

OPTIMISATION OF COMPOSITIONS AND HEAT TREATMENTS OF Pt-BASED SUPERALLOYS

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Nickel-based superalloys are constrained by the melting point of Ni for increased higher temperature uses, and Pt is a candidate for replacement¹. Several experimental Pt-based alloys have been studied at Mintek. The best properties were exhibited by the Pt-Al-Cr and Pt-Al-Ru alloys which had $\sim\text{Pt}_3\text{Al}$ precipitates in a (Pt) matrix. However, the precipitate volume fraction was not as high as in the Ni-based superalloys. Ternary alloys were combined, and the $\text{Pt}_{84}\text{Al}_{11}\text{Ru}_2\text{Cr}_3$ alloy is the optimum composition so far², but the volume fraction still needs improvement. Thus, this work is an investigation to increase the $\sim\text{Pt}_3\text{Al}$ volume fraction in Pt-Al-Ru-Cr alloys, by varying compositions and heat treatments.

Six alloys of different compositions were selected using the optimum composition as the basis. The nominal compositions of these alloys are given in Table 1. Alloys were prepared by arc-melting pure (at least 99.9%) elements together. The samples were then sectioned, and one half was heat treated in air at 1500°C for 18 hours and quenched in water, followed by homogenization heat treatment at 1100°C for 120 hours and air cooling. Metallographic preparation was undertaken, finishing with an oxide polishing (OP-S) technique. Microstructural analyses were carried out in an HR FEI Nova NanoSEM in the BSE mode, also using EDX. XRD was done for confirmation of the (Pt) and $\sim\text{Pt}_3\text{Al}$ phases.

Typical examples of the microstructures in both the as-cast and heat treated conditions are shown in Figs. 1 and 2 for $\text{Pt}_{85}\text{Al}_7\text{Ru}_3\text{Cr}_5$. The as-cast alloy (Fig. 1) had (Pt) dendrites with fine $\sim\text{Pt}_3\text{Al}$ precipitates, surrounded by a mixture of (Pt) + $\sim\text{Pt}_3\text{Al}$. The mixture was deduced to arise from the eutectoid reaction, since (Pt) was crystallographically aligned. The heat treated sample had $\sim\text{Pt}_3\text{Al}$ precipitates in a (Pt) matrix. In all samples, the precipitates were spherical rather than cuboid. The average precipitate size was below 1 μm . The $\sim\text{Pt}_3\text{Al}$ volume fraction was observed to increase with increasing Pt:Al ratios. By visual examination, $\text{Pt}_{85}\text{Al}_7\text{Ru}_3\text{Cr}_5$ had a high volume fraction of the $\sim\text{Pt}_3\text{Al}$ precipitates, although confirmatory measurements by image analysis still needs to be done.

EDX phase analyses were also carried out on all samples. Table 2 shows the EDX analyses of $\text{Pt}_{85}\text{Al}_7\text{Ru}_3\text{Cr}_5$. The partitioning behaviour of elements in the phases in both conditions of the sample was similar. X-ray diffraction confirmed the presence of (Pt) and $\sim\text{Pt}_3\text{Al}$.

DST, NRF, the Mellon Foundation, Mintek and the PDI are thanked for support.

References:

1. Wolff, I.M. & Hill, P.J. (2000) Platinum Metals Rev., **44**, 158.
2. Cornish, L.A. *et al.* (2007) J. South Afr. Inst. Min. & Met., **107**, 697.

Table 1. Nominal alloy compositions (at.%).

Alloy no.	Pt	Al	Ru	Cr
1	78	15.5	2	4.5
2	80	14	3	3
3	81.5	11.5	2.5	4.5
4	82	12	2	4
5	84	11	2	3
6	85	7	3	5

Table 2. EDX phase analysis compositions (at.%).

	As-cast		Heat treated	
	(Pt)	(Pt) + $\sim\text{Pt}_3\text{Al}$	(Pt)	$\sim\text{Pt}_3\text{Al}$
Pt	90.4±0.5	84.3±0.2	89.1±0.4	83.4±0.2
Al	2.9±0.3	13.7±0.1	5.3±0.4	14.1±0.2
Cr	4.9±0.2	1.4±0.3	4.1±0.1	1.8±0.1
Ru	1.8±0.4	0.6±0.2	1.5±0.1	0.7±0.2

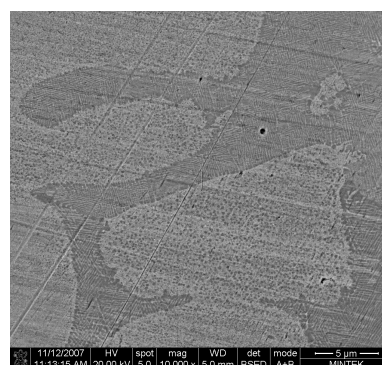


Figure 1. BSE image of as-cast $\text{Pt}_{85}\text{Al}_7\text{Ru}_3\text{Cr}_5$: (Pt) dendrites (light) with eutectic (Pt) + $\sim\text{Pt}_3\text{Al}$ (dark).

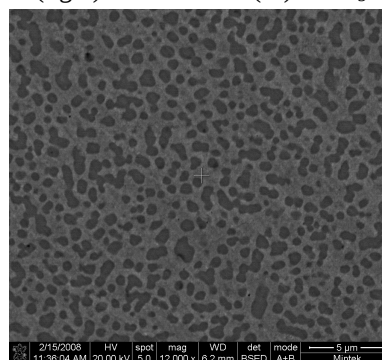


Figure 2. BSE image of heat treated $\text{Pt}_{85}\text{Al}_7\text{Ru}_3\text{Cr}_5$: $\sim\text{Pt}_3\text{Al}$ precipitates (dark) in a (Pt) matrix (light).

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