1189.98 696	138.12 914	96.489 25	0.91231	0.17831	2	240.16174	8.73826	4.40899	0.0166 256	0.012483 149	0.0041 785	5.223E-05	25.944125	21.28702
1189.99 597	138.60 219	96.482 13	0.91714	0.17831	2	240.14402	8.75598	4.42671	0.0168 569	0.012697 755	0.0042 506	5.405E-05	26.48426	21.76007
1189.99 493	139.07 523	96.476 58	0.92266	0.17831	2	240.13021	8.76979	4.44053	0.0170 372	0.012865 04	0.0043 069	5.549E-05	26.907511	22.23311
1190.00 67	139.54 828	96.471 05	0.92763	0.17831	2	240.11644	8.78356	4.45429	0.0172 168	0.013031 722	0.0043 629	5.694E-05	27.331172	22.70616
1190.00 266	140.02 132	96.464 72	0.93301	0.17831	2	240.10069	8.79931	4.47004	0.0174 224	0.013222 517	0.0044 271	5.862E-05	27.818491	23.1792
1189.98 891	140.49 437	96.459 13	0.9381	0.17831	2	240.08677	8.81323	4.48396	0.0176 039	0.013391 007	0.0044 837	6.013E-05	28.250945	23.65225
1190.00 163	140.96 741	96.454 3	0.94331	0.17831	2	240.07475	8.82525	4.49598	0.0177 608	0.013536 59	0.0045 327	6.145E-05	28.626194	24.12529

APPENDIX 21: Data for the reactivity of Vietnamese anthracite at 1240°C.

Temp./- C	Time/ min	Mass/ %	DTA/(mW/ mg)	Sensit./( $\neq$ V/mW)	Segm ent	mg change	mg evolved	CO evolved	%R	%R(adj)	lf(X)	Pf(X)	ti(model)	ti(exp)
1240.37 961	122.21 081	96.434 51	0.38559	0.16246	2	239.4468 883	8.853111 67	4.153463 08	0	0	0	0	0	0
1241.63 232	122.69 385	96.388 62	0.52434	0.16206	2	239.3329 435	8.967056 54	4.267407 95	0.0035591	0.003559 087	0.0011 878	4.229E-06	3.377358	0.48304
1240.94 101	123.17 69	96.361 38	0.65651	0.16228	2	239.2653 065	9.034693 46	4.335044 87	0.0044417	0.004441 708	0.0014 828	6.589E-06	4.216685	0.96609
1240.82 388	123.65 995	96.333 43	0.66199	0.16232	2	239.1959 067	9.104093 31	4.404444 72	0.0053473	0.005347 334	0.0017 856	9.554E-06	5.078623 4	1.44914
1240.69 251	124.14 299	96.304 25	0.67712	0.16236	2	239.1234 528	9.176547 25	4.476898 66	0.0062928	0.006292 814	0.0021 02	1.324E-05	5.979288 3	1.93218
1240.58 92	124.62 604	96.279 3	0.68511	0.16239	2	239.0615 019	9.238498 1	4.538849 51	0.0071012	0.007101 235	0.0023 727	1.686E-05	6.750035 7	2.41523
1240.48 934	125.10 909	96.256 21	0.69018	0.16243	2	239.0041 694	9.295830 57	4.596181 98	0.0078494	0.007849 389	0.0026 233	2.061E-05	7.463855	2.89828
1240.41 955	125.59 213	96.232 12	0.69345	0.16245	2	238.9443 54	9.355646 04	4.655997 45	0.0086299	0.008629 944	0.0028 85	2.492E-05	8.209133 1	3.38132
1240.34 485	126.07 518	96.210 85	0.69879	0.16247	2	238.8915 406	9.408459 45	4.708810 86	0.0093191	0.009319 127	0.0031 161	2.907E-05	8.867630 7	3.86437
1240.28 806	126.55 823	96.190 67	0.70404	0.16249	2	238.8414 336	9.458566 39	4.758917 8	0.009973	0.009972 992	0.0033 354	3.33E-05	9.492784 5	4.34742
1240.24 606	127.04 127	96.170 82	0.70872	0.1625	2	238.7921 461	9.507853 94	4.808205 35	0.0106162	0.010616 165	0.0035 513	3.775E-05	10.10809 7	4.83046
1240.20 523	127.52 432	96.151 31	0.71408	0.16252	2	238.7437 027	9.556297 27	4.856648 68	0.0112483	0.011248 321	0.0037 636	4.239E-05	10.71323 9	5.31351
1240.15 881	128.00 737	96.135 35	0.71856	0.16253	2	238.7040 741	9.595925 95	4.896277 36	0.0117655	0.011765 451	0.0039 373	4.638E-05	11.20854 4	5.79656
1240.12 602	128.49 041	96.118 3	0.72304	0.16254	2	238.6617 389	9.638261 1	4.938612 51	0.0123179	0.012317 899	0.0041 229	5.086E-05	11.73794 6	6.2796
1240.10 664	128.97 346	96.100 03	0.72751	0.16255	2	238.6163 745	9.683625 51	4.983976 92	0.0129099	0.012909 877	0.0043 219	5.588E-05	12.30554 1	6.76265
1240.09 095	129.45 651	96.083 91	0.73196	0.16255	2	238.5763 485	9.723651 47	5.024002 88	0.0134322	0.013432 192	0.0044 976	6.05E-05	12.80660 9	7.2457
1240.08 924	129.93 955	96.066 5	0.73683	0.16255	2	238.5331 195	9.766880 5	5.067231 91	0.0139963	0.013996 305	0.0046 874	6.571E-05	13.34805 7	7.72874
1240.07 301	130.42 26	96.050 47	0.74141	0.16256	2	238.4933 17	9.806682 99	5.107034 4	0.0145157	0.014515 703	0.0048 622	7.069E-05	13.84684 7	8.21179
1240.05 858	130.90 565	96.034 86	0.74564	0.16256	2	238.4545 574	9.845442 62	5.145794 03	0.0150215	0.015021 493	0.0050 324	7.572E-05	14.33280 7	8.69484
1240.03 562	131.38 869	96.018 3	0.75062	0.16257	2	238.4134 389	9.886561 1	5.186912 51	0.0155581	0.015558 064	0.0052 132	8.125E-05	14.84859 9	9.17788
1240.03 455	131.87 174	96.005 87	0.75556	0.16257	2	238.3825 752	9.917424 79	5.217776 2	0.0159608	0.015960 816	0.0053 488	8.552E-05	15.23593 2	9.66093
1240.03 145	132.35 479	95.982 7	0.76012	0.16257	2	238.3250 441	9.974955 9	5.275307 31	0.0167116	0.016711 562	0.0056 018	9.379E-05	15.95832 9	10.14398
1240.01 084	132.83 783	95.969 21	0.76573	0.16258	2	238.2915 484	10.00845 157	5.308802 98	0.0171487	0.017148 661	0.0057 492	9.878E-05	16.37916 3	10.62702
1240.01 032	133.32 088	95.962 46	0.7715	0.16258	2	238.2747 882	10.02521 182	5.325563 23	0.0173674	0.017367 372	0.0058 23	0.0001013	16.58980 2	11.11007
1240.00 489	133.80 393	95.946 52	0.77578	0.16258	2	238.2352 092	10.06479 084	5.365142 25	0.0178839	0.017883 854	0.0059 972	0.0001075	17.08739 9	11.59312
1239.99 89	134.28 697	95.932 13	0.78111	0.16258	2	238.1994 788	10.10052 121	5.400872 62	0.0183501	0.018350 114	0.0061 545	0.0001132	17.53682 2	12.07616
1240.00 432	134.77 002	95.919 07	0.78619	0.16258	2	238.1670 508	10.13294 919	5.433300 6	0.0187733	0.018773 279	0.0062 973	0.0001185	17.94488 2	12.55921
1239.99 766	135.25 307	95.905 5	0.79115	0.16258	2	238.1333 565	10.16664 35	5.466994 91	0.019213	0.019212 969	0.0064 458	0.0001241	18.36905 2	13.04226
1239.99 05	135.73 611	95.892 34	0.79576	0.16258	2	238.1006 802	10.19931 978	5.499671 19	0.0196394	0.019639 375	0.0065 898	0.0001297	18.78057 9	13.5253
1239.99 258	136.21 916	95.878 39	0.80072	0.16258	2	238.0660 424	10.23395 763	5.534309 04	0.0200914	0.020091 378	0.0067 425	0.0001358	19.21699 3	14.00835
1239.99 288	136.70 221	95.863 99	0.80589	0.16258	2	238.0302 872	10.26971 283	5.570064 24	0.020558	0.020557 962	0.0069 002	0.0001422	19.66768 5	14.4914

1240.00	137.18	95.851	0.81052	0.16258	2	237.9989	10.30109	5.601449	0.0209675	0.020967	0.0070	0.0001479	20.06346	14.97444
421	525	35				021	795	36		518	386			
1240.00	137.66	95.839	0.81534	0.16258	2	237.9691	10.33089	5.631245	0.0213563	0.021356	0.0071	0.0001535	20.43934	15.45749
478	83	35				061	395	36		338	701			
1239.99	138.15	95.826	0.82119	0.16258	2	237.9377	10.36222	5.662580	0.0217652	0.021765	0.0073	0.0001595	20.83479	15.94054
21	135	73				706	941	82		247	084		2	
1239.98	138.63	95.813	0.82618	0.16259	2	237.9039	10.39607	5.696424	0.0222069	0.022206	0.0074	0.000166	21.26206	16.42358
357	439	1				273	27	11		881	578		8	
1240.00	139.11	95.799	0.83027	0.16258	2	237.8707	10.42927	5.729621	0.0226401	0.022640	0.0076	0.0001726	21.68137	16.90663
582	744	73				296	041	82		091	044			
1240.00	139.60	95.787	0.83573	0.16258	2	237.8401	10.45986	5.760212	0.0230393	0.023039	0.0077	0.0001788	22.06789	17.38968
273	049	41				39	097	38		28	395		8	
1239.99	140.08	95.775	0.84035	0.16258	2	237.8098	10.49010	5.790455	0.0234339	0.023433	0.0078	0.000185	22.45018	17.87272
421	353	23				961	391	32		932	731			
1239.99	140.56	95.763	0.84499	0.16258	2	237.7802	10.51975	5.820102	0.0238208	0.023820	0.0080	0.0001912	22.82507	18.35577
181	658	29				491	093	34		807	042		1	
1239.99	141.04	95.749	0.85052	0.16258	2	237.7466	10.55337	5.853722	0.0242595	0.024259	0.0081	0.0001983	23.25036	18.83882
095	963	75				293	075	16		526	528		8	
1240.00	141.53	95.737	0.85606	0.16258	2	237.7163	10.58368	5.884039	0.0246551	0.024655	0.0082	0.0002049	23.63404	19.32186
337	267	54				118	818	59		15	869		3	
1239.99	142.01	95.726	0.86051	0.16258	2	237.6890	10.61092	5.911278	0.0250106	0.025010	0.0084	0.0002109	23.97887	19.80491
824	572	57				733	669	1		596	074		9	
1239.99	142.49	95.713	0.86501	0.16258	2	237.6576	10.64233	5.942688	0.0254205	0.025420	0.0085	0.0002179	24.37667	20.28796
583	877	92				634	664	05		477	463		2	
1240.00	142.98	95.701	0.87011	0.16258	2	237.6267	10.67329	5.973651	0.0258245	0.025824	0.0086	0.0002249	24.76895	20.771
125	181	45				004	965	06		525	834		9	
1239.99	143.46	95.689	0.87507	0.16258	2	237.5966	10.70331	6.003670	0.0262163	0.026216	0.0088	0.0002318	25.14943	21.25405
138	486	36				809	912	53		261	163		7	
1239.99	143.94	95.677	0.87977	0.16258	2	237.5664	10.73353	6.033888	0.0266106	0.026610	0.0089	0.0002389	25.53257	21.7371
751	791	19				628	723	64		589	501		9	
1239.99	144.43	95.665	0.88416	0.16258	2	237.5362	10.76373	6.064081	0.0270046	0.027004	0.0090	0.000246	25.91555	22.22014
538	095	03				695	051	92		593	838		3	
1239.98	144.91	95.652	0.88935	0.16258	2	237.5061	10.79387	6.094225	0.0273979	0.027397	0.0092	0.0002533	26.29804	22.70319
71	4	89				259	413	54		949	173		1	
1239.99	145.39	95.640	0.89432	0.16258	2	237.4757	10.82424	6.124592	0.0277942	0.027794	0.0093	0.0002607	26.68351	23.18624
842	705	66				588	122	63		221	519		3	
1240.01	145.88	95.629	0.89825	0.16258	2	237.4470	10.85296	6.153320	0.0281691	0.028169	0.0094	0.0002679	27.04831	23.66928
175	009	09				305	953	94		108	793		9	
1240.00	146.36	95.617	0.90374	0.16258	2	237.4192	10.88072	6.181080	0.0285314	0.028531	0.0096	0.0002748	27.40095	24.15233
416	314	91				705	947	88		358	024		3	
1239.99	146.84	95.605	0.90853	0.16258	2	237.3891	10.91089	6.211249	0.028925	0.028925	0.0097	0.0002825	27.78432	24.63538
79	619	76				021	792	33		038	362		3	
1240.01	147.32	95.594	0.91327	0.16258	2	237.3610	10.93890	6.239257	0.0292905	0.029290	0.0098	0.0002898	28.14037	25.11842
113	923	48				938	616	57		529	604		3	
1239.99	147.81	95.581	0.9185	0.16258	2	237.3277	10.97220	6.272554	0.029725	0.029725	0.0100	0.0002985	28.56382	25.60147
367	228	07				968	319	6		035	082			
1239.99	148.29	95.568	0.92426	0.16258	2	237.2966	11.00338	6.303741	0.030132	0.030132	0.0101	0.0003068	28.96058	26.08452
468	533	51				103	967	08			466		8	
1239.98	148.77	95.556	0.92861	0.16259	2	237.2662	11.03370	6.334058	0.0305276	0.030527	0.0102	0.0003149	29.34645	26.56756
23	837	3				929	71	51		624	812			
1239.99	149.26	95.545	0.93242	0.16258	2	237.2395	11.06049	6.360850	0.0308772	0.030877	0.0104	0.0003222	29.68755	27.05061
646	142	51				013	867	08		237	002		9	

APPENDIX 22: Data for the reactivity of Vietnamese anthracite at 1290°C.

Temp./- C	Time/ min	Mass/ %	DTA/(mW/ mg)	Sensit./(† V/mW)	Segm ent	mg change	mg evolved	CO evolved	%R	%R(adj)	lf(X)	Pf(X)	ti(model)	ti(exp)
1289.57 904	126.95 971	96.1173 6	0.32687	0.14691	1	239.13999	9.66001	5.27993	0	0	0	0	0	0
1291.32 882	127.45 372	96.0554 9	0.36335	0.14636	2	238.98606	9.81394	5.43387	0.0001 533	0.003315 929	0.0011 065	3.671E-06	0.4298384	0.49401
1290.94 088	127.94 772	96.0025 7	0.57647	0.14648	2	238.85439	9.94561	5.56553	0.0018 646	0.016822 163	0.0056 391	9.504E-05	2.1941117	0.98801
1290.71 532	128.44 173	95.9519 3	0.62424	0.14656	2	238.72840	10.0716 0	5.69152	0.0035 022	0.025340 8	0.0085 193	0.0002165	3.318157	1.48202
1290.59 819	128.93 574	95.9022 8	0.62502	0.14659	2	238.60487	10.1951 3	5.81505	0.0051 077	0.032385 384	0.0109 138	0.0003547	4.2543968	1.97603
1290.49 978	129.42 974	95.8536 6	0.63079	0.14662	2	238.48391	10.3160 9	5.93602	0.0066 8	0.038557 132	0.0130 212	0.0005042	5.0796772	2.47003
1290.40 278	129.92 375	95.8099 3	0.63713	0.14666	2	238.37503	10.4249 7	6.04489	0.0080 951	0.043686 197	0.0147 794	0.0006488	5.7691498	2.96404
1290.32 217	130.41 776	95.7652 4	0.64274	0.14668	2	238.26392	10.5360 8	6.15601	0.0095 393	0.048605 508	0.0164 717	0.000805	6.4335402	3.45805
1290.25 474	130.91 176	95.7224 4	0.64638	0.1467	2	238.15743	10.6425 7	6.26250	0.0109 233	0.053080 02	0.0180 16	0.000962	7.0405263	3.95205
1290.22 1	131.40 577	95.6802 5	0.65167	0.14671	2	238.05246	10.7475 4	6.36746	0.0122 877	0.057300 061	0.0194 769	0.0011233	7.6153399	4.44606
1290.18 177	131.89 978	95.6381 3	0.65791	0.14672	2	237.94767	10.8523 3	6.47226	0.0136 497	0.061352 255	0.0208 839	0.0012902	8.1694511	4.94007
1290.15 999	132.39 378	95.5970 5	0.663	0.14673	2	237.84546	10.9545 4	6.57447	0.0149 782	0.065170 024	0.0222 131	0.0014583	8.6934554	5.43407
1290.11 744	132.88 779	95.5563 2	0.66954	0.14674	2	237.74412	11.0558 8	6.67580	0.0162 953	0.068839 85	0.0234 943	0.00163	9.1989482	5.92808
1290.09 523	133.38 18	95.5151 6	0.67497	0.14675	2	237.64172	11.1582 8	6.77821	0.0176 263	0.072444 336	0.0247 559	0.0018082	9.6971637	6.42209
1290.06 873	133.87 58	95.4743 1	0.68132	0.14676	2	237.54008	11.2599 2	6.87984	0.0189 473	0.075928 591	0.0259 786	0.0019896	10.180394	6.91609
1290.06 196	134.36 981	95.4337 1	0.68618	0.14676	2	237.43907	11.3609 3	6.98086	0.0202 602	0.079308 205	0.0271 675	0.0021741	10.650654	7.4101
1290.04 217	134.86 382	95.3945 6	0.69271	0.14677	2	237.34167	11.4583 3	7.07826	0.0215 262	0.082495 21	0.0282 913	0.0023559	11.095513	7.90411
1290.03 76	135.35 782	95.3537 3	0.69922	0.14677	2	237.24008	11.5599 2	7.17985	0.0228 465	0.085749 833	0.0294 416	0.0025494	11.551221	8.39811
1290.02 339	135.85 183	95.3134 2	0.70529	0.14677	2	237.13979	11.6602 1	7.28014	0.0241 501	0.088899 014	0.0305 572	0.0027442	11.993528	8.89212
1290.02 646	136.34 584	95.2720 8	0.71227	0.14677	2	237.03694	11.7630 6	7.38299	0.0254 869	0.092067 451	0.0316 823	0.0029477	12.439902	9.38613
1290.01 498	136.83 984	95.2300 2	0.71781	0.14678	2	236.93229	11.8677 1	7.48764	0.0268 47	0.095231 913	0.0328 086	0.0031586	12.887087	9.88013
1290.00 157	137.33 385	95.1892 9	0.72269	0.14678	2	236.83095	11.9690 5	7.58897	0.0281 641	0.098243 241	0.0338 828	0.0033663	13.31391	10.37414
1290.01 438	137.82 786	95.1481 7	0.72874	0.14678	2	236.72865	12.0713 5	7.69128	0.0294 939	0.101233 798	0.0349 52	0.0035795	13.739029	10.86815
1290.01 617	138.32 186	95.1044 6	0.73446	0.14678	2	236.61990	12.1801 0	7.80003	0.0309 073	0.104361 428	0.0360 727	0.0038098	14.184964	11.36215
1290.00 116	138.81 587	95.0627 7	0.74063	0.14678	2	236.51617	12.2838 3	7.90375	0.0322 555	0.107298 183	0.0371 274	0.004033	14.604929	11.85616
1290.00 301	139.30 988	95.0209 7	0.7458	0.14678	2	236.41217	12.3878 3	8.00775	0.0336 072	0.110199 856	0.0381 718	0.00426	15.021067	12.35017
1290.00 858	139.80 388	94.9775 4	0.75163	0.14678	2	236.30412	12.4958 8	8.11581	0.0350 116	0.113171 733	0.0392 438	0.0044994	15.448505	12.84417
1290.00 682	140.29 789	94.9356 8	0.75742	0.14678	2	236.19997	12.6000 3	8.21995	0.0363 653	0.115996 925	0.0402 652	0.0047333	15.856008	13.33818
1289.99 774	140.79 19	94.8946 8	0.76215	0.14678	2	236.09796	12.7020 4	8.32196	0.0376 911	0.118728 604	0.0412 548	0.0049654	16.251106	13.83219
1290.00 493	141.28 59	94.8512 6	0.76673	0.14678	2	235.98993	12.8100 7	8.42999	0.0390 952	0.121585 1	0.0422 917	0.0052145	16.665401	14.32619
1290.01 103	141.77 991	94.8085 5	0.77242	0.14678	2	235.88355	12.9164 5	8.53638	0.0404 78	0.124363 286	0.0433 025	0.0054629	17.069466	14.8202



1290.00 296	142.27 392	94.7672 6	0.77759	0.14678	2	235.78094	13.0190 6	8.63898	0.0418 116	0.127011 413	0.0442 679	0.0057054	17.455656	15.31421
1290.00 463	142.76 792	94.7243 5	0.78322	0.14678	2	235.67418	13.1258 2	8.74574	0.0431 992	0.129735 578	0.0452 63	0.0059608	17.853999	15.80821
1290.01 27	143.26 193	94.6827 9	0.78744	0.14678	2	235.57078	13.2292 2	8.84914	0.0445 431	0.132344 987	0.0462 182	0.0062109	18.23658	16.30222
1290.00 564	143.75 594	94.6407 3	0.79297	0.14678	2	235.46614	13.3338 6	8.95379	0.0459 033	0.134957 881	0.0471 766	0.0064669	18.620675	16.79623
1289.99 264	144.24 994	94.5985	0.7994	0.14678	2	235.36107	13.4389 3	9.05886	0.0472 689	0.137554 212	0.0481 308	0.0067267	19.003333	17.29023
1290.01 155	144.74 395	94.5563 4	0.80379	0.14678	2	235.25617	13.5438 3	9.16375	0.0486 322	0.140120 179	0.0490 758	0.0069889	19.382498	17.78424
1290.00 604	145.23 796	94.5133 3	0.80904	0.14678	2	235.14917	13.6508 3	9.27076	0.0500 231	0.142712 064	0.0500 322	0.0072592	19.76649	18.27825
1290.00 908	145.73 196	94.4711 4	0.81433	0.14678	2	235.04420	13.7558 0	9.37573	0.0513 874	0.145230 138	0.0509 632	0.007527	20.14051	18.77225
1290.00 457	146.22 597	94.4297 8	0.81903	0.14678	2	234.94129	13.8587 1	9.47863	0.0527 249	0.147676 058	0.0518 693	0.0077922	20.504726	19.26626
1289.99 558	146.71 998	94.3884 3	0.82372	0.14678	2	234.83841	13.9615 9	9.58151	0.0540 62	0.150099 772	0.0527 688	0.0080598	20.866527	19.76027
1289.99 929	147.21 398	94.3469 2	0.82967	0.14678	2	234.73514	14.0648 6	9.68479	0.0554 044	0.152511 85	0.0536 658	0.0083309	21.227477	20.25427
1290.00 751	147.70 799	94.3039 8	0.83528	0.14678	2	234.62830	14.1717 0	9.79162	0.0567 929	0.154985 596	0.0545 874	0.008614	21.598576	20.74828
1290.00 067	148.20 2	94.2626 5	0.83999	0.14678	2	234.52547	14.2745 3	9.89445	0.0581 295	0.157346 673	0.0554 688	0.008889	21.953648	21.24229
1290.00 515	148.69 6	94.2203 8	0.84614	0.14678	2	234.42031	14.3796 9	9.99962	0.0594 964	0.159741 877	0.0563 646	0.0091728	22.314729	21.73629
1289.99 353	149.19 001	94.1780 7	0.85163	0.14678	2	234.31504	14.4849 6	10.1048 9	0.0608 646	0.162120 137	0.0572 557	0.0094593	22.674133	22.2303
1290.00 386	149.68 402	94.1349 7	0.85695	0.14678	2	234.20781	14.5921 9	10.2121 2	0.0622 583	0.164523 64	0.0581 58	0.0097536	23.038245	22.72431
1289.99 902	150.17 802	94.0919 7	0.86223	0.14678	2	234.10082	14.6991 8	10.3191 0	0.0636 488	0.166902 872	0.0590 529	0.0100499	23.399566	23.21831
1290.00 143	150.67 203	94.0489 2	0.86819	0.14678	2	233.99371	14.8062 9	10.4262 1	0.0650 41	0.169266 714	0.0599 437	0.010349	23.759429	23.71232
1290.00 147	151.16 604	94.0040 9	0.87372	0.14678	2	233.88218	14.9178 2	10.5377 5	0.0664 907	0.171709 548	0.0608 66	0.010663	24.132242	24.20633
1289.99 362	151.66 004	93.9583	0.87938	0.14678	2	233.76825	15.0317 5	10.6516 8	0.0679 714	0.174185 525	0.0618 027	0.0109866	24.511076	24.70033
1290.00 063	152.15 405	93.9149 6	0.88456	0.14678	2	233.66042	15.1395 8	10.7595 1	0.0693 729	0.176511 69	0.0626 845	0.0112954	24.867875	25.19434

APPENDIX 23: Data for the reactivity of Vietnamese anthracite at 1340°C.

np./-C	Time/ min	Mass/ %	DTA/(mW /mg)	Sensit./(† V/mW)	Segm ent	mg change	mg evolved	CO evolved	%R	%R(adj)	lf(X)	Pf(X)	ti(model)	ti(exp)
1340.90 469	132.30 654	95.201 79	-1.48216	0.1309	2	235.148 42	11.85158	7.38157	0	0	0	0	0	0
1340.93 738	132.80 96	95.052 64	0.72792	0.13089	2	234.780 02	12.21998	7.74997	0.0033763	0.0033763 44	0.0011267	3.806E-06	0.2717433	0.50306
1340.57 28	133.31 267	94.954 13	0.39156	0.131	2	234.536 70	12.46330	7.99329	0.0065659	0.0065658 65	0.0021934	1.441E-05	0.5291832	1.00613
1340.47 888	133.81 574	94.844 3	0.48959	0.13103	2	234.265 42	12.73458	8.26457	0.0101219	0.0101219	0.0033854	3.431E-05	0.8170506	1.5092
1340.36 539	134.31 88	94.736 33	0.47629	0.13107	2	233.998 74	13.00126	8.53126	0.0136177	0.0136177 12	0.00456	6.219E-05	1.1009153	2.01226
1340.28 916	134.82 187	94.626 98	0.49239	0.13109	2	233.728 64	13.27136	8.80135	0.0171582	0.0171582 06	0.0057524	9.889E-05	1.3892949	2.51533
1340.23 712	135.32 494	94.515 97	0.49963	0.13111	2	233.454 45	13.54555	9.07555	0.0207524	0.0207524 47	0.0069659	0.0001449	1.6829703	3.0184
1340.18 333	135.82 8	94.404 81	0.51136	0.13112	2	233.179 88	13.82012	9.35011	0.0243515	0.0243515 44	0.008184	0.0001998	1.9779747	3.52146
1340.14 424	136.33 107	94.292 81	0.52018	0.13114	2	232.903 24	14.09676	9.62675	0.0279778	0.0279778 38	0.0094143	0.0002642	2.2761573	4.02453
1340.09 865	136.83 414	94.180 71	0.52813	0.13115	2	232.626 35	14.37365	9.90364	0.0316074	0.0316073 71	0.0106488	0.0003378	2.5755656	4.5276
1340.08 689	137.33 72	94.065 31	0.53595	0.13115	2	232.341 32	14.65868	10.1886 8	0.0353437	0.0353437 49	0.0119228	0.0004231	2.8847967	5.03066
1340.07 517	137.84 027	93.951 6	0.54423	0.13116	2	232.060 45	14.93955	10.4695 4	0.0390254	0.0390254 09	0.0131815	0.0005167	3.1905063	5.53373
1340.04 54	138.34 334	93.837 18	0.55253	0.13117	2	231.777 83	15.22217	10.7521 6	0.0427301	0.0427300 58	0.0144512	0.0006205	3.4991399	6.0368
1340.04 575	138.84 64	93.722 85	0.56145	0.13117	2	231.495 44	15.50456	11.0345 5	0.0464318	0.0464317 92	0.0157232	0.0007339	3.8085542	6.53986
1340.03 101	139.34 947	93.605 91	0.57043	0.13117	2	231.206 60	15.79340	11.3233 9	0.050218	0.0502180 32	0.0170276	0.0008599	4.126097	7.04293
1340.01 912	139.85 254	93.490 16	0.58031	0.13117	2	230.920 70	16.07930	11.6093 0	0.0539657	0.0539657 42	0.0183222	0.0009948	4.4414757	7.546
1340.01 128	140.35 56	93.373 38	0.59086	0.13118	2	230.632 25	16.36775	11.8977 4	0.0577468	0.0577468 02	0.0196318	0.0011411	4.7607436	8.04906
1340.00 459	140.85 867	93.255 81	0.60214	0.13118	2	230.341 85	16.65815	12.1881 4	0.0615534	0.0615534 4	0.0209538	0.0012988	5.083277	8.55213
1340.01 13	141.36 174	93.136 32	0.61277	0.13118	2	230.046 71	16.95329	12.4832 8	0.0654222	0.0654222 43	0.0223011	0.0014698	5.4122217	9.0552
1340.00 29	141.86 48	93.013 76	0.62579	0.13118	2	229.743 99	17.25601	12.7860 0	0.0693904	0.0693904 45	0.0236868	0.0016566	5.750824	9.55826
1340.00 971	142.36 787	92.887 73	0.63935	0.13118	2	229.432 69	17.56731	13.0973 0	0.073471	0.0734709 98	0.0251159	0.0018607	6.1002956	10.0613 3
1340.00 1	142.87 094	92.761 19	0.65222	0.13118	2	229.120 14	17.87986	13.4098 5	0.0775681	0.0775680 63	0.0265549	0.002078	6.4524987	10.5644
1339.99 817	143.37 4	92.629 86	0.66279	0.13118	2	228.795 75	18.20425	13.7342 4	0.0818202	0.0818202 17	0.028053	0.0023168	6.8194399	11.0674 6
1339.99 547	143.87 707	92.498 07	0.67356	0.13118	2	228.470 23	18.52977	14.0597 6	0.0860873	0.0860872 65	0.029561	0.0025699	7.1891164	11.5705 3
1340.00 083	144.38 014	92.364 79	0.68429	0.13118	2	228.141 03	18.85897	14.3889 6	0.0904026	0.0904025 55	0.0310908	0.0028398	7.5644609	12.0736
1339.99 727	144.88 32	92.229 3	0.695	0.13118	2	227.806 37	19.19363	14.7236 2	0.0947894	0.0947894	0.0326509	0.0031286	7.947575	12.5766 6
1339.99 494	145.38 627	92.092 09	0.70788	0.13118	2	227.467 46	19.53254	15.0625 3	0.0992319	0.0992319 34	0.034236	0.0034361	8.3371532	13.0797 3
1339.99 629	145.88 934	91.952 59	0.7204	0.13118	2	227.122 90	19.87710	15.4070 9	0.1037486	0.1037486 14	0.0358529	0.0037641	8.7348976	13.5828
1340.00 774	146.39 24	91.806 9	0.73111	0.13118	2	226.763 04	20.23696	15.7669 5	0.1084657	0.1084657 1	0.0375474	0.0041236	9.1520968	14.0858 6
1340.00 496	146.89 547	91.660 91	0.74265	0.13118	2	226.402 45	20.59755	16.1275 4	0.1131925	0.1131925 21	0.0392514	0.0045011	9.5720212	14.5889 3
1339.99 716	147.39 854	91.511 52	0.75318	0.13118	2	226.033 45	20.96655	16.4965 4	0.1180294	0.1180294 15	0.0410013	0.0049055	10.003676	15.092

1340.00 591	147.90 16	91.361 11	0.76477	0.13118	2	225.661 94	21.33806	16.8680 5	0.1228993	0.1228993 34	0.0427696	0.0053312	10.440288	15.5950 6
1339.99 596	148.40 467	91.208 51	0.77676	0.13118	2	225.285 02	21.71498	17.2449 7	0.1278402	0.1278401 6	0.0445704	0.0057825	10.885337	16.0981 3
1339.99 46	148.90 774	91.056 96	0.78824	0.13118	2	224.910 69	22.08931	17.6193 0	0.132747	0.1327469 9	0.0463655	0.0062499	11.329416	16.6012
1339.99 166	149.41 08	90.899 97	0.79901	0.13118	2	224.522 93	22.47707	18.0070 7	0.13783	0.1378299 54	0.0482323	0.0067546	11.791654	17.1042 6
1339.99 185	149.91 387	90.740 5	0.80983	0.13118	2	224.129 04	22.87097	18.4009 6	0.1429932	0.1429932 14	0.050136	0.0072888	12.263527	17.6073 3
1339.99 557	150.41 694	90.577 4	0.82077	0.13118	2	223.726 18	23.27382	18.8038 1	0.148274	0.1482740 06	0.052091	0.0078577	12.748597	18.1104
1340.00 757	150.92	90.412 34	0.83218	0.13118	2	223.318 48	23.68152	19.2115 1	0.1536183	0.1536182 57	0.0540778	0.0084569	13.242048	18.6134 6
1340.00 894	151.42 307	90.246 6	0.84401	0.13118	2	222.909 10	24.09090	19.6208 9	0.1589845	0.1589845 25	0.0560811	0.0090825	13.740143	19.1165 3
1340.00 758	151.92 614	90.079 5	0.85468	0.13118	2	222.496 37	24.50364	20.0336 3	0.1643948	0.1643948 27	0.0581096	0.0097377	14.245	19.6196
1340.00 518	152.42 92	89.910 8	0.86653	0.13118	2	222.079 68	24.92032	20.4503 2	0.1698569	0.1698569 33	0.0601664	0.0104244	14.757443	20.1226 6
1340.00 003	152.93 227	89.739 01	0.87723	0.13118	2	221.655 35	25.34465	20.8746 4	0.1754191	0.1754190 86	0.0622701	0.0111498	15.282145	20.6257 3
1340.00 137	153.43 534	89.565 73	0.88617	0.13118	2	221.227 35	25.77265	21.3026 4	0.1810295	0.1810294 82	0.0644017	0.0119085	15.814365	21.1288
1339.99 435	153.93 84	89.391 83	0.89623	0.13118	2	220.797 82	26.20218	21.7321 7	0.18666	0.1866599 51	0.0665507	0.0126975	16.351518	21.6318 6
1339.99 095	154.44 147	89.214 87	0.90668	0.13118	2	220.360 73	26.63927	22.1692 6	0.1923895	0.1923894 97	0.0687478	0.0135289	16.901273	22.1349 3
1339.99 622	154.94 454	89.038 34	0.91565	0.13118	2	219.924 70	27.07530	22.6052 9	0.1981051	0.1981051 19	0.0709499	0.0143873	17.452893	22.638
1339.99 562	155.44 76	88.859 17	0.92767	0.13118	2	219.482 15	27.51785	23.0478 4	0.2039062	0.2039062 19	0.0731956	0.0152885	18.01607	23.1410 6
1339.99 439	155.95 067	88.678 34	0.93586	0.13118	2	219.035 50	27.96450	23.4944 9	0.2097611	0.2097610 66	0.0754733	0.0162288	18.587881	23.6441 3
1339.99 946	156.45 374	88.497 74	0.94614	0.13118	2	218.589 42	28.41058	23.9405 7	0.2156085	0.2156084 66	0.0777593	0.0171992	19.162432	24.1472
1339.98 714	156.95 68	88.314 48	0.95575	0.13118	2	218.136 77	28.86323	24.3932 3	0.221542	0.2215419 9	0.0800906	0.018216	19.749028	24.6502 6
1339.99 818	157.45 987	88.133 67	0.96214	0.13118	2	217.690 16	29.30984	24.8398 3	0.2273962	0.2273961 89	0.0824024	0.0192514	20.331363	25.1533 3
1339.99 633	157.96 294	87.949 39	0.97215	0.13118	2	217.234 99	29.76501	25.2950 0	0.2333627	0.2333627 39	0.0847706	0.0203398	20.928579	25.6564
1339.99 067	158.46 6	87.764 74	0.98066	0.13118	2	216.778 91	30.22109	25.7510 8	0.2393413	0.2393412 68	0.0871559	0.0214643	21.53079	26.1594 6
1339.99 984	158.96 907	87.582 69	0.98767	0.13118	2	216.329 24	30.67076	26.2007 5	0.2452356	0.2452356 15	0.0895199	0.0226066	22.12829	26.6625 3

APPENDIX 24: Data for the reactivity of Vietnamese anthracite at 1390°C.

Temp./- min	Time/ min	Mass/ %	DTA/(mW /mg)	Sensit./(† V/mW)	Segm ent	mg change	mg evolved	CO evolved	%R	%R(adj)	If(X)	Pf(X)	ti(model)	ti(exp)
1391.05 548	137.24 423	93.564 83	0.68599	0.11572	2	231.198 69	15.90131	11.83757	0	0	0	0	0	0
1390.70 491	137.75 825	93.256 97	0.84691	0.11582	2	230.437 97	16.66203	12.59829	0.0273 612	0.004525887	0.0015 109	6.842E-06	0.2840369	0.51402
1390.45 149	138.27 227	92.939 22	1.02579	0.1159	2	229.652 81	17.44719	13.38345	0.0376 431	0.007303442	0.0024 404	1.784E-05	0.4589139	1.02804
1390.34 564	138.78 63	92.613 67	1.05297	0.11593	2	228.848 38	18.25162	14.18789	0.0481 773	0.010574594	0.0035 374	3.745E-05	0.6654195	1.54207
1390.27 057	139.30 032	92.279 42	1.0951	0.11595	2	228.022 45	19.07755	15.01382	0.0589 93	0.014328517	0.0047 992	6.887E-05	0.9031411	2.05609
1390.18 95	139.81 434	91.939 52	1.13319	0.11597	2	227.182 55	19.91745	15.85371	0.0699 916	0.018516932	0.0062 108	0.0001152	1.1693151	2.57011
1390.15 163	140.32 837	91.589 38	1.16847	0.11599	2	226.317 36	20.78264	16.71891	0.0813 215	0.023190405	0.0077 907	0.0001811	1.46749	3.08414
1390.11 07	140.84 239	91.237 45	1.19974	0.116	2	225.447 74	21.65226	17.58853	0.0927 094	0.028228347	0.0094 994	0.000269	1.7903177	3.59816
1390.07 966	141.35 641	90.881 05	1.23035	0.11601	2	224.567 07	22.53293	18.46919	0.1042 419	0.033656052	0.0113 47	0.0003833	2.1397587	4.11218
1390.05 112	141.87 044	90.515 53	1.25869	0.11602	2	223.663 87	23.43613	19.37239	0.1160 694	0.039543657	0.0133 589	0.0005306	2.5207465	4.62621
1390.03 047	142.38 446	90.144 99	1.28583	0.11602	2	222.748 27	24.35173	20.28800	0.1280 595	0.045826588	0.0155 15	0.0007147	2.929562	5.14023
1390.01 796	142.89 848	89.771 42	1.3134	0.11603	2	221.825 18	25.27482	21.21109	0.1401 475	0.052466029	0.0178 038	0.0009396	3.364121	5.65425
1390.01 206	143.41 251	89.391 26	1.33731	0.11603	2	220.885 80	26.21420	22.15046	0.1524 488	0.059523193	0.0202 483	0.0012134	3.8289213	6.16828
1390.00 689	143.92 653	89.009 63	1.36238	0.11603	2	219.942 80	27.15720	23.09347	0.1647 977	0.066900109	0.0228 167	0.001538	4.3180146	6.6823
1390.02 03	144.44 055	88.626 94	1.38263	0.11602	2	218.997 17	28.10283	24.03910	0.1771 809	0.074580514	0.0255 052	0.0019184	4.8307855	7.19632
1390.00 723	144.95 457	88.239 36	1.39939	0.11603	2	218.039 46	29.06054	24.99681	0.1897 223	0.082637586	0.0283 415	0.0023642	5.3726546	7.71034
1389.99 304	145.46 86	87.854 87	1.41346	0.11603	2	217.089 38	30.01062	25.94688	0.2021 637	0.090898118	0.0312 668	0.0028717	5.9324651	8.22437
1390.00 097	145.98 262	87.467 95	1.42187	0.11603	2	216.133 30	30.96670	26.90296	0.2146 838	0.09947155	0.0343 217	0.0034531	6.518106	8.73839
1390.00 371	146.49 664	87.083 2	1.42883	0.11603	2	215.182 59	31.91741	27.85368	0.2271 336	0.108248568	0.0374 693	0.0041066	7.1226078	9.25241
1390.00 03	147.01 067	86.702 98	1.43186	0.11603	2	214.243 06	32.85694	28.79320	0.2394 369	0.117161945	0.0406 87	0.0048316	7.7417111	9.76644
1390.00 006	147.52 469	86.318 14	1.4313	0.11603	2	213.292 12	33.80788	29.74414	0.2518 896	0.126419898	0.0440 521	0.0056508	8.3903965	10.2804 6
1389.99 808	148.03 871	85.943 87	1.42996	0.11603	2	212.365 15	34.73485	30.67111	0.2640 285	0.135667625	0.0474 373	0.0065374	9.0442073	10.7944 8
1390.00 136	148.55 274	85.570 31	1.42687	0.11603	2	211.444 24	35.65576	31.59203	0.2760 881	0.14506797	0.0509 032	0.0075096	9.7148949	11.3085 1
1390.00 749	149.06 676	85.199 82	1.42273	0.11603	2	210.528 76	36.57124	32.50751	0.2880 765	0.154618611	0.0544 506	0.0085717	10.4027	11.8225 3
1389.99 571	149.58 078	84.835 31	1.41759	0.11603	2	209.628 05	37.47195	33.40822	0.2998 714	0.164211134	0.0580 406	0.0097151	11.100127	12.3365 5
1390.00 047	150.09 481	84.473 06	1.41155	0.11603	2	208.732 93	38.36707	34.30334	0.3115 932	0.173932979	0.0617 071	0.0109534	11.813832	12.8505 8
1390.00 328	150.60 883	84.114 4	1.40373	0.11603	2	207.846 68	39.25332	35.18959	0.3231 988	0.183740379	0.0654 352	0.0122849	12.540965	13.3646
1389.99 839	151.12 285	83.761 06	1.39479	0.11603	2	206.973 58	40.12642	36.06269	0.3346 323	0.193576091	0.0692 041	0.0137048	13.277544	13.8786 2
1389.99 796	151.63 688	83.414 92	1.38523	0.11603	2	206.118 27	40.98173	36.91800	0.3458 327	0.203375752	0.0729 898	0.0152048	14.018882	14.3926 5
1390.00 211	152.15 09	83.070 8	1.37663	0.11603	2	205.267 95	41.83205	37.76832	0.3569 679	0.213276836	0.0768 464	0.0168085	14.775604	14.9066 7
1389.99 862	152.66 492	82.735 75	1.36704	0.11603	2	204.440 04	42.65996	38.59623	0.3678 095	0.223066531	0.0806 915	0.0184826	15.531584	15.4206 9

1389.99 125	153.17 895	82.403 81	1.35582	0.11603	2	203.619 81	43.48019	39.41645	0.3785 505	0.232908711	0.0845 899	0.0202558	16.299565	15.9347 2
1390.01 132	153.69 297	82.078	1.34677	0.11603	2	202.814 74	44.28526	40.22153	0.3890 931	0.242705913	0.0885 038	0.0221123	17.072113	16.4487 4
1390.01 319	154.20 699	81.760 32	1.33831	0.11603	2	202.029 75	45.07025	41.00652	0.3993 727	0.252387344	0.0924 047	0.0240379	17.84361	16.9627 6
1390.00 65	154.72 102	81.449 16	1.32884	0.11603	2	201.260 87	45.83913	41.77539	0.4094 413	0.261991662	0.0963 08	0.0260392	18.617062	17.4767 9
1389.98 815	155.23 504	81.143 79	1.32042	0.11603	2	200.506 31	46.59369	42.52996	0.4193 225	0.271532807	0.1002 193	0.0281185	19.39358	17.9908 1
1390.00 033	155.74 906	80.843 16	1.3096	0.11603	2	199.763 45	47.33655	43.27282	0.4290 504	0.28103633	0.1041 493	0.0302818	20.175285	18.5048 3
1390.00 127	156.26 309	80.554 71	1.30354	0.11603	2	199.050 69	48.04931	43.98558	0.4383 841	0.290256694	0.1079 954	0.0324699	20.941731	19.0188 6
1390.00 115	156.77 711	80.265 5	1.29742	0.11603	2	198.336 05	48.76395	44.70022	0.4477 425	0.299600428	0.1119 271	0.0347786	21.726673	19.5328 8
1389.99 024	157.29 113	79.984	1.28856	0.11603	2	197.640 46	49.45954	45.39580	0.4568 513	0.308789351	0.1158 279	0.0371404	22.50687	20.0469
1390.00 009	157.80 516	79.711 36	1.28204	0.11603	2	196.966 77	50.13323	46.06950	0.4656 735	0.317776837	0.1196 768	0.0395395	23.278057	20.5609 3
1390.00 366	158.31 918	79.445 75	1.27642	0.11603	2	196.310 45	50.78955	46.72582	0.4742 681	0.32661485	0.1234 948	0.041986	24.044388	21.0749 5
1389.99 951	158.83 32	79.183 79	1.26985	0.11603	2	195.663 15	51.43685	47.37312	0.4827 447	0.335410212	0.1273 276	0.0445084	24.815032	21.5889 7
1389.99 08	159.34 723	78.925 72	1.26339	0.11603	2	195.025 45	52.07455	48.01081	0.4910 954	0.344150813	0.1311 703	0.0471032	25.588962	22.103
1390.00 011	159.86 125	78.676 64	1.25682	0.11603	2	194.409 98	52.69002	48.62629	0.4991 552	0.352657716	0.1349 431	0.0497144	26.350103	22.6170 2
1390.00 481	160.37 527	78.432 75	1.25232	0.11603	2	193.807 33	53.29267	49.22894	0.5070 47	0.361054187	0.1386 995	0.0523762	27.109169	23.1310 4
1390.00 324	160.88 93	78.193 77	1.24681	0.11603	2	193.216 81	53.88319	49.81946	0.5147 8	0.369345256	0.1424 412	0.0550884	27.866476	23.6450 7
1390.00 205	161.40 332	77.958 99	1.24322	0.11603	2	192.636 66	54.46334	50.39960	0.5223 771	0.377551486	0.1461 771	0.0578563	28.623798	24.1590 9
1390.00 139	161.91 734	77.728 7	1.23902	0.11603	2	192.067 62	55.03238	50.96865	0.5298 289	0.385658965	0.1499 003	0.0606738	29.37975	24.6731 1
1389.99 687	162.43 137	77.502 85	1.23599	0.11603	2	191.509 54	55.59046	51.52673	0.5371 37	0.393665706	0.1536 096	0.0635386	30.134023	25.1871 4
1389.99 975	162.94 539	77.286 03	1.23329	0.11603	2	190.973 78	56.12622	52.06249	0.5441 529	0.401403745	0.1572 256	0.0663865	30.870421	25.7011 6
1389.99 129	163.45 941	77.069 3	1.22831	0.11603	2	190.438 24	56.66176	52.59803	0.5511 659	0.409188587	0.1608 95	0.0693314	31.618804	26.2151 8
1390.01 196	163.97 344	76.855 14	1.22529	0.11603	2	189.909 05	57.19095	53.12722	0.5580 957	0.416929924	0.1645 761	0.0723407	32.370654	26.7292 1
1389.99 647	164.48 746	76.646 86	1.22427	0.11603	2	189.394 39	57.70561	53.64188	0.5648 353	0.42450496	0.1682 097	0.0753647	33.113892	27.2432 3
1390.00 079	165.00 148	76.442 29	1.22177	0.11603	2	188.888 90	58.21110	54.14737	0.5714 548	0.431989192	0.1718 312	0.0784309	33.8557	27.7572 5
1389.99 708	165.51 551	76.244 26	1.21999	0.11603	2	188.399 57	58.70043	54.63670	0.5778 628	0.439275571	0.1753 877	0.0814924	34.58519	28.2712 8
1389.98 988	166.02 953	76.046 18	1.21803	0.11603	2	187.910 11	59.18989	55.12616	0.5842 723	0.446604316	0.1789 96	0.0846488	35.326331	28.7853
1389.99 657	166.54 355	75.851 14	1.21537	0.11603	2	187.428 17	59.67183	55.60810	0.5905 834	0.453859973	0.1825 999	0.0878514	36.067556	29.2993 2
1389.99 709	167.05 758	75.659 18	1.21376	0.11603	2	186.953 83	60.14617	56.08243	0.5967 949	0.461039008	0.1861 973	0.0910976	36.80843	29.8133 5

