

THE IMPLEMENTATION OF THE DISCRETE
FOURIER TRANSFORM BY TABLE LOOK UP
TECHNIQUE

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A Dissertation Submitted to the Faculty of Engineering,
University of the Witwatersrand, Johannesburg, for the
Degree of Master of Science in Engineering

Johannesburg 1976

I declare that this dissertation is my own work and has not
previously been submitted for any degree at any University.

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ABSTRACT

The Development of a Discrete Fourier Transform Algorithm using the Table Look Up Method

The development of a system to compute the Discrete Fourier Transform (DFT) of a time sampled, wide dynamic range noiselike signal is reported in this dissertation. The mathematical basis of the algorithm is covered and an algorithm is then developed and programmed on a Nova 1200 minicomputer. The results are then compared with those of a Fast Fourier Transform Algorithm. (FFT)

Fourier analysis of continuous and sampled time signals is discussed and it is shown that the Fourier Series Coefficients of a sampled time sequence are related by a constant to the Discrete Fourier Transform of that time sequence. The Fourier Series Coefficients are considered to be a special case of the bivariate time average which is solved using a computational algorithm based on statistical averaging methods and a table look up method. The signal component of the bivariate average is sampled with a logarithmic analog to digital converter (LADC) thus allowing a wide dynamic range signal to be represented by a short word length. The problem of generating the sinusoidal component is overcome by spacing the abscissas in the statistical average numerical integration formula sinusoidally and generating linear in time addresses which correspond to the arguments of a sinusoidal wave.

The Fourier Series Coefficient algorithm is extended to compute Discrete Fourier Transforms and the linear address (argument)

generator is modified to generate addresses that correspond to all the frequencies extracted by the DFT. This algorithm is termed the Discrete Fourier Transform using the Table Look Up method (DFTTLU).

The basic features of this technique are summarized. The LADC output word and the generated address form an address pair which specifies a constant, in a stored table of constants, which is added to an accumulator. The accumulator is initially set to zero, and after the number of samples in a signal burst have been processed, will contain a number proportional to the harmonic, the frequency of which has been set by the generated addresses (arguments). The remaining harmonics are processed by setting the frequency of the generated addresses accordingly. The basic calculation step of this technique requires no multiplication. The algorithm is programmed in Assembler Code and is run on a minicomputer system that has a LADC peripheral.

An indication of the accuracy of the DFTTLU is obtained by comparing its results with those of an FFT algorithm of known accuracy analysing the same signal. The FFT is also programmed on the minicomputer and a 12 bit analog to digital converter peripheral (synchronised with the LADC) samples and encodes the signal. The differences between the results are less than 2% of the maximum harmonic amplitude for the worst case.

Although the aim of the work is the development of a real time Fourier Transform system that analyses noise-like signals, the system developed is slow because of the inherent complexity of the

Assembler Code needed to generate the addresses. It is envisaged that a hardware based system would simplify and overcome this problem.

ACKNOWLEDGEMENTS

This work has been supported by bursaries from the Council for Scientific and Industrial Research and the University of the Witwatersrand.

The author wishes to thank Professor Hanrahan who initiated and supervised the project and who offered many suggestions.

Thanks are also due to Mr Rex van Olst for the use of the Nova Fast Fourier Transform Calculation, Mr Alistair Walker for the use of the double word square root routine and Mrs Towsey who typed the manuscript.

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1 FOURIER ANALYSIS OF SIGNALS USING A DIGITAL SIGNAL PROCESSING SYSTEM

1.1 Introduction

In recent years digital instrumentation, with its inherent reliability, accuracy and ease of reading has rivalled, and in many cases surpassed analog instrumentation in most fields of electrical measurements. A glance at most electronic instrument makers' catalogues will show that digital voltmeters and frequency counters are common 'off the shelf' items while digital signal processing modulus such as those performing the Fast Fourier Transform (FFT), designed for use as 'stand alone' apparatus, or add on peripherals for a mini-computer (microprocessor), are entering the market in increasing numbers. The improvements in digital electronics technology and the resulting decrease in costs have given rise to digital systems designed to compute more complex electrical measurements such as time averages, correlation coefficients and Fourier Transforms of signals.

Simplicity and accuracy are two important aspects in the design of a digital signal measurement system. Most systems consist of;

1. An analog to digital converter (ADC) which samples the amplitude of an analog signal with respect to time and represents this amplitude with a digital code word.
2. A digital processor which calculates the required measurement (eg time average) of the analog signal. The digital

processor can be a special purpose digital instrument or a computer programmed to perform the required measurement.

3. The output display displays the result of the measurement in a digital (eg LED or NIXIE display) or graphic (eg CRO or plotter display) form.

The accuracy of most existing digital signal processing systems relies in most cases, not on theoretical considerations, but on processing a large number of time samples to reduce sampling errors, and on finely quantised amplitude levels in the ADC to reduce amplitude quantisation errors. The resulting digital instrument is usually more accurate than its analog counterpart and less complex than an analog instrument of comparable accuracy. The major sources of error in most digital signal processing systems can be broadly classified as;

1. Time sampling errors
2. Amplitude quantising errors.
3. Rounding or truncating errors in the numerical

algorithm used to calculate the measurement.

These errors are discussed in chapter 4 and chapter 2 of references 5 and 14 respectively.

Hanrahan (ref. 6) reviews some of the literature on these errors and presents a study of the underlying theory of time averages of amplitude quantised time sampled data. The particular approach used in this work leads to the development of a simple algorithm, based on a table look up (TLU) method and on statistical

averages, to calculate time averages of signals. The basic features of the TLU method are as follows:

Samples of the signal being processed are quantised fairly coarsely. The quantiser output word is used as an address to specify a constant, in a table of constants, which is added to an accumulator. The accumulator, initially set to zero, contains a number proportional to the required average after a large number of samples have been processed. This technique can compute multivariate as well as single variate time averages. A simplified block diagram of a system to calculate a single variate average is given in Fig 1.1.

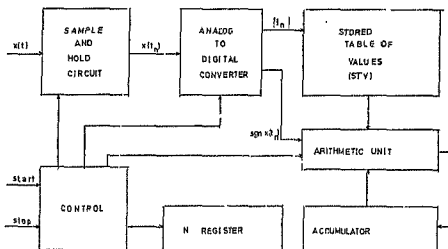


Fig.1.1 Single Variate Time Average System

This approach in implementing a digital processor has the following advantages:

1) A simple ADC is used. The ADC has fewer amplitude levels when compared with most commercially produced ADC¹¹ and less bits are needed to code an amplitude level.

2) The basic calculation step does not need a multiplication operation.

These factors allow a relatively simple digital signal processing system to be developed to compute time averages such as:

1. Mean value
2. Mean square value
3. Correlation Coefficients
4. Autocorrelation Coefficients
5. Fourier Coefficients.

The table look up method is not exact because of the quantisation of the signals in both time and amplitude. The accuracy obtainable ranges from errors of a few per cent with relatively coarse amplitude quantisation (ie approximately 8 levels and 500 - 1 000 samples) to 0.1% error with 16 - 64 amplitude levels and up to 4 000 samples.

The TLU method does not restrict the ADC characteristic and consequently the ADC characteristic can be chosen to suit the properties of the signal being processed. Signals that have a wide dynamic range and a Gaussian or similar amplitude distribution (ie noise like signals) are of particular interest in the fields

of acoustic and vibration analysis. These signals can be quantised logarithmically, so providing high resolution at low signal amplitudes and coarse resolution at high signal amplitudes. Hanrahan¹⁰ describes a system that has a 19 level, 3dB spacing logarithmic analog to digital converter (LADC) to compute the mean and mean square values of noise signals to an accuracy of the order of 0,5dB. A logical extension of the work, suggested by Professor Hanrahan as the subject of this dissertation, is Fourier Analysis of logarithmically quantised noiselike signals, the aim of the work being the development of a real time on line digital Fourier Analyser that exploits the advantages of the LADC and the TLU method. This system could be used in acoustic signal analysis, low frequency vibration analysis or any application that requires the Fourier Transform of noiselike, wide dynamic range signals.

1.2 Review of the Literature

The literature pertinent to the TLU method, analog to digital converters and Fourier Analysis systems is reviewed in this section. An existing TLU system that calculates Fourier Coefficients is described and the LADC is discussed. A brief description of the state of the art in Fourier Analysis systems is given.

1.2.1 The Table Look Up Method and the Logarithmic Analog to Digital Converter

Hanrahan⁶ describes a TLU system that calculates the Fourier Coefficients of deterministic signals which are quantised

into eight positive and eight negative linearly spaced levels in this particular case. The typical error is given as a percentage of the maximum value fundamental which is defined to be 1. The errors are of the same order or better than those of a conventional heterodyne wave analyser (viz. 3 per cent full scale error and 6 per cent spurious response). A more complex system based⁷ on the same principle reduces the errors to one per cent error and one per cent spurious response.

The concept of quantising wide dynamic range noise-like signals using a logarithmic analog to digital converter (LADC) is discussed in reference 8 and a TLU system incorporating an LADC to calculate mean and mean square values is described. The error analysis shows the errors to be of the order of 0.1 dB provided that a noise-like signal is processed. The error rises to approximately 2dB when a deterministic signal is processed. Applications of this system are discussed in reference 9. The design considerations of a LADC computer peripheral and the computer programme needed to compute mean and mean square values of a noise-like signal is covered in reference 10. The LADC developed has 19 positive and 19 negative levels spaced 3dB apart.

1.2.2 The State of the Art in Fourier Analysis Systems

Fourier analysis systems can be divided into two types, analog and digital systems. The systems described here are just a few of the many systems available.

1.2.2.1 Analog Systems

The heterodyne wave analyser was used by Bell Telephone Laboratories² in the late forties as the basis of the 'Sona Graph' spectrum analyser. This electro-mechanical instrument, which is used to analyse speech signals, produces a frequency spectrogram of about 2,5 seconds of speech signals in about three minutes. The dynamic range of the spectrogram is about 12dB.

Today, the best description of the state of the art is found in electronic equipment catalogues.^{3,12} For example, the specifications of the HP 3580A Spectrum Analyser are summarized below.¹²

Frequency Range:	5Hz to 50kHz
Dynamic Range	80dB
Maximum Error	1dB
Sweeptime	0,1 sec. to 2 000 sec.
Minimum Bandwidth	1Hz

A bandpass filter (1Hz minimum bandwidth) is placed between the required lower and upper frequency limits and the filter output is displayed on a CRT.

Another analog system is the Bruel and Kjaer³ Type 3347 Real Time one third Octave Analyser. This system consists of 30 one third octave filters with centre frequencies from 25Hz to 20kHz. The filter outputs are scanned every 20ms and the results are displayed on a CRT in the form of a bar graph - the horizontal axis is the

frequency axis. The dynamic range of the instrument is 64dB and the CRT displays a range of 50dB with a resolution of 0,2dB.

Generally the analog Fourier analysis instruments are complicated and require a calibration or setting up procedure before they can be used.

1.2.2.2 Digital Systems

Digital systems that perform Fourier Analysis can be divided into two types.

1. Systems that use linear filter theory or recursive techniques.¹¹
2. Systems that use the Cooley Tukey Fast Fourier Transform (FFT).⁵

The FFT algorithm is used in virtually all digital systems. Most minicomputers with 4K of memory core and the ability to control an ADC peripheral can be programmed to analyse electrical signals using the FFT algorithm.

An example of a big commercially produced system that uses the FFT is the HP5451 series.¹² This consists of a minicomputer, keyboard, a dual 10 bit analog to digital converter, a display control unit and a CRT, and a software package to control the system. A Fourier Transform of 1024 time samples is produced in about 100ms. and has a dynamic range of 80dB and a frequency range of 0 - 100kHz.

At the other end of the scale there are the 'FFT modules', an example of which is the Plessey SPM-02. This is designed for

use as a 'stand alone' or add on FFT processor with a minicomputer or microprocessor. The module can process 1 024 complex points in 250ms with a frequency range of 0 - 50 kHz.

All the above examples must not be construed as a complete description as the state of the art, but they do give an indication of the different methods used in Fourier analysis.

1.3 The Present Work

The present work is concerned with the development of a digital system that exploits the advantages of the TLU method and the LADC to perform real time on line Fourier Transforms of noise signals that have a wide dynamic range. The system is implemented as a software programme that is run on a Nova 1200 minicomputer in conjunction with the 19 level, 3dB spacing logarithmic analog to digital converter.¹⁰ The speed and accuracy of the system are investigated by varying certain parameters and comparing the results with those given by an algorithm of known accuracy (eg Cooley Tukey Fast Fourier Transform, FFT). The ultimate aim of this work is the development of a Fourier Analysis Instrument that can rival and, in some cases, replace existing digital (and analog) Fourier Analysis systems that process noiselike signals.

The flexibility of the computer facilitates changes to the algorithms in the light of results obtained in analysing signals. The programme steps needed to implement the algorithm are analogous to the steps required if the algorithm is implemented in a special purpose hardware digital instrument.

1.4 Scope and Format of the Dissertation

This dissertation first covers the mathematical basis of the DFT TLU and then discusses the development of a computational algorithm. The algorithm is programmed on a Nova 1200 minicomputer and the results are compared with the results of an FFT algorithm.

Fourier analysis of continuous and time sampled signals is covered in Chapter 2 and it is shown that the Fourier Coefficients of a time sampled, periodic signal are related to the Discrete Fourier Transform of that time sampled signal. The Fourier Coefficients are also shown to be a special case of the bivariate time average which is solved using a computational algorithm based on statistical averaging methods and a table look up method. The problem of generating the sinusoidal component of the bivariate average is discussed and a simple linear in time sinusoidal channel address generation is developed.

In Chapter 3 the linear in time address generator is modified so that the Fourier Coefficient system can be extended to compute the Discrete Fourier Transform.

The algorithm that is programmed to solve the DFT TLU is discussed in detail in Chapter 4 and numerical values of harmonics and the machine code scale factors are derived and tabulated.

The DFTTLU is compared with the FFT in Chapter 5 in order

to obtain an error characteristic. The results of the FFT are regarded as the 'true' value and the differences between the FFT and the DFT TLU are termed the 'errors'.

The conclusions and recommendations for further work are covered in Chapter 6.

Derivations or discussions that break the continuity of this dissertation are covered by the appendices at the end of this report. The generation of the linear in time addresses which replace sine or cosine waves needed for Fourier Transform Analysis is discussed in Appendices A3 and A4 and the derivation of the stored table of values (STV) is discussed in A1 and A2. A system that compares the results of the DFT TLU and an FFT algorithm is given in A6.

2. THEORY UNDERLYING THE APPLICATION OF THE TABLE LOOK UP METHOD TO THE DISCRETE FOURIER TRANSFORM

2.1 Introduction

This chapter reviews the definitions of the Fourier Series Coefficients and the Fourier Transform for continuous and sampled input data. In a sampled data system, where the signal is periodic, band limited and sampled at its Nyquist Rate, the complex Fourier Coefficients are shown to be samples of the continuous Fourier Transform taken at integral multiples of a frequency proportional to the sampling rate. It is then shown that the complex Fourier Coefficients are proportional to the Discrete Fourier Transform (DFT) points of the sampled signal. The complex Fourier Coefficients are a special case of the bivariate time average⁵ and are solved with statistical averages and the table look up technique. In this dissertation the theory that shows how the table look up method can be used to solve a bivariate statistical time average is not given as this is covered in appendices 3 and 7 of reference 6.

2.2 The Fourier Series Coefficients and the Fourier Transform

For a continuous, periodic, real time function $x(t)$ of period T_1 , the general equation of the Fourier Series can be written as follows:

$$x(t) = \frac{a_0}{2} + \sum_{r=1}^{\infty} a_r \cos(2\pi r f_1 t) + b_r \sin(2\pi r f_1 t) \quad 2.1$$

r is the order of the Fourier Series Coefficients and $f_1 = 1/T_1$.

The Fourier Series Coefficients are written as follows:

$$a_r = \frac{2}{T_1} \int_{-T_1/2}^{T_1/2} x(t) \cos(2\pi r f_1 t) dt. \quad 2.2$$

$$b_r = \frac{2}{T_1} \int_{-T_1/2}^{T_1/2} x(t) \sin(2\pi r f_1 t) dt \quad 2.3$$

Equations 2.2 and 2.3 can be written in the exponential form

$$c_r = \frac{1}{T_1} \int_{-T_1/2}^{T_1/2} x(t) e^{-j2\pi r f_1 t} dt \quad 2.4$$

$$\text{ie } c_r = \frac{a_r - jb_r}{2} \quad 2.5$$

The Fourier Transform can be written as

$$X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt \quad 2.6$$

Consider a burst waveform $x(t)$ of duration NT . By definition as $x(t)$ is time limited, its Fourier Transform cannot be band limited. Hence it cannot be sampled fast enough to completely prevent aliasing. However, if the sampling interval T is small enough, aliasing can be reduced to negligible extent. Under these circumstances the interpolation^s (sampling) theorem may be applied, and it would be possible to reconstitute $x(t)$ almost exactly from its samples $x_s(nT)$, i.e.

$$x(t) = \sum_{n=0}^{N-1} \frac{\sin \pi \left(\frac{t-nT}{NT} \right)}{\pi \left(\frac{t-nT}{NT} \right)} x_s(nT) \quad 2.7$$

where N is a finite number. If the signal burst is repeated to give $x_p(t)$, the Fourier series coefficients of $x_p(t)$ can be computed. The periodic repetition of the sampled burst can be written as

$$x_p(t) = \sum_{l=-\infty}^{\infty} \sum_{n=0}^{N-1} \frac{\sin \frac{\Omega}{2}(t - nT - lNT)}{\frac{\Omega}{2}(t - nT - lNT)} x_s(nT) \quad 2.8$$

$$\Omega = 2\pi/N T \quad 2.9$$

In this case the complex Fourier

Series Coefficients are denoted D_k .

$$D_k = \frac{1}{NT} \int_0^{NT} x_p(t) e^{-jk\Omega t} dt \quad 2.10$$

$$D_k = \frac{1}{NT} \int_0^{NT} \sum_{l=-\infty}^{\infty} \sum_{n=0}^{N-1} \frac{\sin \frac{\Omega}{2}(t - nT - lNT)}{\frac{\Omega}{2}(t - nT - lNT)} x_s(nT) e^{-jk\Omega t} dt \quad 2.11$$

$$D_k = \frac{1}{NT} \sum_{n=0}^{N-1} \int_0^{NT} x_s(nT) e^{-jk\Omega t} \sum_{l=-\infty}^{\infty} \frac{\sin \frac{\Omega}{2}(t - nT - lNT)}{\frac{\Omega}{2}(t - nT - lNT)} dt \quad 2.12$$

$$D_k = \frac{1}{NT} \sum_{n=0}^{N-1} x_s(nT) e^{-j\Omega Tnk} \quad 2.13$$

The DFT of $x_p(nT)$ exists and is

$$X(k\Omega) = \sum_{n=0}^{N-1} x_p(nT) e^{-j\Omega Tnk} \quad 2.14$$

$$= \sum_{n=0}^{N-1} x_s(nT) e^{-j\Omega Tnk} = X_k \quad 2.15$$

From equations 2.13 and 2.15

$$NTD_k = X_k \quad 2.16$$

The k th Fourier series coefficient D_k of a periodic or repeated burst waveform sampled sufficiently fast to reduce aliasing to a negligible level, multiplied by the waveform period or burst duration NT , is equal to the k th harmonic of the DFT, X_k , of that waveform.

It is meaningless to talk of the Fourier Transform of a sequence of samples⁵ but a sequence of discrete numbers $x_s(nT)$ with a time function

$$f(t) = \sum_{n=-\infty}^{\infty} x_s(nT) \delta(t - nT) \quad 2.17$$

has a Fourier Transform.

$$F(\omega) = \sum_{n=-\infty}^{\infty} x_s(nT) e^{-j\omega nT} \quad 2.18$$

The time function of equally spaced impulses $\delta(t - nT)$, has a transform that is periodic in frequency with period $\frac{2\pi}{T}$. In most cases the DFT of a sampled time function will only approximate the Fourier Transform of the time function (cf equations 2.14 and 2.18) but the properties of the DFT and the Fourier Transform correspond exactly. However there are only N distinct numbers in the DFT and only N different frequencies can be distinguished. These frequencies are denoted

$$\text{frequency} = k\Omega, \quad k = 0, 1, 2, \dots, N-1 \quad 2.19$$

$$\text{where } \Omega = \frac{2\pi}{NT} \text{ and } T = \text{sampling period}$$

The complex numbers NTD_k can be regarded as samples of the Fourier Transform taken at integral multiples of the frequency Ω and a 'continuous Fourier Transform Spectrum' could be approximated using the interpolation formula

$$X(f_1) = NT \sum_{q=-\infty}^{\infty} D(qf_1) \frac{\sin \pi(f - qf_1) NT}{\pi(f - qf_1) NT} \quad 2.20$$

$$\text{where } f_1 = \frac{\Omega}{2\pi}$$

Algorithms that compute Fourier Series Coefficients a_x, b_x, c_x are of great significance as they can be used to compute a frequency spectrum of a burst like phenomena.

2.3 Expressing the Fourier Series Coefficients as a Bivariate Time Average

Consider equation 2.15

$$X_k = \sum_{n=0}^{N-1} x_S(nT) e^{-j\Omega Tnk} \quad 2.15$$

$$\therefore \text{Re}(X_k) = \sum_{n=0}^{N-1} x_S(nT) \cos \Omega Tnk \quad 2.21$$

$$\text{now } X_k = NT D_k \quad 2.16$$

$$\text{Re}(D_k) = \frac{1}{NT} \sum_{n=0}^{N-1} x_S(nT) \cos \Omega Tnk \quad 2.22$$

$$= \overline{x_S(nT) \cos \Omega Tnk} \quad 2.23$$

$$\operatorname{Re}(D_k) = \overline{x_S(t_n) \cos k\Omega t_n} \quad 2.24$$

Similarly for $\operatorname{Im}(D_k)$

$$\operatorname{Im}(D_k) = \overline{x_S(t_n) \sin k\Omega t_n} \quad 2.25$$

2.4 The Evaluation of the Time Average as a Statistical Average

In reference 6 a versatile method of calculating time averages, using amplitude quantised time sampled data, and based on statistical averages and equivalent to the required bivariate time average, has been developed. This method is applied to the estimation of D_k . The general average, expressed as a statistical average¹³ is

$$\overline{xy} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} XY p_{xy}(X, Y) dXdY \quad 2.26$$

where $p(X, Y)$ is the joint probability density function of X and Y .

$$\overline{xy} = \int_{-X_L}^{X_L} \int_{-Y_L}^{Y_L} \operatorname{sgn}(X) \cdot \operatorname{sgn}(Y) p_{xy}(X, Y) dXdY \quad 2.27$$

The intermediate mathematical steps between equations 2.26 and 2.27 are detailed in Appendix 3 in reference 6.

$\pm X_L$ and $\pm Y_L$ are the amplitude limits which $x(t)$ and $y(t)$ are assumed not to exceed. The distribution function, $p_{xy}(X, Y)$ is defined as the joint probability that $x(t)$ is more remote from zero than X AND $y(t)$ is more remote from zero than Y .

$\text{sgn}(X)$ is interpreted as

$$\text{sgn}(X) = 1 \quad X \geq 0+$$

$$\text{sgn}(X) = -1 \quad X \leq 0-$$

Equation 2.27 is the basis for developing the table look up algorithm (TLU) to solve D_k . Numerical integration is performed with respect to one variable (say X) while the other (Y) is held constant at some value Y_r .

$$C(Y_r) = \int_{-X_L}^{X_L} \text{sgn}(X) P_{xy}(X, Y_r) dX \quad 2.28$$

This is estimated with a numerical integration formula

$$\int_{-X_L}^{X_L} f(X) dX \doteq \frac{h_x}{D_x} \sum_{i=0}^{M_x-1} w_i f(X_i) \quad 2.29$$

The only constraint on the quantising of the X channel signal is a one to one correspondence between the M_x quantiser thresholds, X_i , in the interval $0 \leq X \leq X_L$ and the abscissas in the numerical integration formula. h_x and D_x are integration constants and w_i are the integration weights of the formula. The thresholds on the negative axis are:

$$X_{-i} = -X_i; (w_{-i} = w_i) \quad i = 0, 1 \dots M_x - 1$$

The Y channel is similar and the integration weights are denoted u_j

Under these conditions, the integrand, $P_{xy}(X, Y)$, can be estimated as the ratio of the number of sample pairs, C_{ij} , which fell more remote from zero than X_i and Y_j respectively, to the total number of sample pairs, N

$$\text{i.e.} \quad P_{xy}(X, Y) \doteq \frac{C_{ij}}{N} \quad 2.30$$

Equation 2.27 can now be written

$$\overline{xy} \doteq \frac{h_x h_y}{D_x D_y N} \sum_{i=0}^{M_x-1} \sum_{j=0}^{M_y-1} \text{sgn}(X_i) \text{sgn}(Y_j) w_i u_j C_{ij} \quad 2.31$$

N samples of $x(t)$ and N samples of $y(t)$ are taken at sampling instants t_n , $n = 0, 1, 2 \dots N-1$, and the amplitude of the samples are quantised according to the above constraints. At the end of each sampling period C_{ij} is calculated and the summation in equation 2.31 is performed. The algorithm suggested by equation 2.31 is wasteful as $M_x M_y$ sample totals C_{ij} have to be stored and a summation must be performed N times. In appendix 7 of reference 6 equation 2.31 is further simplified and is written

$$\overline{xy} \doteq \frac{h_x h_y}{D_x D_y N} \sum_{n=0}^{N-1} \text{sgn}(x(t_n) \cdot y(t_n)) S(I_n K_n) \quad 2.32$$

$S(I_n K_n)$ is a two dimensional array and each element in the array is calculated according to:

$$S(s, r) = \sum_{i=0}^S \sum_{j=0}^r w_i \cdot u_j \quad \begin{aligned} s &= 0, 1 \dots M_x - 1 \\ r &= 0, 1 \dots M_y - 1 \end{aligned}$$

I_n and K_n are the digital outputs of the ADCs operation on $x(t_n)$ and $y(t_n)$ respectively. I_n is equal to the subscript of the largest X abscissa less than or equal to $x(t_n)$ and K_n is equal to the subscript of the largest Y abscissa less than or equal to $y(t_n)$. The algorithm embodied in equation 2.32 is one of addressing particular locations in a store (table) containing an array of constants $S(s, r)$. An accumulator is initially set to zero.

When the two samples are taken at time t_n I_n and K_n are obtained. These values, acting as addresses, specify that the constant $S(I_n K_n)$ held in address location $(I_n K_n)$ in the stored table of values, is to be added to the accumulator. Signed addition is necessary, the sign being obtained from $\text{sgn}(x(t_n)y(t_n))$. After N address pairs have been similarly processed the accumulator will contain the value

$$\overline{xy} = \frac{D.D.N}{h} \sum_{x,y} x y$$

A block diagram of a system to implement this algorithm is given in Fig.2.1.

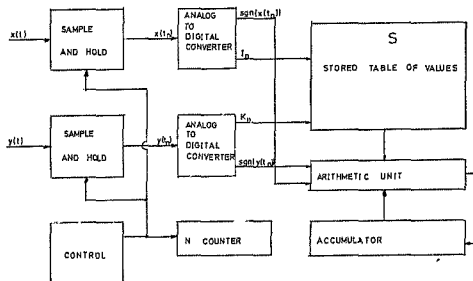


Fig.2.1 System to Estimate $\overline{xy}$

2.5 Applying the Statistical Average using the TLU method to the Discrete Fourier Transform

The Fourier Coefficients can be estimated with equation 2.32

$$\overline{xy} = \frac{h_x h_y}{D_x D_y N} \sum_{n=0}^{N-1} \text{sgn}(x_{S_n} \cdot y(t_n)) S(I_n K_n) \quad 2.32$$

$$R_e(D_k) = \frac{h_x h_y}{D_x D_y N} \sum_{n=0}^{N-1} \text{sgn}(x_{S_n} \cdot y(t_n)) S(I_n K_n) \quad 2.33$$

where $y(t_n) = \cos(\frac{2\pi nk}{N})$ $k = 0 \dots N-1$

$$Im(D_k) = \frac{h_x h_y}{D_x D_y N} \sum_{n=0}^{N-1} \text{sgn}(x_{S_n} \cdot y(t_n)) S(I_n K_n) \quad 2.34$$

where $y(t_n) = \sin(\frac{2\pi nk}{N})$ $k = 0 \dots N-1$

To simplify the equations, T, the sampling period is defined to be one unit of time and equation 2.3 becomes

$$\Omega = \frac{2\pi}{N} \quad 2.35$$

Equation 2.16 is now written as

$$ND_k = X(k\Omega) = F_k = X_k \quad 2.36$$

F_k is the Discrete Fourier Transform implemented with the table lookup method (DFTTLU).

Equations 2.33 and 2.34 are written

$$F_k = \frac{h_x h_y}{D_x D_y} \sum_{n=0}^{N-1} \text{sgn}(x_n \cdot y_n) S(I_n K_n) \quad 2.37$$

$$y_n = \cos(\frac{2\pi nk}{N}) \text{ for } Re(F_k) \quad 2.38$$

$$y_n = \sin(\frac{2\pi nk}{N}) \text{ for } Im(F_k) \quad 2.39$$

The N harmonics can be calculated by setting k to $0, 1 \dots N - 1$ and solving equations 2.37 and 2.38.

ie. If x_n is a band limited signal sampled at its Nyquist Rate, F_k , $k = 0, 1 \dots N - 1$ can be regarded as samples of the Fourier Transform taken at integral multiples of the frequency $\Omega = \frac{2\pi}{N}$.

The signal in the Y channel is deterministic and K_n follows a deterministic pattern. K_n could be generated with a digital sinusoidal address generator. The different frequencies of K_n are denoted K_{nk} . The subscripts nk correspond to the nk in $\sin(\frac{2\pi nk}{N})$.

If the Y channel abscissas (cf. eqn 2.39) follow a sinusoidal pattern, and the integration weights, u_j , and constants h_y and D_y are adjusted accordingly, K_{nk} becomes equivalent to the arguments of the sinusoidal function and has a LINEAR in time characteristic. Thus there is no need for any kind (analog or digital) sinusoidal generator. If the symmetrical properties of the sinusoid are exploited, K_{nk} need only have values that correspond to arguments between 0 and $\frac{\pi}{2}$ radians. The Y channel contribution to the signum function is the sign associated with the quadrant in which the argument falls. Consider the set of addresses (K_{nk} arguments) required by a sine wave. The output of K_{nk} address generator, in sign/magnitude form, must correspond to the cyclic state starting at B in Fig. 2.2

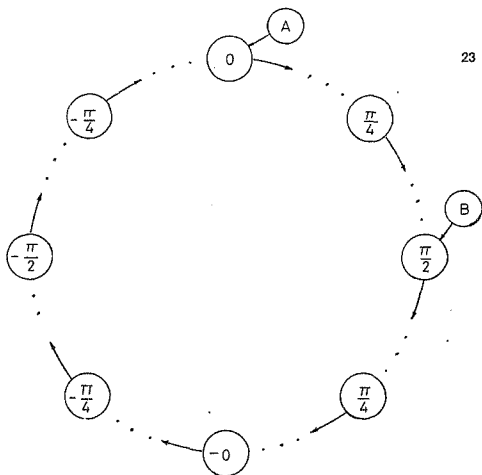


Fig. 2.2 Cyclic States of K_{nk}

The magnitude of the signed address generator (SAG) output forms the Y channel component of the address pair and the sign bit forms the Y channel component of the signum function. (This is similar to the logarithmic analog to digital converter output.) In this dissertation a negative signed address (argument) will never mean that an angular phasor has been displaced clockwise on a phasor diagram but that the sine or cosine of a negative argument has a negative magnitude. A cosine wave is regarded as a sine wave delayed by $\frac{\pi}{2}$ radians. This corresponds to starting the SAG at state A in Fig.2.2. The SAG can be considered a modified UP / DOWN counter which is simple to implement using TTL hardware.¹⁵ The system in Fig.2.1 is modified to incorporate the SAG and the system in Fig.2.3 results.

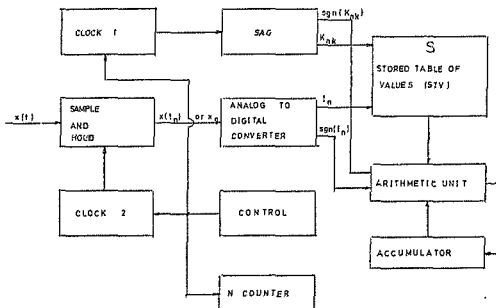


Fig.23 System to Estimate F_k

This system can only calculate one harmonic at a time.

Clock 1 sets the frequency (k) of the required harmonic and Clock 2 sets the sampling rate. The Accumulator is initially set to zero. At each sampling instant, t_n , the output of the quantiser, I_n and the output of the SAG, K_{nk} , form the address pair, $(I_n K_{nk})$ which extracts the constant, $S(I_n K_{nk})$ from location $(I_n K_{nk})$. This constant is either added or subtracted to or from the Accumulator, depending on the signum function. After N samples, the Accumulator contains a value proportional to the DFT frequency set by Clock 1.

In A7 a simple 8 point DFTTLU example shows the linear in time K_{nk} address generator. The signal is linearly quantised and a sine wave is analysed. The results are not exact because of the simplicity of the 'system'.

This chapter has set out the relationship between the Fourier Series Coefficients and the Fourier Transform and has shown that the Fourier Series Coefficients of a sampled, periodic or repeated burst waveform can be regarded as samples of the Fourier Transform of the continuous signal provided that the sampling rate is high enough to prevent aliasing. The properties of the Fourier Transform are valid for the DFT if the signal is band limited and sampled at or above its Nyquist rate. The Fourier Series coefficients are a special case of the bivariate time average which, in turn, is solved with statistical average methods and the table look up method. The TLU method, which requires no multiplication in its basic calculation step can be used to compute the DFT which normally needs complex multiplication and addition.

Finally the flexibility of the TLU techniques is demonstrated by the modification of the X and Y channel abscissas to suit the 'signal' being processed. In the X channel, the abscissas are spaced logarithmically to process noiselike signals with a wide dynamic range. In the Y channel, the abscissas are spaced sinusoidally and there is no need for a sine wave generator.

3 COMPUTING THE DISCRETE FOURIER TRANSFORM FROM THE FOURIER SERIES COEFFICIENTS

3.1 Introduction

If a real band limited signal is sampled at its Nyquist Rate and N of the samples are processed, the DFT allows N distinct frequencies to be extracted.⁵ These frequencies are denoted $k\Omega$ where

$$\Omega = \frac{2\pi}{NT}$$

T = sampling period

The frequencies $\frac{N}{2}$ $(N-1)$ are mirror images
of frequencies 0 $(\frac{N}{2}-1)$

The system in 2.5 can extract N distinct frequencies (one at a time) by setting Clock 1 to generate addresses that are equivalent to the sinusoidal waves of frequencies $k\Omega$, $k = 0, 1, \dots, (N-1)$. The output of the signed address generator (SAG) is denoted by Knk , where K is the signed address generated at time n to extract the k th harmonic. The subscript, nk , is analogous to the nk in the angular argument used in the normal DFT notation.

$$\text{eg. } \sin\left(\frac{2\pi nk}{N}\right) \text{ or } \cos\left(\frac{2\pi nk}{N}\right)$$

N^2 address pairs must be generated to extract N real harmonics and N^2 address pairs must be generated to extract N imaginary harmonics, in order to compute the DFTTLU. The term 'harmonics' is used loosely in this dissertation and will refer to the frequency domain results of the DFTTLU (i.e. the N output points of the DFTTLU). Thus the major problem in implementing the DFTTLU is the simple and efficient operation of the $2N^2$ signed addresses in the Y (sinusoidal) channel.

To clarify the discussion in this chapter, the calculation steps needed to implement an 8 point DFTTLU are presented and methods of generating the signed addresses are discussed with the aid of a DFTTLU system block diagram.

3.2 A System to Implement the Discrete Fourier Transform using the Table Look Up Method

A simple DFTTLU system is discussed to facilitate the explanation of the signed address generator (SAG). I_n is the digital encoded value of the sampled signal amplitude at time $n(n = 0 \dots N - 1)$. K_{nk} is the output of the SAG. The system only extracts imaginary harmonic components (ie. the addresses, K_{nk} , correspond to the arguments of a sine wave). The N^2 calculation steps are detailed in Fig.3.1, and the block diagram of the system to implement these steps is given in Fig. 3.2.

Examination of Fig.3.1 reveals that the n th row of K_{nk} addresses is the same as the n th column of K_{nk} addresses. The DFTTLU calculation steps can thus be solved row by row or column by column. The row by row method or 'Rows Method' is similar to the algorithm used to calculate Fourier Coefficients; the procedure simply being repeated N times. The Rows Method is detailed in 3.2.1. The Columns Method implements the calculation steps by generating columns of address pairs and adding the contents of the specified address to the corresponding Accumulator. Each address pair in a column of address pairs is

associated with a different harmonic and the Accumulator associated with the particular harmonic is incremented. The columns method is described in 3.2.2.

Some notes on the DFTLU system in Fig.3.2.

1. Only imaginary components of the harmonics are extracted.
2. Initially the Accumulators are set to zero.
3. The controller allows N samples of the signal to be taken and the coded amplitude values are stored in the N location I_n array.
4. The SAG is set to state B (cf. Fig.2.2) before a new row or column of K_{nk} addresses are generated.
5. Strobing the SAG causes a K_{nk} value to be generated according to the value of index k .

3.2.1 The Rows Method

Consider Fig.3.2, which shows a system having eight elements for purposes of explanation (see A7). The control is programmed to calculate each harmonic separately as in the system described in section 3.2

- 1) The controller sets the required frequency index on the address generator and switches the corresponding Accumulator on to the adder.
- 2) The controller strobes the SAG and addresses the first location in the I_n array. The output of the SAG and the array form the first address pair, $I_o K_{ok}$.

$$\begin{aligned}
F_0 &\propto S(I_0K_{00}) + S(I_1K_{10}) + S(I_2K_{20}) + S(I_3K_{30}) + S(I_4K_{40}) + S(I_5K_{50}) + S(I_6K_{60}) + S(I_7K_{70}) \\
F_1 &\propto S(I_0K_{01}) + S(I_1K_{11}) + S(I_2K_{21}) + S(I_3K_{31}) + S(I_4K_{41}) + S(I_5K_{51}) + S(I_6K_{61}) + S(I_7K_{71}) \\
F_2 &\propto S(I_0K_{02}) + S(I_1K_{12}) + S(I_2K_{22}) + S(I_3K_{32}) + S(I_4K_{42}) + S(I_5K_{52}) + S(I_6K_{62}) + S(I_7K_{72}) \\
F_3 &\propto S(I_0K_{03}) + S(I_1K_{13}) + S(I_2K_{23}) + S(I_3K_{33}) + S(I_4K_{43}) + S(I_5K_{53}) + S(I_6K_{63}) + S(I_7K_{73}) \\
F_4 &\propto S(I_0K_{04}) + S(I_1K_{14}) + S(I_2K_{24}) + S(I_3K_{34}) + S(I_4K_{44}) + S(I_5K_{54}) + S(I_6K_{64}) + S(I_7K_{74}) \\
F_5 &\propto S(I_0K_{05}) + S(I_1K_{15}) + S(I_2K_{25}) + S(I_3K_{35}) + S(I_4K_{45}) + S(I_5K_{55}) + S(I_6K_{65}) + S(I_7K_{75}) \\
F_6 &\propto S(I_0K_{06}) + S(I_1K_{16}) + S(I_2K_{26}) + S(I_3K_{36}) + S(I_4K_{46}) + S(I_5K_{56}) + S(I_6K_{66}) + S(I_7K_{76}) \\
F_7 &\propto S(I_0K_{07}) + S(I_1K_{17}) + S(I_2K_{27}) + S(I_3K_{37}) + S(I_4K_{47}) + S(I_5K_{57}) + S(I_6K_{67}) + S(I_7K_{77})
\end{aligned}$$

Fig. 3.1 Calculation Steps for 8 point DFTTLU

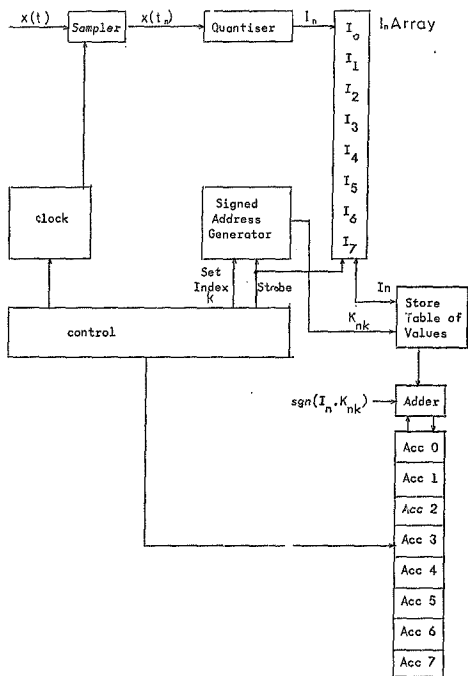


Fig.3.2 Block Diagram of System to Perform Spectral Analysis

3) The contents of the address, I_{ok} in the STV, denoted $S(I_{ok})$ are added to the Accumulator.

4) The controller again strobes the SAG and addresses the next location in the I_n array. The two outputs form the next address pair.

5) The contents of this address in the STV are then added to the Accumulator.

6) The above procedure is repeated for the remaining address pairs and the final value in the Accumulator is

$$S(I_{ok}) + \dots + S(I_{nk}) \propto F_k$$

7) The controller sets the next frequency index k on the SAG and switches the corresponding Accumulator on to the adder.

8) The above procedure is repeated for all the remaining harmonics.

3.2.2 The Columns Method

Consider Fig.3.1. Column i of the signed addresses is the same as row i . If the frequency index, k , is set to zero and the SAG is strobed N times, the first column of signed addresses will be generated. In any column of address pairs, the I_n component does not change but each value in the STV addressed by one of these address pairs must be added to its corresponding Accumulator eg. the value obtained by the second address pair in a column must be added to the second Accumulator in Fig.3.2. To solve the DFTLU column by column the controller in Fig.3.2 must carry out the following steps:

- 1) The controller sets the index k on the SAG.
- 2) The controller selects the value of I_n in the array where $n = k$ and switches it through to one of the address inputs of the STV.
- 3) The controller switches the first Accumulator on to the adder and strobes the SAG.
- 4) The first address pair, $I_0 K_{0k}$, obtains the contents of the STV and adds it to the first Accumulator.
- 5) The controller switches the second Accumulator on to the adder and strobes the SAG.
- 6) The second address pair obtains the corresponding contents of the STV and adds it to the second Accumulator.
- 7) This procedure is repeated for the remaining Accumulators.
- 8) The remaining columns of address pairs are processed similarly.

3.3 Discussion on the Columns and Rows Methods

The Columns method is less complicated to programme as only the K_{nk} component of the address pair changes as each column of address pairs is generated. The disadvantage is that a different Accumulator must be incremented or decremented for each of the address pairs in the column. This problem is overcome by linking the selection of the Accumulators to the strobing of the SAG and the required Accumulator will be selected as each of the K_{nk} values

are generated. The Columns method becomes a real time operation if a column of address pairs can be processed in less than the sampling period and, after the N columns of address pairs have been processed, the Accumulators will contain total proportional to the DFT points. The I_n array is not needed as the column of address pairs can be processed as soon as the I_n value is available from the LADC.

The Nova 1200 instruction set execution times do not permit a column of K_{nk} values to be generated in less than the sampling period and real time operation cannot be achieved. The use of TTL hardware to achieve real time operation is discussed in 6.2. The I_n array must be retained to store the N time samples of the signal burst. The non-real time algorithm and Assembler programme used to process the signal burst is described in A3 and A4 respectively. The most important details of A3 and A4 are summarized here for completeness.

From Fig. A3.3 it can be seen that if the first row and the first column are not counted, the K_{nk} addresses repeat after the row or column in which k or n equal $\frac{N}{4}$ or, in some cases, $\frac{N}{8}$. Thus only the first $\frac{N}{4}$ or $\frac{N}{8}$ columns of address pairs need be generated. The I_n values that share the same columns of K_{nk} values are shuffled out of the I_n array and are stored in a sub-array. These values of I_n follow a similar pattern to the 'bit reversed' pattern⁵ of the FFT and are shuffled in a similar manner. Processing of the DFTTLU cannot begin until all N samples of the signal have been taken and stored in the I_n array of N locations. The advantage of the

modified Columns method is that one column of K_{nk} addresses can be used to generate 4 or 8 columns of address pairs.

The Rows method is the same as the method used to calculate the Fourier Coefficients and this method is repeated N times to solve the DFTLU. In each row the I_n and K_{nk} component of the address pair changes N times and this complicates the programming. Thus the modified columns method is chosen as the basis of the algorithm.

4 THE DETAILED DESCRIPTION OF THE DISCRETE FOURIER TRANSFORM ALGORITHM USING THE TABLE LOOK UP METHOD

4.1 Introduction

The derivation of the integration weights, STV, algorithm and Assembler programme is given in A1, A2, A3 and A4 respectively. The important details of these appendices are given in this chapter under the general headings of:

- 1) The definition of the amplitude quantising levels (the abscissas of the integration formulae), and the resulting integration weights and constants w_i, u_j, h_x, h_y .
- 2) The derivation of the STV, the machine code values that correspond to the STV and the resulting scaling factors D_x and D_y .
- 3) The numerical values of the DFTLU harmonics and the overall machine code scale factor. The overflow and underflow of the Accumulators is considered and the STV and overall scale factor are adjusted to solve this problem. The overall scale factor for the different values of N and for the adjusted STV are tabulated at the end of this chapter.

4.2 The System

The system has two inputs, the X and the Y channel. The X channel consists of N samples of the noise signal which are quantised logarithmically and encoded in the sign magnitude form by the LADC. The LADC has 19 levels spaced at 3dB intervals

and the output word has values between 0_8 and 22_8 . A negative input signal is indicated by setting the most significant bit of the word (Bit zero on the Nova 1200) to one. The output of the LADC (excluding the sign bit) forms half the address pair of the STV. The maximum value of the noise signal is defined to be ± 1 (equivalent to about $\pm 2.5V$) and the integration weights w_i and constant h_x are derived accordingly in A1.1.

The Y channel input is an algorithm, termed the SAG, which generates addresses, K_{nk} , that are equivalent to the arguments of a sinusoidal wave. K_{nk} has values between 0_8 and 17_8 . A negative valued point on the sinusoidal wave is indicated by setting the most significant bit of K_{nk} to one. The K_{nk} word, excluding the sign bit, forms the other half of the STV address pair. The maximum value of the sinusoidal wave is ± 1 and the integration weights v_j and constant h_y are derived accordingly in A1.2. The SAG must generate $N^2/8 K_{nk}$ addresses (see Chapter 3) in order to process a N point transform.

The STV is a 17_8 by 22_8 array and is derived in A.2. The sign bits of the LADC output and K_{nk} form the inputs of the signum function. Only the first $\frac{N}{2}$ harmonics are calculated and there are $\frac{N}{2}$ Accumulators for the real harmonic components and $\frac{N}{2}$ Accumulators for the imaginary harmonic components. The resultant harmonic is then calculated from its real and imaginary components.

The program is divided into the following subprograms

- 1) N samples of the signal are taken at a rate set by an external

In 2.5 it was shown that the harmonics of the DFTLU are approximately equal to the harmonics of the DFT algorithm for the same input signal.

The definition of the DFT⁵ from eqn. 2.15

$$X(kN) = \sum_{n=0}^{N-1} x_s(nT) e^{-j2\pi nk/N} \quad 4.1$$

Consider $x_s(nT)$ is a constant maximum signal (ie zero frequency - dc level).

$$x_s(nT) = 1 \quad n = 0, 1, \dots, N-1 \quad 4.2$$

Then

$$X(kN) = N \quad k = 0 \quad 4.3$$

$$\text{and } X(kN) = 0 \quad k = 1, 2, \dots, N-1 \quad 4.4$$

Consider the case where $x_s(nT) = \sin(\frac{2\pi n}{N})$ ie $k = 1$

$$\text{Then } X(kN) \leq \frac{N}{2} \text{ for } k = 1 \quad 4.5$$

$$X(kN) = 0 \quad k \neq 1 \quad 4.6$$

$(\frac{N}{2})$ is the maximum value that $X(kN)$ can have for a time varying signal of peak value ± 1 . The derivation and values of $(\frac{N}{2})$ are given in 4.4. In the dissertation all harmonics will be

measured with respect to $(\frac{N}{2})$ and a harmonic that has a magnitude half the maximum value is written as

$$X(kN) = 0,5(\frac{N}{2})$$

The decibel scale is defined

$$\text{OdB} \equiv (\frac{N}{2})$$

and a harmonic of $0,5(\frac{N}{2})$ can be written in dB as

$$20 \lg \frac{0,5(\frac{N}{2})}{(\frac{N}{2})} \doteq -6,02 \text{dB} \quad 4.7$$

4.4 DEFTLU Scale Factors

When the algorithm derived in 3.2.2 is programmed, the constants in the STV must be represented by a 2's complement word.

From A2, the maximum constant that has to be stored in the STV is

$$3,407545177$$

The machine code that is chosen to represent this value is

$$40\ 000_8 = 16\ 384_{10} = 2^{14}$$

The remaining constants in the STV are scaled up by the value

$(D_x D_y)$, (cf. eqn 2.37/2.38) where

$$D_x D_y = \frac{16\ 384}{3,407\ 545\ 177}$$

The fractional part of the machine code values of the STV are truncated.

The STV with a maximum value of 2^{14} is defined as

$$S_{14}(I_{n\ nk})$$

If the machine code used to represent 3,407 545 177 is

$$20\ 000_8 = 2^{13} = 8\ 192_{10}$$

the STV is denoted as:

$$S_{13}(I_{n\ nk})$$

ie. If each constant in S_{14} is halved (the machine code is shifted one place to the right), the resulting STV will be

$$S_{13}(I_{n\ nk})$$

Consider the case where the STV is $S_{14}(I_n K_{nk})$ and substituting this into equation 2.37/2.38.

$$F_k = \frac{h_x h_y}{D_x D_y} \sum_{n=0}^{N-1} \text{sgn}(I_n K_{nk}) S_{14}(I_n K_{nk}) \quad 4.8$$

From A1 and A2

$$h_x = 0,3431557502$$

$$h_y = 1.0$$

$$\text{and } (D_x D_y) = \frac{16384}{3,407545177}$$

Substituting these values into $\frac{h_x h_y}{D_x D_y}$ and factorising

$$\text{ie } \frac{h_x h_y}{D_x D_y} = \frac{(0,3431557502)(1.0)(3,407545177)}{(16384)} \quad 4.9$$

$$\frac{h_x h_y}{D_x D_y} = \frac{1}{(2048)(6,841890625)} \quad 4.10$$

$$\text{ie } \frac{h_x h_y}{D_x D_y} = \frac{1}{(2048)(7)} \quad 4.11$$

and substituting into 4.8

$$F_k = \frac{1}{(2048)(7)} \sum_{n=0}^{N-1} \text{sgn}(I_n K_{nk}) S_{14}(I_n K_{nk}) \quad 4.12$$

This form of the equation is easy to solve with a digital computer that uses integer arithmetic.

The computer is programmed to solve the following equation:

$$(2048)F_k = \frac{1}{7} \sum_{n=0}^{N-1} \text{sgn}(I_n K_{nk}) S_{14}(I_n K_{nk}) \quad 4.13$$

The 2048 is considered a computing scale factor. If overflow or underflow of an Accumulator occurs, each constant in the STV is halved and the time samples are reprocessed. Equation 4.9 would then be written as

$$\frac{h_x h_y}{D_x D_y} = \frac{(0.3431557502)(1.0)(3.407545177)}{(8192)} \quad 4.14$$

$$\text{i.e. } \frac{h_x h_y}{D_x D_y} \doteq \frac{1}{(1024)(7)} \quad 4.15$$

The computer would then solve the following equation

$$(1024)F_k = \frac{1}{7} \sum_{n=0}^{N-1} \text{sgn}(I_n K_{nk}) S_{13}(I_n K_{nk}) \quad 4.16$$

The above process would be repeated until no overflow or underflow occurred in the Accumulators.

The general equation is

$$(\text{overall scale factor}) F_k = \frac{1}{7} \sum_{n=0}^{N-1} \text{sgn}(I_n K_{nk}) S(I_n K_{nk}) \quad 4.17$$

The derivation of $(\frac{N}{2})$ defined in 4.3, can now be discussed in the light of equation 4.17.

Consider the case of a $N = 128$ point DFTTLU with an STV S_{11} (i.e. the overall scale factor is 256).

$$(256)F_k = \frac{1}{7} \sum_{n=0}^{127} \text{sgn}(I_n K_{nk}) S_{11}(I_n K_{nk}) \quad 4.18$$

From equation 2.36, equation 4.1 can be written as:

$$(256)X_k = 256 \sum_{n=0}^{127} x_s(nT) e^{-j2\pi nk/128} \quad 4.19$$

Consider the case where a signal

$$x_s(nT) = \sin \frac{2\pi n}{128} \quad k = 1 \quad (\text{as in section 4.3})$$

is processed, both equations 4.18 and 4.19 should give a result less than or equal to 16384. (This is not the case in practice, as equation 4.18 is only valid for noise like signals). 16384 is equivalent to $(\frac{N}{2})$, defined in section 4.3, for the above case.

In Table 4.1, the overall scale factors, the values of $(\frac{N}{2})$, and the corresponding STVs are tabulated for $N = 128, 256, 512, 1024$. The maximum 16 bit 2's complement number that has been chosen to represent $\frac{N}{2}$ is 16384. (i.e. 40 000₈). Thus the STV, S_{14} , (Table A2.3), which has a resolution of 15 bits, will always be used with a resolution of 12 bits or less. This accounts for the blank spaces in Table 4.1.

Table 4.1 $(\frac{N}{2})$ Values

Overall Scale Factor	STV	$(\frac{N}{2})$ Values			
		$N = 128$	$N = 256$	$N = 512$	$N = 1024$
2048	S_{14}				
1024	S_{13}				
512	S_{12}				
256	S_{11}	16 384			
128	S_{10}	8 192	16 384		
64	S_9	4 096	8 192	16 384	
32	S_8	2 048	4 096	8 192	16 384
16	S_7	1 024	2 048	4 096	8 192

4.5 Discussion

The Assembler programme in A4 computes equation 4.17 and automatically adjusts the STV until overflow or underflow of the Accumulators (which contain the partial sum of the harmonics) is eliminated. The programme then lists the number of times the STV constants have been halved and which of the Accumulators had overflowed or underflowed. Once the DFTLU of a signal burst has been computed, the overall scale factor is obtained from Table 4.1, given N and the number of times the STV was adjusted. The layout of the Accumulators in the core is given in A 3.8.7 and subprogrammes are written to analyse or display the harmonic values in the Accumulators. The overall scale factor has been made a positive integer power of 2 and the machine coded harmonic values can be easily scaled to their proper values by shifting them the required number of times to the right. The DFTLU harmonics are also in a suitable form to be compared with the FFT harmonics. This comparison is discussed in Chapter 5.

5 ERROR ANALYSIS

5.1 Introduction

The error characteristics of the DFTTLU can be investigated using the analysis in Chapter 4 of reference 6. This analysis involves the investigation of time and amplitude sampling errors as well as computational errors such as truncation errors and the errors introduced by the abscissa integration formula. The joint probability density function of the noise signal and the N sine and cosine signals must also be calculated to implement this rigorous error analysis. The results of this analysis would show how the DFTTLU of a sampled signal differed from the Fourier Transforms of the continuous signal. However numerical methods and digital systems are used in most modern practical signal processing systems and it would be more useful to know how the results of the DFTTLU differ from the results of another digital Fourier Analysis system of known accuracy given the same sampled time signal. These results would be of practical use to a signal processing system designer faced with the task of choosing a Fourier Analysis system.

The Fast Fourier Transform (FFT) algorithm^{5,16} is used as the Fourier Analysis system of known accuracy.¹⁸ The Assembler programme uses integer arithmetic and can process a maximum of 1 024 complex points (see appendix A5). The FFT harmonics are regarded as the true values and the differences between the FFT and DFTTLU harmonics are regarded as the errors which are analysed

in two ways. One method is to plot each DFTTLU harmonic and its associated error. The other method is to classify the errors according to the magnitude of the associated DFTTLU harmonic and then to calculate an average value of each group of errors.

Clearly the machine code values of the DFTTLU and FFT harmonics must be referred to the same value of $(\frac{N}{2})$ before errors can be calculated. The sampling subprogramme (A4.3) must control the LADC and the ADC (used in conjunction with the FFT) and these peripherals must sample the signal simultaneously. After the two sets of harmonics have been computed the results must either be plotted or averaged. These Assembler programmes are discussed in appendices A4, A5 and A6 while the error plots and error averages are in 5.2 and 5.3 respectively.

5.2 Plotting the Harmonics

The programmes required are:

- 1) The Fast Fourier Transform, G_k , $k = 0, 1 \dots (N-1)$
to supply the true harmonics.
- 2) The DFTTLU. The harmonics are denoted F_k , $k = 0, 1 \dots (N-1)$
- 3) A programme to scale the two sets of harmonics, G_k and F_k , so that comparisons can be made.
- 4) A programme to calculate $G_k - F_k$ and to plot F_k and $G_k - F_k$.

These results are passed to a 10 bit digital to analog converter which is connected to an XY plotter. The $G_k - F_k$ and

the F_k values are plotted on the Y axis while the X axis is the frequency index (k) axis. Band pass, low pass and band stop filtered noise is analysed for $N = 128, 256, 512$ and 1024 and fig 5.1 shows the format of the plot. Fig 5.2 shows a plot of band pass filtered noise and the errors associated with each harmonic.

5.2.1 Scaling the Harmonics, F_k and the Errors, $G_k - F_k$, for the 10 bit Digital to Analog Converter (DAC)

The 10 bit DAC can only process numbers that are in the range -512_{10} to 511_{10} (-1000_8 to 777_8). The format of the A4 page (pages) is given in Fig.5.1. In the case where $N=1024$ and 512 harmonics are plotted, 128 harmonics are plotted to a page for clarity and 4 pages are needed. F_k is plotted in the top half of the page between $Y = 0$ and $Y = 511$. The errors are plotted in the Y direction about $Y = -256$. Errors greater than zero lie between $Y = -256$ and $Y = 0$. Errors less than zero lie between $Y = -256$ and $Y = -512$.

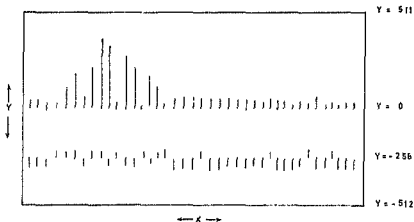


Fig.5.1 Plotter Format

The program calculates the following equation

$$(\text{scale factor})F_k = \left(\frac{1}{2}\right)\left(\frac{1}{N}\right) \sum_{n=0}^{N-1} \text{sgn}(I_n K_{nk}) S(I_n K_{nk}) \quad 5.1$$

The extra factor of a half is included so that the harmonics will not exceed 511, the positive vertical range limit of the plotter. The 'scale factors' in Table 5.1 are half the corresponding 'overall scale factors' in Table 4.1. The fraction of $(\frac{N}{2})$ that corresponds to $Y = 512$ is given in Table 5.1 in place of the value of $(\frac{N}{2})$ in Table 4.1.

These fractions of $(\frac{N}{2})$ are calculated as follows:

Consider a case where $(\frac{N}{2}) = 16\,384$ in Table 4.1. The corresponding value would be 8192 in Table 5.1 (ie. $8192 = (\frac{N}{2})$ for equation 5.1). 512 is one sixteenth ($\frac{1}{16}$) of 8192. Thus $Y = 511$ ($Y = 512$ can not be plotted) is marked as $\frac{1}{16}(\frac{N}{2})$

The 'scale factors', STVs and fractions of $(\frac{N}{2})$ that correspond to $Y = 512$ are tabulated in Table 5.1 for $N = 128, 256, 512, 1024$.

5.2.2 Discussion

The harmonic plots are not intended to give numerical values of errors, but rather to show trends in errors. In fig 5.3 an amplitude distribution of errors associated with the band stop and band pass regions is given. Two trends, valid for band pass, low pass and band stop filtered noise, emerge.

- 1) The DFTLU estimate of low magnitude harmonics is greater than that of the FFT.
- 2) The difference in the estimates of the higher magnitude

harmonics follow a random pattern and have lower values than the lower magnitude harmonic differences.

These results are consistent with those obtained in the error analysis of Fourier Series Coefficient in Chapter 4.8 of reference 6. The results of the harmonic plots and the simple amplitude distributions suggest further investigation into the variation of errors with the harmonic amplitude and the calculation of a mean value of the random errors.

Table 5.1 Scales for Harmonic Plots.

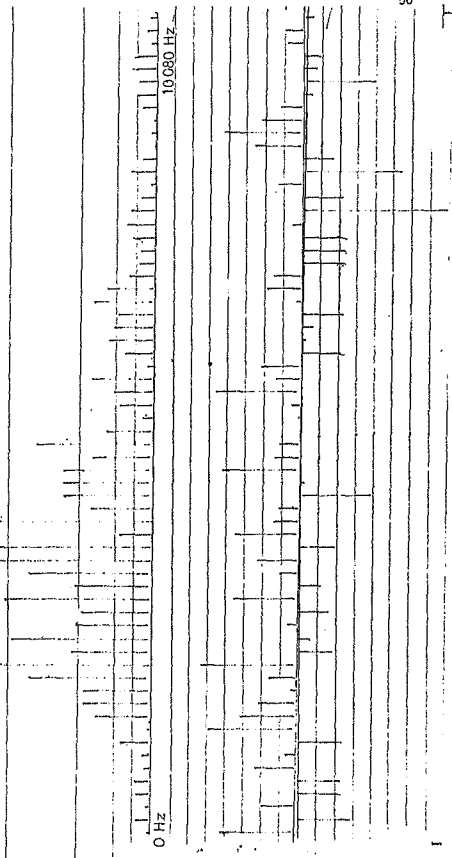
Scale Factor	STV	Value of Harmonic at $Y = 512$			
		$N = 128$	$N = 256$	$N = 512$	$N = 1024$
1024	S_{14}				
512	S_{13}				
256	S_{12}				
128	S_{11}	$\frac{1}{16} \left(\frac{N}{2}\right)$			
64	S_{10}	$\frac{1}{32} \left(\frac{N}{2}\right)$	$\frac{1}{16} \left(\frac{N}{2}\right)$		
32	S_9	$\frac{1}{64} \left(\frac{N}{2}\right)$	$\frac{1}{32} \left(\frac{N}{2}\right)$	$\frac{1}{16} \left(\frac{N}{2}\right)$	
16	S_8	$\frac{1}{128} \left(\frac{N}{2}\right)$	$\frac{1}{64} \left(\frac{N}{2}\right)$	$\frac{1}{32} \left(\frac{N}{2}\right)$	$\frac{1}{16} \left(\frac{N}{2}\right)$
8	S_7	$\frac{1}{256} \left(\frac{N}{2}\right)$	$\frac{1}{128} \left(\frac{N}{2}\right)$	$\frac{1}{64} \left(\frac{N}{2}\right)$	$\frac{1}{32} \left(\frac{N}{2}\right)$

Fig. 5.2 HARMONIC PLOTS

N	Δ (Hz)
128	160
256	80
512	40
1 024	20

DP12.81
N=128
0.5 Vrms 2KHz -4KHz B Pass
Sampling Rate = 20.48KHz
SR5 = 4
SCNT = 0
2(MAN-SCNT) = 8

1(N)
32 Z



DP 2561

N=256

0.5Vrms 2KHz -4KHz B. Pass

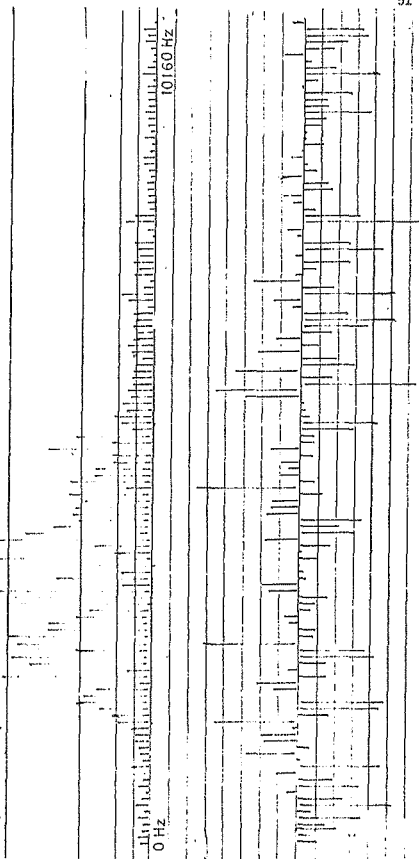
Sampling Rate = 20.48 KHz

SR5 = 5

SCNT = 0

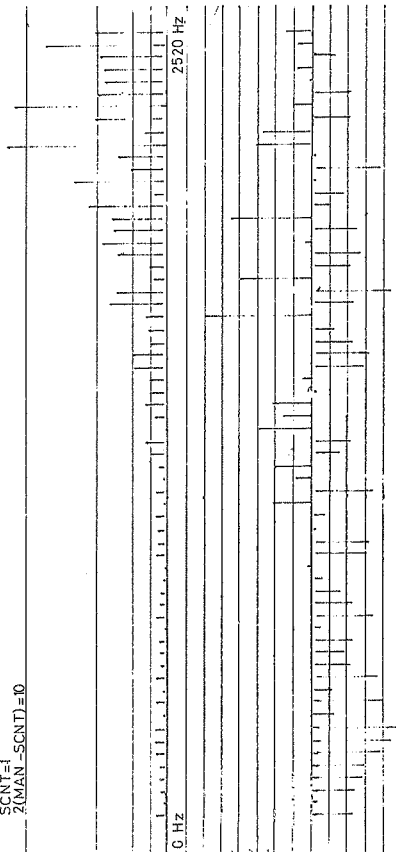
2(MAN-SCN T)=10

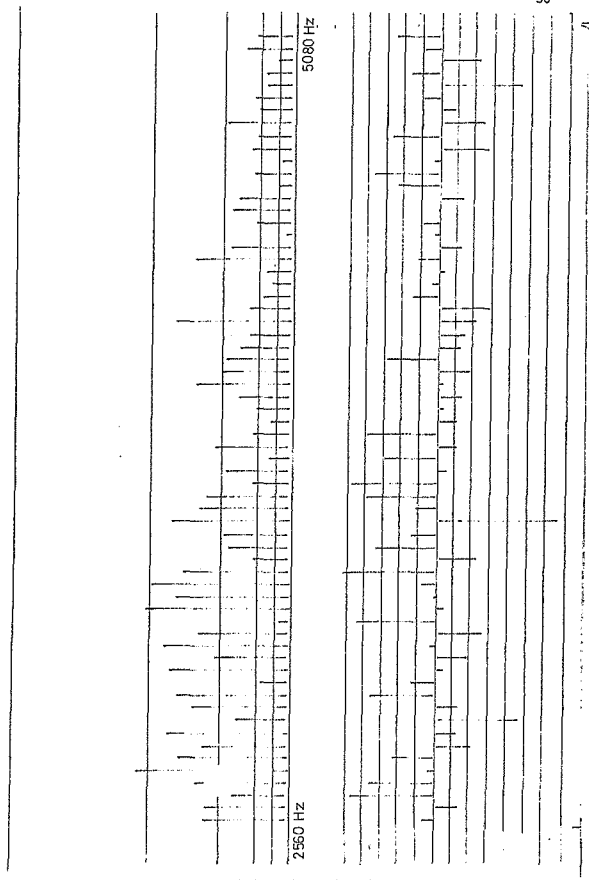
$\frac{1}{32} \frac{N}{2}$

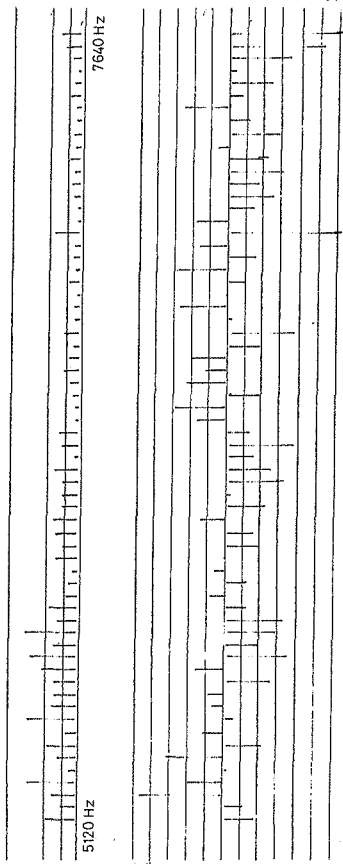


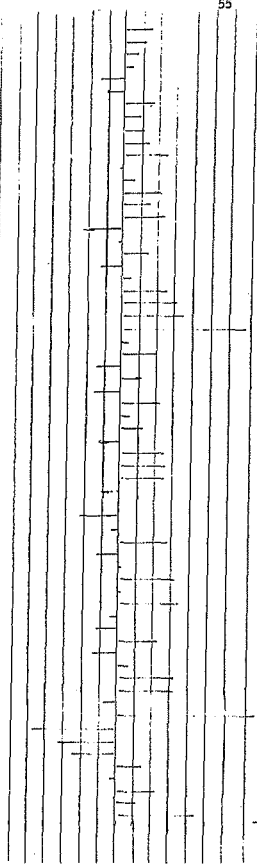
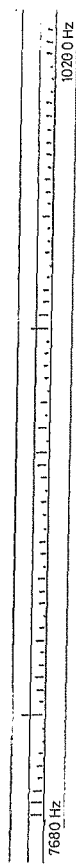
DP5121
 N=512
 0.5Vrms 2KHz-4KHz B.Pass
 Sampling Rate=2048KHz
 SR5=6
 SCNT=1
 2(MAN-SCNT)=10

$\frac{1}{32} \left(\frac{N}{2} \right)$





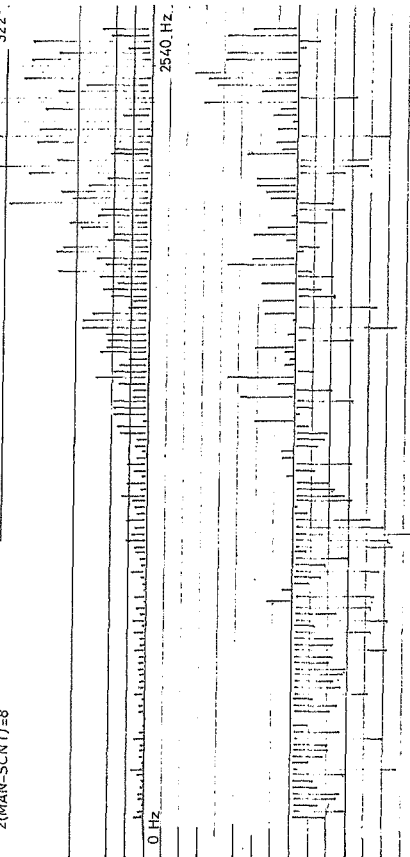


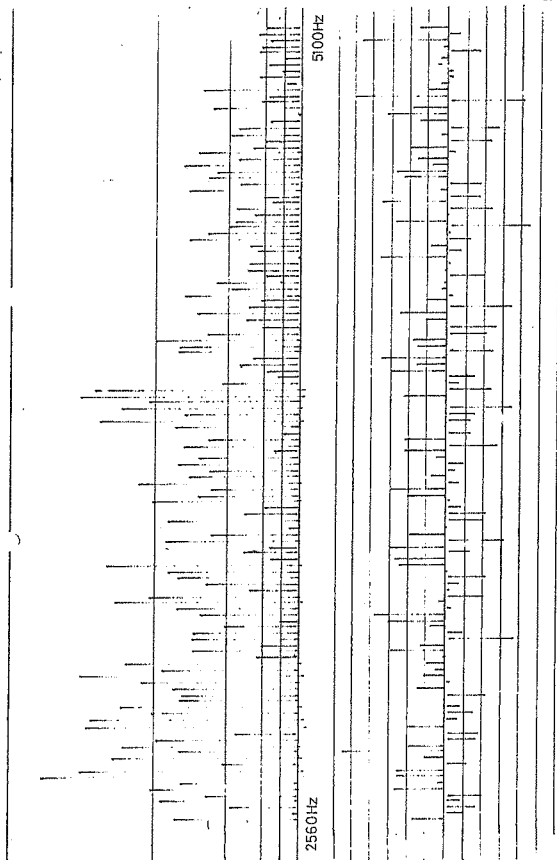


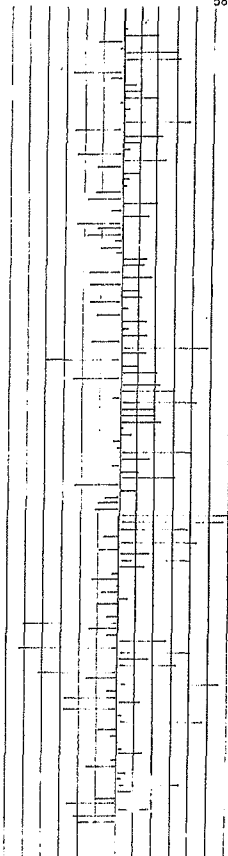
DP1024I
 N=1024
 0.5 V rms 2 KHz -4 KHz B Pass
 Sampling Rate = 20.48 KHz
 SR5=6
 SCNT=2
 2(MAN-SCNT)=8

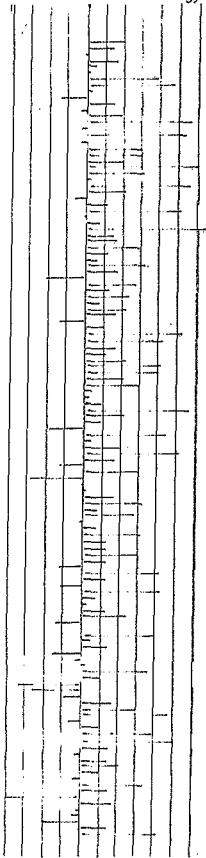
16 (N)

32 (N)









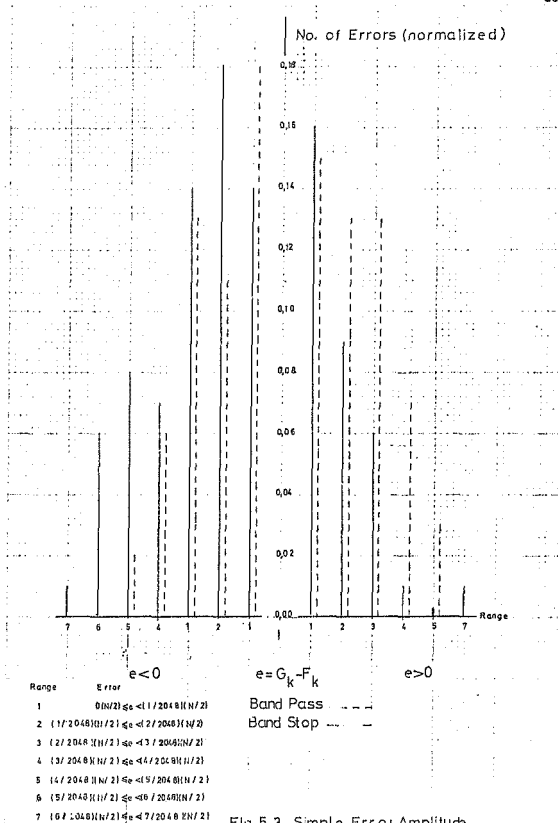


Fig. 5.3 Simple Error Amplitude
Distribution of DP 10241 in fig. 5.2

5.3 A Numerical Error Analysis

The plots of the harmonics and their errors in Fig.5.2 show that the errors have random magnitudes and signs. The section deals with a method of calculating a mean value of the errors and investigating the variation of the errors with the magnitudes of the harmonics. In this dissertation, the term 'spurious response' is used to describe harmonics that have a zero or very small value. In Fig.5.2, the errors associated with the spurious response tend to have larger magnitudes and have the same sign. The programmes needed for this analysis are:

- 1) The FFT programme.
- 2) The DFTLU programme.
- 3) The scaling programme.
- 4) A Programme that quantises F_k and classifies the errors accordingly. It then calculates a mean value of each group of errors.

The result is a graph of mean error plotted against harmonic magnitude.

5.3.1 Quantising the Harmonics

The harmonic is coarsely quantised so that the number of harmonics that fall into any quantising level is reasonably high and statistically meaningful averages can be calculated. The maximum value of any harmonic is $(\frac{N}{2})$ and this is divided into approximately 6dB quantising levels.

eg $(\frac{N}{2})$, $\frac{1}{2}(\frac{N}{2})$, $\frac{1}{4}(\frac{N}{2})$

The maximum machine code value that can represent $(\frac{N}{2})$ is $16\ 384 = 2^{14}$. The quantising programme calculates the ranges according to the following formula:

$$2^{p-1} \leq H_p < 2^p \quad p = 1, 2, \dots, 12, 13, 14. \quad 5.2$$

H_p are those harmonics that have a value in the range

defined above. The number of harmonics in the limits is denoted N_p . There are 15 quantising levels, this being set by choosing 2^{14} to be the maximum value of $(\frac{N}{2})$. If overflow or underflow of the Accumulators occurs (A3.10.5) and the STV is halved, $(\frac{N}{2})$ is also halved and the quantising level (levels) above the new value of $(\frac{N}{2})$ will be empty. Fig.5.4 shows the spacing of the quantising level on a linear scale.

5.3.2 Definition of Error Terms

As in the previous case (5.2) the error in a harmonic is defined as:

$$\text{error} = G_k - F_k \quad 5.3$$

In this case the magnitude of the error is used.

$$e = |G_k - F_k| \quad 5.4$$

The errors, e , that are associated with harmonics

in the range H_p are denoted e_p . The mean error,

E_p is defined as

$$E_p = \frac{1}{N_p} \sum_{N_p} e_p \quad 5.5$$

ie E_p is the average of the magnitudes of the errors associated

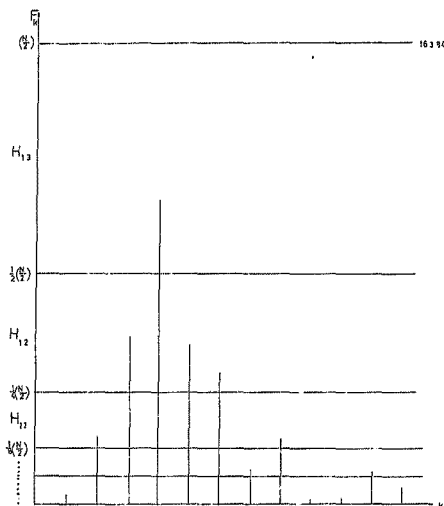


Fig.5.4 Amplitude quantisation of the Harmonics

with harmonic magnitudes in the range H_p . The standard deviation of e_p is denoted σ_p and is defined as

$$\sigma_p = \sqrt{\frac{\sum_N (e_p)^2 - (\sum_N e_p)^2 / N_p}{N-1}} \quad 5.6$$

The percentage mean error is

$$E_p / (N/2) \times 100 \% \quad 5.7$$

The percentage standard deviation is

$$\sigma_p / (N/2) \times 100 \% \quad 5.8$$

The Assembler programme that computes e_p , $(e_p)^2$ and N_p is given in A4.12.7.

5.3.3 Error Tests

The system that implements the error tests is given in A6. The input signal consists of filtered noise which amplified to have an rms value of about 2V at the ADC and is attenuated to about 0,5V rms at the LADC input.

Test One

The constants in the STV are adjusted so that the machine code of $40\,000_8$ is equivalent to $(\frac{N}{2})$. Filtered noise is processed for $N=128,256,512$ and $1\,024$. Errors from about 30 transforms are averaged to get repeatable results for E_p and σ_p .

Test Two

This test is similar to test one but the machine code equivalent to $(\frac{N}{2})$ is set to $20\,000_8$ ie One less bit is used to represent the constants in the STV.

Test Three

This test is similar to test one but the machine code equivalent to $(\frac{N}{2})$ is set to $10\,000_8$.

Test Four

The attenuator (see A6) is set to 14,7 dB, 17,7dB and 8,7dB. In each case tests similar to test one are performed and E_p is

measured. It was not possible to measure σ_p as there was not enough memory core to hold the results of $(e_p)^2$ (see A4.12.7). The STV is adjusted to maximum possible resolution ie. As many bits as possible are used to represent the constants in the STV without Accumulators overflowing or underflowing.

5.3.4 Discussion of Test Procedure

Only band pass and low pass filtered noise is used in the above tests. In this dissertation wide band low pass filtered noise is noise that is cut off at 5kHz while narrow band low pass filtered noise is cut off at 2kHz. Wide band pass filtered noise has a pass band from 2kHz to 5kHz. Narrow band pass filtered noise has a pass band from 2,5kHz to 3,5kHz. In all cases the roll off is 24dB/octave.

In test one the maximum value of $(\frac{N}{2})$ (ie. the maximum harmonic magnitude that could occur) is 40 000₈. STVs S_{11} , S_{10} , S_9 , S_8 are used for $N=128$, 256, 512, 1024 respectively. The effects of using one less bit to represent the constants in the STV are investigated in tests two and three. Test four investigates superficially the effect of overloading or underloading the LADC.

5.3.5 Discussion of Error Test Result

The processing of noiselike signals results in harmonics that have large variations in magnitude and errors from at least thirty transforms must be accumulated before repeatable values of E_p and σ_p can be calculated. The results of the error tests

are in the form of a graph of E_p and σ_p plotted as a function of H_p . In most of the results E_p and its corresponding value of σ_p differed by less than 0,01 per cent of $(\frac{N}{2})$ in magnitude and both are represented by the same line on the graph.

If wide band low pass or wide band pass filtered noise is processed, there is an approximately even distribution of harmonic magnitudes in the H_p ranges and an error characteristic similar to Fig.5.5 is obtained. This result confirms those in section 4.8 or 5.4 of reference 6. Reducing the resolution of the STV by 2 bits has no effect on the results in Fig.5.5.

If narrow band low pass or narrow band pass filtered noise is processed, there is an uneven distribution of harmonic magnitudes, the number of high magnitudes being much less than the number of low magnitudes. If the results of 30 - 60 transforms are accumulated, the number of harmonics in the higher H_p ranges is of the order of 10 - 20 while the number of harmonics in the lower H_p ranges is of the order of 1000. The values of E_p and σ_p associated with the higher H_p ranges will not be as reliable as those in the lower H_p ranges. The error characteristic is given in Fig.5.6 and the less reliable results are indicated by a dotted line. Fig.5.7 and Fig.5.8 show the variation of E_p and σ_p as the number of bits representing a constant in the STV is reduced.

Tests one, two and three show that:

- 1) If the noise signal being processed has a narrow bandwidth, the STV constants must have maximum resolution for maximum accuracy.

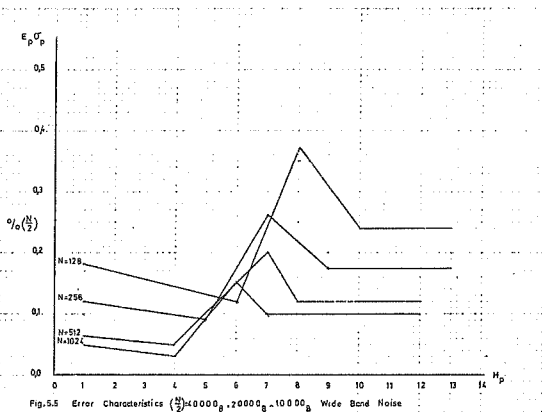
- 2) The higher magnitude harmonics of a narrow band noise signal can have errors of the order of $2\% (\frac{N}{2})$
- 3) The minimum error is of the order of $0,5\% (\frac{N}{2})$
- 4) The accuracy of the lower magnitude harmonics is independent of type of pass band of the noise signal and the resolution of the STV.

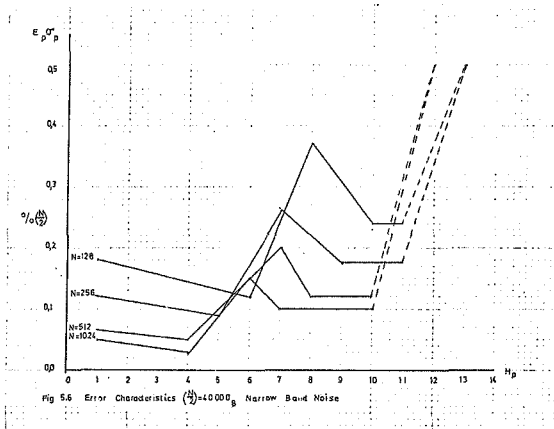
Test four shows that overloading or underloading the LADC can cause errors of the order of $18\% (\frac{N}{2})$ in the high magnitude harmonics. This error is independent of the type of pass band of the noise signal (Fig.5.9).

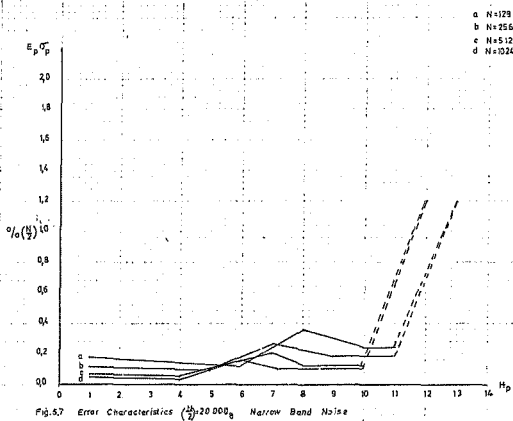
This error analysis is a simple and practical method of obtaining an error characteristic of the DFTTLU using a minicomputer with 16K core and an integer arithmetic facility. The analysis has only been superficially implemented as, for example, the following has not been investigated.

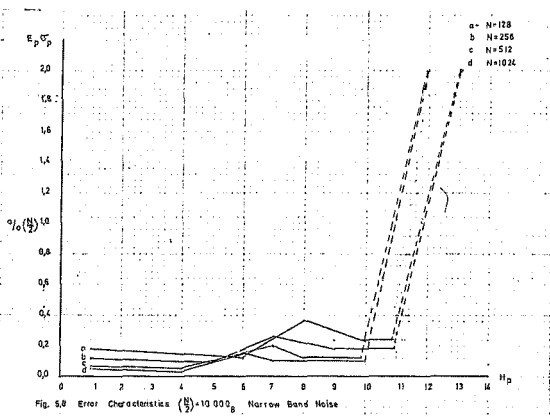
- 1) 3 - 6 bits to represent an STV constant.
- 2) more or less than 16 'abscissas' in the Y channel.
- 3) less than 18 'abscissas' in the X channel.

The investigation has shown that the DFTTLU is a simple and practical algorithm to take Fourier Transforms of noise like signals.









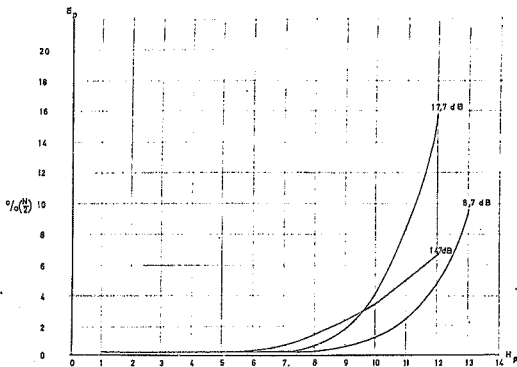


Fig 5.9 Error Characteristics - Varying Attenuator - N any of above values

6 CONCLUSIONS

6.1 General Discussion

The Discrete Fourier Transform of a sampled noise signal can be computed using the table look up algorithm. The differences between the resulting harmonics and the harmonics obtained using the Fast Fourier Transform are less than 0,5% of the maximum harmonic magnitude for a noiselike signal which has been filtered so that it has a pass band of the order of 3000 Hz.

The ultimate aim of the work is the development of a real time Fourier Transform system that processes wide dynamic range noiselike signals - the present system meets all the aims except that of real time operation because the number of calculation steps is proportional to N^2 and the Assembler code needed to generate the K_{nk} addresses is inherently cumbersome. Investigation has shown that the decimation⁵ in time or frequency used by the Fast Fourier Transform to reduce the number of calculation steps to $N \log N$ cannot be applied to the table look up method.

6.2 Real Time Operation

Real time operation can be achieved if a set of harmonics can be processed in a time less than the signal burst time. This means that a column of address pairs (real and imaginary) must be processed in less than the sampling period. The most time consuming operation is the generation of the K_{nk} addresses using the Assembler Code. This operation lends itself to hardware

implementation as the K_{nk} generator is simply an UP/DOWN counter that uses sign/magnitude notation. A basic step in the table look up algorithm (described in Chapter 3.3) is

- 1) Generate a K_{nk} address
- 2) Combine the logarithmic analog to digital converter output, I_n , and K_{nk} to form an address pair.
- 3) Extract the required constant from the Stored Table of Values.
- 4) Adding (or subtracting) to constant to (or from) to correct Accumulator

$\frac{N}{2}$ of the basic steps are required to process a column and the time needed is less than

$$2 \frac{(\text{Sampling period})}{N}$$

Duplicate systems are needed as the real and imaginary harmonic components must be computed simultaneously. The formulae derived in A3.5.3 can be used to simplify the design of the K_{nk} generator ie. When processing a column of address pairs it is simpler to process all the address pairs that contribute to the add harmonics separately, then the even numbered harmonics that are multiples of four and finally the remaining even numbered harmonics. The K_{nk} generator is then limited to specified values in each case. In addition only $\frac{N}{4}$ sets of columns of $\frac{N}{4}$ rows of K_{nk} need be generated.

6.3 Recommendations for Future Work

The logical extension of this work is the design and construction of a fast, simple and relatively accurate Fourier Transform instrument which has the following advantages when compared with a system based on the Fast Fourier Transform.

1) The basic calculation step does not require multiplication. The only multiplication needed is in the calculation of the resultant harmonics.

2) The logarithmic analog to digital converter is less complicated than the linear one required by the Fast Fourier Transform.

3) The wordlength depends on the number of levels in the logarithmic analog to digital converter which is of the order of 16 - 20. The Fast Fourier Transform needs a linear analog to digital converter with about 1 000 - 2 000 levels.

4) The table look up Fourier Transform algorithm is less complex than a Fast Fourier Transform of comparable accuracy.

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A1 Integration Formulae and Integration Weights

1.1 Input Signal Channel Integration Formula

The Logarithmic Analog to Digital Converter LADC quantises the input signal into 3dB levels. The quantising is illustrated in Fig.A1.1.

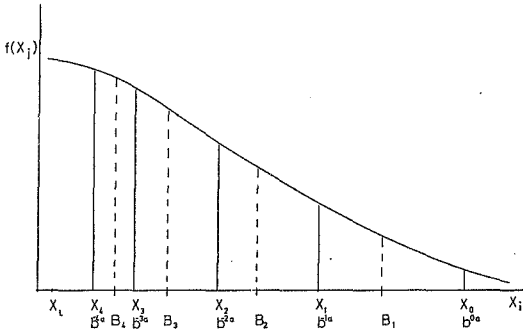


Fig. A1.1 LADC Thresholds

The tangent rule for integration is us. d.⁶

X_i are the thresholds of the LADC

b is the base of the logarithm

a is the index of the logarithm.

The abscissa axis must be divided into integration panels, B_i , to implement the integration.

These panels are defined

$$X_i = \frac{B_i + B_{i+1}}{2} \quad A1.1$$

The quantiser threshold is placed in the centre of the panel.

$$X_i = X_0 b^{-ia} \quad A1.2$$

$$B_i = B_0 b^{-ic} \quad A1.3$$

$$X_0 = \frac{B_0 + B_1}{2} = 1 \quad A1.4$$

(The maximum threshold is defined to be 1).

$$\frac{B_0 + B_1}{2} \approx 1 \quad A1.5$$

$$\frac{B_0 + B_0 b^{-a}}{2} = 1 \quad A1.6$$

$$B_0 = \frac{2}{1 + b^{-a}} \quad A1.7$$

$$B_i = \frac{2b^{-ia}}{1 + b^{-a}} \quad A1.8$$

The area, a_i of a panel i

$$a_i = (B_i - B_{i+1}) f(X_i) \quad A1.9$$

The area under the curve from X_L , the lowest threshold to X_0 is

$$X_0 \int_{X_L} f(x) dx \approx \sum_{i=0}^{M_x-1} a_i \quad A1.10$$

M_x is the number of thresholds.

$$\sum_{i=0}^{M_x-1} a_i = \sum_{i=0}^{M_x-1} (B_i - B_{i+1}) f(X_i) \quad A1.11$$

$$= \sum_{i=0}^{M_x-1} h_x w_i f(X_i) \quad A1.12$$

$$h_x = \frac{2(1 - b^{-a})}{1 + b^{-a}} \quad A1.13$$

$$w_i = b^{-ia} \quad A1.14$$

h_x is the integration constant and w_i is the integration weight.

The area of the panel between $X = 0$ and $X = X_L$ is small and is neglected.

Thus:

$$\int_0^{X_0} f(x) dx \approx \frac{2(1 - b^{-a})}{(1 + b^{-a})} \sum_{i=0}^{M_x-1} b^{-ia} f(X_i) \quad A1.15$$

The notation used for the subscript in w_i and the index in b^{ia} is not compatible with the sinusoidal subscript notation in A1.2. Normally when the subscript is set to zero it is associated with zero on the abscissa axis. In the above case, zero index is associated with X_0 , the maximum abscissa value. The following index numbering modification is introduced to allow a zero numbered subscript to be associated with the weight at X_L .

$$i' = (M_x - 1) - i$$

$$\text{and } w_i = b^{-i'a}$$

The integration weights in table A1.1 are calculated using the above formula.

Table A1.1 The Signal Channel Integration Weights

i	w_i
0	0,00000000000
1	0,002762135866
2	0,00390625
3	0,005524271729
4	0,0078125
5	0,0110485434
6	0,015625
7	0,0220970869
8	0,03125
9	0,0441941738
10	0,0625
11	0,0883883476
12	0,125
13	0,1767766954
14	0,25
15	0,3535533905
16	0,5
17	0,7071066711
18	1,0

$$w_i = b^{-i^t \alpha}$$

$$b = 2,0$$

$$\alpha = 0,5$$

$$i^t = (M_x - 1) - i$$

1.2 The Sinusoidal Channel Integration Formula

1.2.1 Introduction

The problem of generating sine and cosine waves in a digital system is usually complicated. The Table look up Method simplifies this by incorporating the sinusoidal wave values into the integration formula. Thus only the linear in time arguments of the sine and cosine wave need be generated. This section shows how the linear arguments are manipulated mathematically to produce a sinusoidal output.

1.2.2 The Sinusoidal Argument

From chapter 2

$$e^{-j\frac{2\pi nk}{N}} = \cos\left(\frac{2\pi nk}{N}\right) - j \sin\left(\frac{2\pi nk}{N}\right) \quad A1.16$$

where N = number of time samples in the DFT

n = index of time sample n = 0,1 N - 1

k = index of harmonic k = 0,1 N - 1

When taking the periodicity of the sinusoidal wave into account, the maximum value of (nk) is N - 1.

When $\frac{\pi}{2}$ symmetry is also taken into account the maximum value of nk is $\frac{N}{4}$.

The term 'argument' is used for the term (nk). However, the strict definition of argument is $\left(\frac{2\pi nk}{N}\right)$. In this work nk and machine code values that are proportional to (nk) are termed 'arguments'.

1.2.3 'Quantising' the Sine Waves

The quantisation and integration formulae are discussed. It must be noted that no actual sine wave quantiser exists and 'quantising' is implemented by the mathematical algorithm.

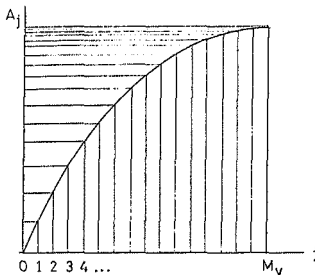


Fig.A1.2 Linearly quantised arguments

$$A_j = \sin\left(\frac{j}{M_y} \frac{\pi}{2}\right) \quad j = 0 \dots M_y \quad \text{A1.17}$$

$$Y_j = \frac{A_j + A_{j-1}}{2}$$

The integration formula used is the very simple tangent rule.

The 'quantisation' levels are given by A_j .

The abscissas are given by Y_j

The area of panel j is a_j .

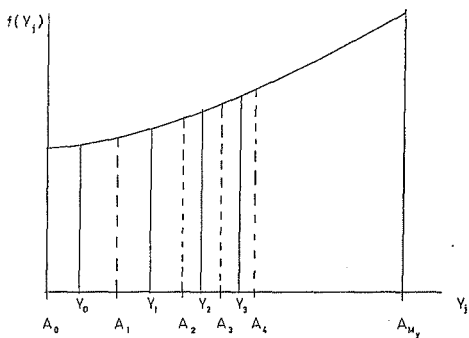


Fig. A1.3 The 'Quantisation' Levels in the Sinusoidal Channel

$$a_j = (A_{j+1} - A_j) f(Y_j) \quad \text{A1.18}$$

$$\int_0^1 f(y) dy \doteq \sum_{j=0}^{M_y-1} a_j \quad \text{A1.19}$$

$$\sum_{j=0}^{M_y-1} a_j = \sum_{j=0}^{M_y-1} (A_{j+1} - A_j) f(Y_j) \quad \text{A1.20}$$

$$= \sum_{j=0}^{M_y-1} h_y v_j f(Y_j) \quad \text{A.21}$$

$$h_y = 1 \quad \text{A1.22}$$

$$u_j = (A_{j+1} - A_j) \approx \sin\left(\frac{(j+1)\pi}{M_y^2}\right) - \sin\left(\frac{j\pi}{M_y^2}\right) \quad \text{Al.23}$$

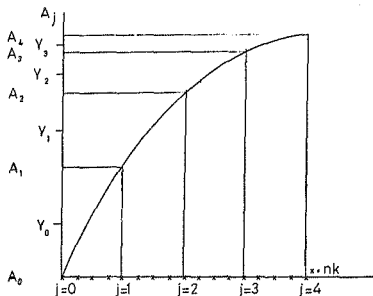


Fig.AL.4 Y_j and its corresponding arguments, nk .

$\left(\frac{N}{4}\right)$, the number of arguments in the range $0 - \frac{\pi}{2}$ is greater than M_y , the number of sinusoidal 'quantising' levels. To facilitate computing the following definition is made.

$$2^q M_y = \frac{N}{4} \quad q = 0, 1, 2, \dots \quad \text{Al.24}$$

If an argument, nk , is generated such that

$$(2^q)(j) \leq (nk) < (2^q)(j+1) \quad \text{Al.25}$$

the corresponding integration weight is u_j

This is illustrated in Fig.AL.4 for $N = 64$, $M_y = 4$ and $q = 2$.

Notes on Definition

1. The Nova 1200 machine code value of the argument

equivalent to $\frac{\pi}{2}$, necessitates the following modification to equation

A1.25 for the case $j \approx M_y - 1$

$$(2^q)(M_y - 1) \leq nk \leq (2^q)(M_y) \quad \text{A1.26}$$

2. In chapter (2.5) the argument defining $\sin \pi$ is defined as -0. As the sine wave enters the third quadrant (cosine wave enters second quadrant), the first 'quantised' level has a nominal value of -Y. Thus the arguments that define this level must have negative signs.

3. The 'quantised' abscissas Y_j are of no importance, but u_j , the associated integration weight (with w_i) forms the basis of the STV.

Table A1.2 The Sinusoidal Channel Integration Weights

j	u_j
0	0,0980171401
1	0,0970731818
2	0,0951943551
3	0,0923987554
4	0,0887133045
5	0,0841734959
6	0,078823051
7	0,0727134975
8	0,065903672
9	0,0584591587
10	0,0504516523
11	0,0419582682
12	0,033060803
13	0,0238449447
14	0,0143994464
15	0,0048152733

A2 Derivation of the Stored Table of Values

The STV is derived from the integration weights in Tables A1.1 and A1.2. The 2-D array has its elements calculated according to the following equation.

$$S(s, r) = \sum_{i=0}^s \sum_{j=0}^r w_i u_j$$

$$\text{where } s = 0, 1, \dots, M_x - 1 \quad (M_x = 19)$$

$$\text{and } r = 0, 1, \dots, M_y - 1 \quad (M_y = 16)$$

$$\text{eg. } S(2, 3) = \sum_{i=0}^2 \sum_{j=0}^3 w_i u_j = (w_0 + w_1 + w_2)(u_0 + u_1 + u_2 + u_3)$$

A2.1 The Machine Code for the Stored Table Values

From Tables A2.1 and A2.2, the max. value in the STV is

$$S(18, 15) = \sum_{i=0}^{18} \sum_{j=0}^{15} u_j w_i = 3,407545177$$

This value is defined to be equivalent to the machine code

$$40000_8 = 2^{14} = 16384_{10}$$

The remaining values in the STV are adjusted to this scale multiplying them by

$$(D_{x,y}) = \frac{16384}{3,407545177} = 4808,1533$$

The machine code values of the STV are given in A4.15

$$\text{From A1.1 } h_x = 0,3431458$$

$$\text{From A1.2 } h_y = 1,0.$$

$$\frac{h_x h_y}{D_x D_y} \div \frac{1}{(2048)(7)}$$

Table A2.1 Input Signal Channel Weights

$s = I$	$\sum_{i=0}^s w_i$
0	0,000000000
1	0,002762135866
2	0,006668385866
3	0,0121926576
4	0,0200051576
5	0,031053701
6	0,046678701
7	0,0687757879
8	0,100025788
9	0,1442199619
10	0,2067199619
11	0,2951083096
12	0,4201083096
13	0,596885005
14	0,846885005
15	1,200438396
16	1,700438396
17	2,407545177
18	3,407545177

Table A2.2 Sinusoidal Channel Weights

$r = K$	$\sum_{j=0}^r u_j$
0	0,0980171401
1	0,1950903219
2	0,290284677
3	0,3826834324
4	0,4713967369
5	0,5555702328
6	0,6343932838
7	0,7071067813
8	0,7730104533
9	0,8314696120
10	0,8819212643
11	0,9238795325
12	0,9569403355
13	0,9807852802
14	0,9951847266
15	1,0000000000

Table A2.3 Stored Table of Values (STV)

$$S(I_n, K_{nk})$$

$$S(\text{row}, \text{column})$$

$$D D_{x y} = 4808, 1533$$

I	k = 0	K = 1	K = 2	K = 3
0	0,0000	0,0000	0,0000	0,0000
1	1,3017259	2,5909162	3,8551549	5,0822651
2	3,1426918	6,2551196	9,3073079	12,269858
3	5,7461907	11,437045	17,017757	22,434572
4	9,4280754	18,765358	27,921923	36,809576
5	14,635026	29,129117	43,342683	57,13882
6	21,998795	43,785743	65,151015	85,888826
7	32,412744	64,513355	95,992674	126,54749
8	47,140283	93,826607	139,60933	184,04751
9	67,96818	135,28182	201,29265	265,36485
10	97,4233257	193,90833	288,52598	380,36488
11	139,079	276,81868	411,89248	542,99939
12	197,98916	394,07169	586,35914	772,99944
13	281,3007	559,89249	833,09227	1098,2685
14	399,12101	794,3985	1182,0255	1558,2687
15	565,74409	1126,0401	1675,4918	2208,8071
16	801,38471	1595,0521	2373,3584	3228,8073
17	1134,6308	2258,3353	3360,291	4429,8841
18	1605,9121	3196,3593	4756,0243	6269,8845

I	K = 0	K = 1	K = 2	K = 3
0	0,0000	0,0000	0,0000	0,0000
1	1,3017259	2,5909162	3,8551549	5,0822651
2	3,1426918	6,2551196	9,3073079	12,269858
3	5,7461907	11,437045	17,017757	22,434572
4	9,4280754	18,765358	27,921923	36,809576
5	14,635026	29,129117	43,342683	57,13882
6	21,998795	43,785743	65,151015	85,888826
7	32,412744	64,513355	95,992674	126,54749
8	47,140283	93,826607	139,60933	184,04751
9	67,96818	135,28182	201,29265	265,36485
10	97,4233257	193,90833	288,52598	380,36488
11	139,079	276,81868	411,89248	542,99939
12	197,98916	394,07169	586,35914	772,99944
13	281,3007	559,89249	833,09227	1098,2685
14	399,12101	794,3985	1182,0255	1558,2687
15	565,74409	1126,0401	1675,4918	2208,8071
16	801,38471	1595,0521	2373,3584	3128,8073
17	1134,6308	2258,3353	3360,291	4429,8841
18	1605,9121	3196,3593	4756,0243	6269,8845

I	K = 4	K = 5	K = 6	K = 7
0	0,000	0,0000	0,000	0,000
1	6,2604308	7,3783054	8,4251236	9,3908029
2	15,114245	17,813074	20,340355	22,671749
3	27,635333	32,569952	37,190907	41,45369
4	45,342736	53,439222	61,021065	68,015235
5	70,384586	82,952711	94,721865	105,57878
6	105,79949	124,69125	142,38218	158,70187
7	155,88361	183,71849	209,78408	233,82931
8	226,71322	267,19557	305,10471	340,07549
9	326,88148	385,25006	439,90852	490,33037
10	468,54069	552,20423	630,54978	702,82273
11	668,87697	788,31294	900,1571	1003,3321
12	952,19541	1122,2212	1281,4396	1428,3168
13	135,8682	1594,4389	1820,6545	2029,336
14	1919,505	2262,2556	2583,2196	2879,3055
15	2720,8506	3206,691	3661,6494	4081,3438
16	3854,1244	4542,3243	5186,7795	5781,2827
17	5456,8155	6431,195	7343,6393	8185,3594
18	7723,363	9102,4616	0393,899	11595,237

I	K = 8	K = 9	K = 10	K = 11
0	0,000	0,0000	0,000	0,000
1	10,266043	1,042415	11,538163	12,269674
2	24,784795	26,659151	28,276768	29,622061
3	45,317253	48,744382	51,702081	54,161853
4	74,354385	79,977454	84,830306	88,866183
5	115,41892	124,14751	131,6805	137,94532
6	173,49319	186,61366	197,93695	207,35398
7	255,62265	274,95418	291,63778	305,5127
8	371,77118	399,89647	424,15068	444,33002
9	536,0301	576,56751	611,55233	640,64747
10	768,32715	826,43209	876,57813	918,28211
11	1096,8446	1179,7937	1251,381	1310,9165
12	1561,4387	1679,5229	1781,4326	1866,1858
13	2218,474	2386,2467	2531,0387	2651,4552
14	3147,6622	3385,705	3591,1419	3761,9937
15	4461,7329	4799,1526	5090,3543	5332,5324
16	6320,1093	6798,0692	7210,5607	7553,6095
17	8948,2506	9824,9643	10208,985	10694,687
18	12665,003	13622,797	14449,398	15136,841

I	K = 12	K = 13	K = 14	K = 15
0	0,000	0,000	0,000	0,0000
1	12,708741	13,025417	13,216649	13,2806
2	30,682079	31,446613	31,908297	32,062689
3	56,100022	57,49792	58,342075	58,62437
4	92,046237	94,339841	93,74892	94,188068
5	142,88166	146,44198	148,59197	149,31095
6	214,77409	220,12582	223,3576	224,43834
7	316,4454	324,33057	329,09223	330,68458
8	460,23026	471,69826	478,6235	480,93938
9	663,57289	680,10777	690,09277	693,43185
10	951,14261	974,84314	989,1553	993,94145
11	1357,8274	1391,6616	1412,0933	1418,9259
12	1932,9668	1981,1324	2010,2184	2019,9451
13	2746,3368	2814,7699	2856,095	2869,9145
14	3896,6157	3993,7114	4052,3451	4071,9529
15	5523,3558	5660,9865	5744,0983	5771,8918
16	7823,9136	8018,8695	8136,5985	8175,9685
17	11077,393	11353,419	11520,104	11575,846
18	15678,509	16069,185	16305,105	16384,000

A.3 The Discrete Fourier Transform using the Table Look Up Algorithm

A3.1 Introduction

This appendix describes the modifications made to the 'Columns method' algorithm in 3.3.2 by exploiting the $\frac{\pi}{2}$ symmetry of the sinusoidal wave and shuffling the order of the I_n samples. A notation is introduced and a 128 point DFTTLU example is used to clarify the detailed explanation of the algorithm. The explanation is divided as follows:

- 1) The signed address generator.
- 2) The shuffling of the time samples, I_n
- 3) The table look up and accumulate routine
- 4) The calculation of the resultant harmonics

A3.2 Reducing the Number of Address Pairs from N^2 to $(\frac{N}{4})^2$

Fig.A3.1 shows the calculation steps normally needed to solve an 8 point DFTTLU. N constants from the STV have to be accumulated to calculate one harmonic and N^2 constants have to be accumulated to calculate N harmonics. The output of the SAG for $N=8$ is encoded as in Fig.A3.2 and $\frac{\pi}{2}$ is represented by $\frac{N}{4}$ ie.

2. The K_{nk} components of the address pairs are shown in Fig.A3.3. From this figure it can be seen that if the rows and columns of zeros are ignored, only the first $\frac{N}{4}$ rows or columns need be generated as the remaining addresses are similar

$$\begin{aligned}
F_0 &= S(I_0 K_{00}) \cdot S(I_1 K_{10}) \cdot S(I_2 K_{20}) \cdot S(I_3 K_{30}) \cdot S(I_4 K_{40}) \cdot S(I_5 K_{50}) \cdot S(I_6 K_{60}) \cdot S(I_7 K_{70}) \\
F_1 &= S(I_0 K_{01}) \cdot S(I_1 K_{11}) \cdot S(I_2 K_{21}) \cdot S(I_3 K_{31}) \cdot S(I_4 K_{41}) \cdot S(I_5 K_{51}) \cdot S(I_6 K_{61}) \cdot S(I_7 K_{71}) \\
F_2 &= S(I_0 K_{02}) \cdot S(I_1 K_{12}) \cdot S(I_2 K_{22}) \cdot S(I_3 K_{32}) \cdot S(I_4 K_{42}) \cdot S(I_5 K_{52}) \cdot S(I_6 K_{62}) \cdot S(I_7 K_{72}) \\
F_3 &= S(I_0 K_{03}) \cdot S(I_1 K_{13}) \cdot S(I_2 K_{23}) \cdot S(I_3 K_{33}) \cdot S(I_4 K_{43}) \cdot S(I_5 K_{53}) \cdot S(I_6 K_{63}) \cdot S(I_7 K_{73}) \\
F_4 &= S(I_0 K_{04}) \cdot S(I_1 K_{14}) \cdot S(I_2 K_{24}) \cdot S(I_3 K_{34}) \cdot S(I_4 K_{44}) \cdot S(I_5 K_{54}) \cdot S(I_6 K_{64}) \cdot S(I_7 K_{74}) \\
F_5 &= S(I_0 K_{05}) \cdot S(I_1 K_{15}) \cdot S(I_2 K_{25}) \cdot S(I_3 K_{35}) \cdot S(I_4 K_{45}) \cdot S(I_5 K_{55}) \cdot S(I_6 K_{65}) \cdot S(I_7 K_{75}) \\
F_6 &= S(I_0 K_{06}) \cdot S(I_1 K_{16}) \cdot S(I_2 K_{26}) \cdot S(I_3 K_{36}) \cdot S(I_4 K_{46}) \cdot S(I_5 K_{56}) \cdot S(I_6 K_{66}) \cdot S(I_7 K_{76}) \\
F_7 &= S(I_0 K_{07}) \cdot S(I_1 K_{17}) \cdot S(I_2 K_{27}) \cdot S(I_3 K_{37}) \cdot S(I_4 K_{47}) \cdot S(I_5 K_{57}) \cdot S(I_6 K_{67}) \cdot S(I_7 K_{77})
\end{aligned}$$

FigA3.1 Calculation Steps for 8 point DFTTLU

K_{nk} $k \neq l$	SAG output	Conventional Sine Argument
K_{0l}	0	0
K_{1l}	1	$\frac{\pi}{2}$
K_{2l}	2	$\frac{\pi}{2}$
K_{3l}	1	$\frac{3\pi}{4}$
K_{4l}	-0	π
K_{5l}	-1	$\frac{5\pi}{4}$
K_{6l}	-2	$\frac{3\pi}{2}$
K_{7l}	-1	$\frac{7\pi}{4}$

Fig.A 3.2 SAG Output $N=8$

$\begin{matrix} n \\ k \end{matrix}$	0	1	2	3	4	5	6	7
0	0	0	0	0	0	0	0	0
1	0	1	2	1	-0	-1	-2	-1
2	0	2	-0	-2	0	2	-0	-2
3	0	1	-2	1	-0	-1	2	-1
4	0	-0	0	-0	0	-0	0	-0
5	0	-1	2	-1	-0	1	-2	1
6	0	-2	-0	2	0	-2	-0	2
7	0	-1	-2	-1	-0	1	2	1

Fig.A 3.3 K_{nk} Components of Address Pairs $N=8$

Consider Fig.A3.3. The results of exploiting the symmetry are:

- 1) The addresses in columns $2n+1$, $n=0 \dots \frac{N}{2}-1$ have the same absolute values.
- 2) The addresses in columns $4n+2$, $n=0 \dots \frac{N}{4}-1$ have the same absolute values.
- 3) The addresses in columns $4n$, $n=0 \dots \frac{N}{4}-1$ have the same absolute values.
- 4) The above 3 points also apply to the corresponding rows of addresses.
- 5) Only the first $\frac{N}{4}$ rows in the first $\frac{N}{4}$ columns need be generated if the rows and columns of zeros are ignored.

If some of the rows in some of the columns are considered it is possible to extract columns of K_{nk} values that are:

- 1) Identical in magnitude and sign
- 2) Identical in magnitude but opposite in sign.

These columns are termed similar. If the odd numbered rows in the odd numbered columns are considered, the resulting columns are similar. The same applies to rows $4k+2$, $k=0 \dots \frac{N}{4}-1$ in columns $2n+1$, $n=0 \dots \frac{N}{2}-1$ and rows $4k$, $k=0 \dots \frac{N}{4}-1$ in columns $2n+1$, $n=0 \dots \frac{N}{2}-1$. This can be extended to columns $4n+2$ and $4n$, $n=0 \dots \frac{N}{4}-1$. Thus there are nine sets of similar columns. Each column in each set of columns is associated with more than one time sample. Thus one column of K_{nk} addresses can be used to derive several columns of address pairs $I_n K_{nk}$. For example

consider the odd numbered rows in column 1. Samples I_1 , I_3 , I_5 , I_7 share the same column of K_{nk} but K_{nk} has opposite signs for I_5 and I_7 . These time samples are also termed similar. This can be extended to the remaining eight sets of similar columns.

The similar time samples follow a pattern similar to the reverse bit notation used in the FFT⁵. The time samples are shuffled in much the same way that they are shuffled in the F.F.T algorithm. This is not apparent in this simple 8 point example and, in A3.5, a 128 point DFTTLU example shows the similar columns and the shuffled time samples. To simplify explanation, a notation for the nine sets of similar columns is introduced in A3.4.

A3.3 Shuffling the Order of the Time Samples I_n

The time samples are stored in the I_n array in the order in which they are sampled. In A3.5 it is shown that one of the first $\frac{N}{4}$ or $\frac{N}{8}$ columns of K_{nk} addresses can be paired with 4 or 8 I_n values respectively to form 4 or 8 columns of address pairs. The 4 or 8 I_n values do not occur in the sampled order and follow a bit reversed order. The notation in A3.5 and the example in A3.5 facilitate the explanation of the Shuffling Routine in A3.9.

A3.4 Notation

The following points are repeated for clarity:

- 1) Given an N point DFT/DFTLU the time samples, I_n , are numbered from $n=0 \dots N-1$.
- 2) The harmonics, F_k , are numbered from $k=0 \dots N-1$.
- 3) N (in this case) is a positive integer power of 2.
- 4) The columns of address pairs (or K_{nk} values) are numbered according to the number of their associated time sample (I_n , $n=0 \dots N-1$).
- 5) The rows of address pairs are numbered according to the frequency index k , $k=0 \dots N-1$.

Odd numbered time samples and their corresponding columns are termed OTS.

The even numbered columns that are NOT multiples of 4 are termed E4TS.

The remaining even numbered columns are termed E4TS.

The rows are numbered in a similar way.

The odd numbered rows contribute to the odd numbered harmonics.

The rows are termed OH.

Similarly, the even-numbered rows that are NOT multiples of 4 are termed E4H.

The remaining rows are termed E4H.

The terminology is used to define the 9 sets of columns of arguments in the following way:

eg. The set of the odd numbered rows in the odd numbered columns of addresses is called OTS/OH.

Similarly, the even numbered rows that are NOT multiples of 4 in the even numbered columns that are multiples of 4 are termed E4TS/E4H.

Thus the 9 sets of columns of addresses are listed as follows:

- 1) OTS/OH
- 2) OTS/E4H
- 3) OTS/E4H
- 4) E4 TS/OH
- 5) E4TS/E4H
- 6) E4TS/E4H
- 7) E4TS/OH
- 8) E4TS/E4H
- 9) E4TS/E4H.

A3.5 A 128 point DFTTLU example

A3.5.1 The Signed Address Generator SAG output

The 8 point DFTTLU example is not very useful as there are only 2 points in the range $0 - \frac{\pi}{2}$ rad. A 128 point DFTTLU has points

0, 1, 2, 29, 30, 31, 32 in the range $0 - \frac{\pi}{2}$

This notation is used in Fig.A3.4.1 and Fig.A3.4.2 which list the columns of K_{nk} values for the imaginary and real harmonics respectively (cf. Fig.A3.3).

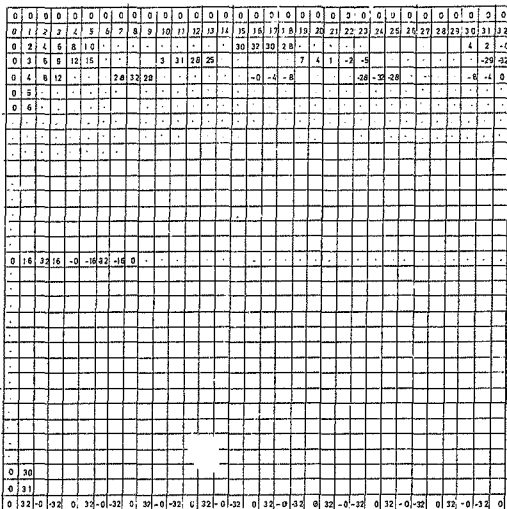


Fig A 34.1 SIGNED ARGUMENTS /ADDRESSES (sine) N=128

A3.5.2 Shuffling the Time Samples

Fig.A3.5 lists the columns of K_{nk} components of the address pairs that are equal or opposite signed eg. if the set OTS/OH(sine) is considered, columns 1, 63, 65, 127 have K_{nk} values of equal magnitudes but columns 65, 127 have opposite signs to columns 1, 63. Clearly time samples $I_1, I_{63}, I_{65}, I_{127}$ are similar (cf. A3.2). If the set OTS/E4H(sine) is considered columns 9, 23, 41, 55, 73, 87, 105, 119 have K_{nk} values of equal magnitude but the signs of columns 41, 55, 105, 119 are opposite to columns 9, 23, 73, 87. Time samples $I_9, I_{23}, I_{41}, I_{55}, I_{73}, I_{87}, I_{105}, I_{119}$ are similar.

In this case 8 columns of K_{nk} values are similar if even numbered harmonics, which are not multiples of 4 are considered. The remaining 7 sets are interpreted in a similar manner.

The columns of signs in Fig.A3.5 show which columns of K_{nk} values are opposite signed. Consider the listing needed OTS/OH and consider the first column of numbers:

	sine	cosine
1	+	+
63	+	-
65	-	-
127	-	+

This states that the columns of K_{nk} values, 1, 63, 65, 127 have the same magnitude but that columns 65 and 127 are opposite signed to 1 63 when the sine (imaginary) harmonics are considered. This listing also shows that time samples 1, 63, 65 and 127 are

similar. The remaining 8 sets of listings are interpreted in the same way.

A3.5.3 Formulae to Shuffle the Time Samples

The nine sets of shuffled I_n in Fig.A3.5 are generated with the following formulae. Consider the formula for the OTS/OH set:

$$\begin{aligned} \text{ie.} \quad & 1 + 2n \\ & \left(\frac{N}{2} - 1\right) - 2n \quad n = 0 \dots \frac{N}{8} - 1 \\ & \left(\frac{N}{2} + 1\right) + 2n \\ & (N - 1) - 2n \end{aligned}$$

Here $N = 128$ and consider the case for $n = 0$.

$$\begin{aligned} \text{ie.} \quad & 1 \\ & 63 \\ & 65 \\ & 127 \end{aligned}$$

columns of K_{nk} values numbered 1, 63, 65 and 127 have the same magnitudes and time samples $I_1, I_{63}, I_{65}, I_{127}$ shuffled out of the I_n array.

ODD TIME SAMPLES

Odd harmonics	1	3	5	7	9	11	13	15	17	19	21	23	25	27	29	31	+	+
	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	+	+
	65	67	69	71	73	75	77	79	81	83	85	87	89	91	93	95	-	-
	127	125	123	121	119	117	115	113	111	109	107	105	103	101	99	97	-	+
E_4 harmonics	1	3	5	7	9	11	13	15									+	+
	31	29	27	25	23	21	19	17									+	+
	33	35	37	39	41	43	45	47									-	-
	63	61	59	57	55	53	51	49									-	+
	65	67	69	71	73	75	77	79									+	+
	95	93	91	89	87	85	83	81									+	-
	97	99	101	103	105	107	109	111									-	-
	127	125	123	121	119	117	115	113									-	+
E_4 harmonics	1	3	5	7	9	11	13	15	17	19	21	23	25	27	29	31	+	+
	33	35	37	39	41	43	45	47	49	51	53	55	57	59	61	63	+	+
	65	67	69	71	73	75	77	79	81	83	85	87	89	91	93	95	+	+
	97	99	101	103	105	107	109	111	113	115	117	119	121	123	125	127	+	+

Fig.A3.5.1 Groups of Shuffled Time Samples including sign patterns for N = 128

E4 TIME SAMPLES

[illegible]

Fig.A3.5. Groups of Shuffled Time Samples including sign patterns for $N = 128$

E4 TIME SAMPLES

	0	4	8	12	16	20	24	28	(32)	sin	cos
Cid										+	+
harmonic	(64)	60	56	52	48	44	40	36	32	+	-
	64	68	72	76	80	84	88	92	(96)	-	-
	(128)	124	120	116	112	108	104	100	96	-	+
E4											
harmonic	0	4	8	12	16	20	24	28		+	+
	32	36	40	44	48	52	56	60		-	-
	64	68	72	76	80	84	88	92		+	+
	96	100	104	108	112	116	120	124		-	-
E4											
harmonic	0	4	8	12	16	20	24	28		+	+
	32	36	40	44	48	52	56	60		+	+
	64	68	72	76	80	84	88	92		+	+
	96	100	104	108	112	116	120	124		+	+

Fig.A3.5.3 Groups of Shuffled Time Samples including sign patterns for N = 128

Table A 3.1 Formulae to Shuffle Time Samples

OTS/OH $n=0,1,\dots,(N/8)-1$	$\overline{E4TS}/OH$ $n=0,1,\dots,(N/16)-1$	$E4TS/OH$ $n=0,1,\dots,(N/16)-1$
$1+2n$	$2+4n$	$0+4n$
$(\frac{N}{2}-1)-2n$	$(\frac{N}{2}-2)-4n$	$\frac{N}{2}-4n$
$(\frac{N}{2}+1)+2n$	$(\frac{N}{2}+2)+4n$	$\frac{N}{2}+4n$
$(N-1)-2n$	$(N-2)-4n$	$N-4n$
OTS/ $\overline{E4H}$ $n=0,1,\dots,(N/16)-1$	$\overline{E4TS}/\overline{E4H}$ $n=0,1,\dots,(N/32)-1$	$\overline{E4TS}/\overline{E4H}$ $n=0,1,\dots,(N/16)-1$
$1+2n$	$2+4n$	$0+4n$
$(\frac{N}{4}-1)-2n$	$(\frac{N}{4}-2)-4n$	$\frac{N}{4}+4n$
$(\frac{N}{4}+1)+2n$	$(\frac{N}{4}+2)+4n$	$\frac{N}{2}+4n$
$(\frac{N}{2}-1)-2n$	$(\frac{N}{2}-2)-4n$	$\frac{3N}{4}+4n$
$(\frac{N}{2}+1)+2n$	$(\frac{N}{2}+2)+4n$	
$(\frac{3N}{4}-1)-2n$	$(\frac{3N}{4}-2)-4n$	
$(\frac{3N}{4}+1)+2n$	$(\frac{3N}{4}+2)+4n$	
$(N-1)-2n$	$(N-2)-4n$	
OTS/ $\overline{E4H}$ $n=0,1,\dots,(N/8)-1$	$\overline{E4TS}/\overline{E4H}$ $n=0,1,\dots,(N/16)-1$	$E4TS/\overline{E4H}$ $n=0,1,\dots,(N/16)-1$
$1+2n$	$2+4n$	$0+4n$
$(\frac{N}{4}+1)+2n$	$(\frac{N}{4}+2)+4n$	$\frac{N}{4}+4n$
$(\frac{N}{2}+1)+2n$	$(\frac{N}{2}+2)+4n$	$\frac{N}{2}+4n$
$(\frac{3N}{4}+1)+2n$	$(\frac{3N}{4}+2)+4n$	$\frac{3N}{4}+4n$

A3.6 Algorithm to Generate the Signed Addresses (K_{nk})

A3.6.1 The Four State UP/DOWN Counter

The generator, a software program, must simulate a 4 state UP/DOWN counter. Consider the K_{nk} values needed for the imaginary harmonic components. The states are listed in Table A3.2

Table A3.2 The 4 states of the K_{nk} generator.

State	Radian Argument		Signed Radian Argument		Output of Signed Address Generator
1	$0 - \frac{\pi}{2}$	+	$0 - \frac{\pi}{2}$	+	$0 - \frac{N}{4}$
2	$\frac{\pi}{2} - \pi$	+	$\frac{\pi}{2} - 0$	+	$\frac{N}{4} - 0$
3	$\pi - \frac{3\pi}{2}$	-	$0 - \frac{\pi}{2}$	-	$0 - \frac{N}{4}$
4	$\frac{3\pi}{2} - 2\pi$	-	$\frac{\pi}{2} - 0$	-	$\frac{N}{4} - 0$

To facilitate explanation, the radian equivalents of the K_{nk} values are used and clearly $\frac{\pi}{2} \equiv \frac{N}{4}$. In A3.7 the machine code values of K_{nk} are discussed.

A3.6.2 The Starting and Incrementing Arguments

The algorithm requires two input values.

- 1) The starting argument
- 2) The incrementing argument.

The starting argument is the first value in a column of K_{nk} values. The incrementing argument is added to the starting argument and the resulting subtotal is the next K_{nk} value in the column. The incrementing argument is repeatedly added to the subtotal to give the remaining K_{nk} values. The problem of having a subtotal greater than $\frac{\pi}{2}$ is discussed in the next section. Assuming the problem of changing from state 1 to state 2 is overcome, the K_{nk} values in state 2 are obtained by repeatedly subtracting the incrementing argument from the subtotal. The problem of having a subtotal less than 0 is also discussed in the next section.

A3.6.3 Subtotal greater than $\frac{\pi}{2}$ (overflow) less than 0, (underflow)
and incrementing arguments greater than $\frac{\pi}{2}$

It must be noted that the sign component of the argument is only added to the argument at a later stage. The values here are in the 'unsigned' form.

The maximum value that the register can hold is $\frac{\pi}{2}$. Values greater than $\frac{\pi}{2}$ will appear in the 'overflowed' form while value less than 0 will appear in 'the underflowed' form.

Once overflow or underflow takes place the resulting subtotal must be modified in order to be compatible with the next state. If $\frac{\pi}{2}$ is chosen in the above manner, the modification is simply implemented by taking the $\frac{\pi}{2}$'s complement' of the overflow or underflow value.

Consider overflow from state 1 to state 2.

$$\text{eg. } \frac{\pi}{3} + \frac{\pi}{3} = \frac{\pi}{6} \text{ overflow (correct answer is } \frac{2\pi}{3})$$

The $\frac{\pi}{2}$'s complement of $\frac{\pi}{6}$ is $\frac{\pi}{3}$ and.

$$\sin\left(\frac{\pi}{3}\right) \equiv \sin\left(\frac{2\pi}{3}\right)$$

Consider underflow from state 2 to state 3

$$\text{eg } \frac{\pi}{6} - \frac{\pi}{3} = \frac{\pi}{3} \text{ overflow}$$

The $\frac{\pi}{2}$'s complement of $\frac{\pi}{6}$ is $\frac{\pi}{6}$. In this case state 3 is negative and the output would be $-\frac{\pi}{6}$. By definition

$$\sin\left(-\frac{\pi}{6}\right) \equiv -\sin\left(\frac{\pi}{6}\right)$$

In Fig.A3.6 the output of an SAG is given where the starting argument is zero and the incrementing argument is $\frac{\pi}{3}$.

Conventional Argument	0	$\frac{\pi}{3}$	$\frac{2\pi}{3}$	π	$\frac{4\pi}{3}$	$\frac{5\pi}{3}$	2π	State
Signed Argument	0	$\frac{\pi}{3}$	OVF	—	—	—	—	1
	—	$\frac{\pi}{3}$	UNF	—	—	—	—	2
	—	—	$-0 - \frac{\pi}{3}$	OVF	—	—	—	3
	—	—	—	$-\frac{\pi}{3}$	UNF	—	—	4
	—	—	—	—	—	0	—	1

Fig.A3.6 SAG Output

Adding $\frac{\pi}{2}$ is implemented by taking the $\frac{\pi}{2}$'s complement of the subtotal and moving to the next state. Adding π is implemented by moving to the next state but one.

Adding $\frac{3\pi}{2}$ is implemented by taking the $\frac{\pi}{2}$'s complement of the subtotal and moving to the next state but two.

Increments greater than $\frac{\pi}{2}$ are written in the overflowed form.

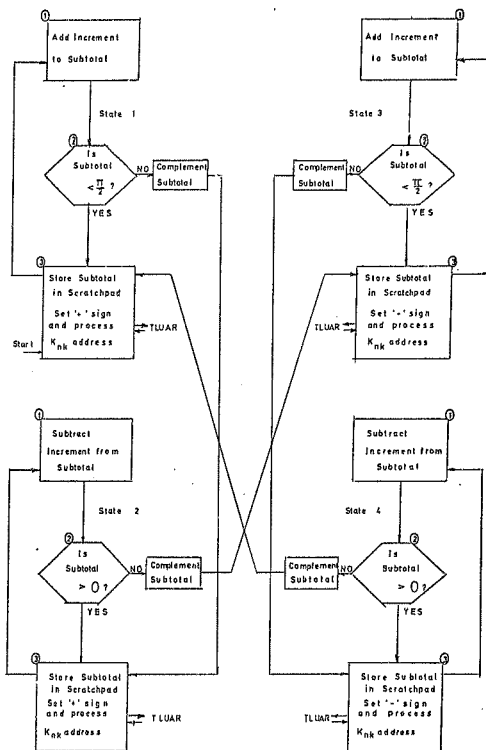
eg. an increment of $\frac{3}{4}\pi$ is written as $\frac{\pi}{4}$ and is added by taking the $\frac{\pi}{2}$'s complement of the subtotal and adding $\frac{\pi}{4}$ to the result.

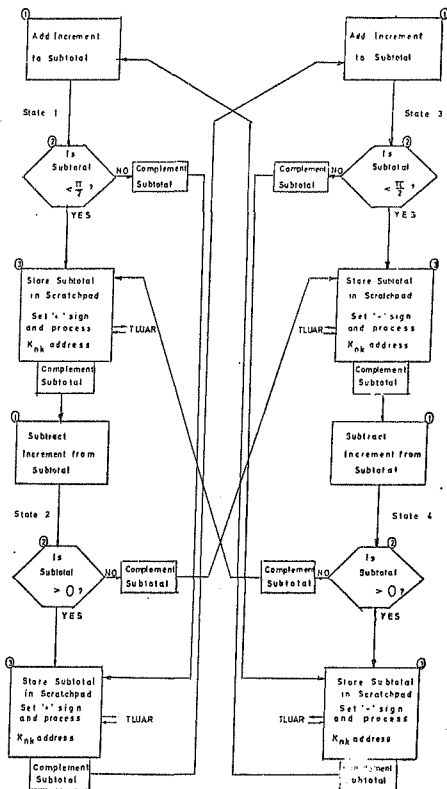
A3.6.4 Flowchart of Algorithm to Generate K_{nk} values

There are four similar algorithms for the four cases of incrementing arguments.

- | | | |
|---------|--------------------------------------|------------|
| Case 1. | $0 < \text{Inc} < \frac{\pi}{2}$ | Fig.A3.7 |
| Case 2. | $\frac{\pi}{2} < \text{Inc} < \pi$ | Fig.A3.8 |
| Case 3. | $\pi < \text{Inc} < \frac{3}{2}\pi$ | Fig.A3.9 |
| Case 4. | $\frac{3}{2}\pi < \text{Inc} < 2\pi$ | Fig.A3.10. |

Step 3 processes the argument to conform to the sinusoidal 'quantising levels' defined in A1.2.3. The subtotal must not be destroyed in the processing and it is stored in a 'scratch pad' memory location. The sign bit is added in the last step of the processing and is placed in the most significant bit (MSB) position. The cosine value is derived in step 3 by taking the $\frac{\pi}{2}$'s complement of the sine argument and setting the signbit (MSB) to the sign of the following state. The algorithm is entered at step 3 and the start argument is stored in the scratch pad. The Assembler program is in A4.5.

Fig.A3.7 Case1 $0 < \text{inc.} < \frac{\pi}{2}$

Fig. A 3.8 Case 2 $\frac{\pi}{2} < inc. < \pi$

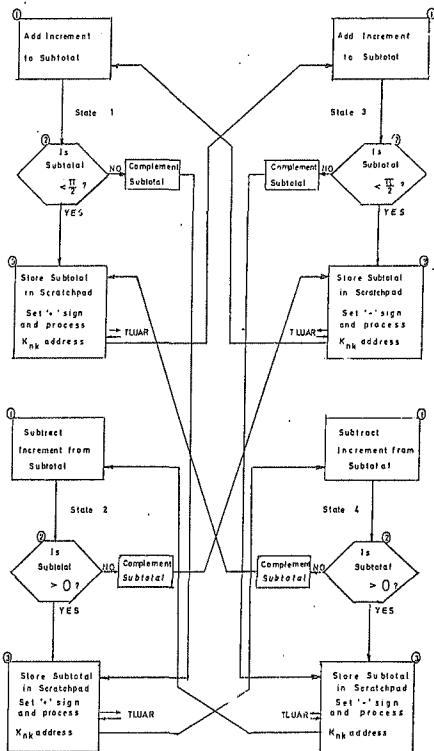


Fig. A3.9 Case 3 $\pi < \text{inc.} < \frac{3\pi}{2}$

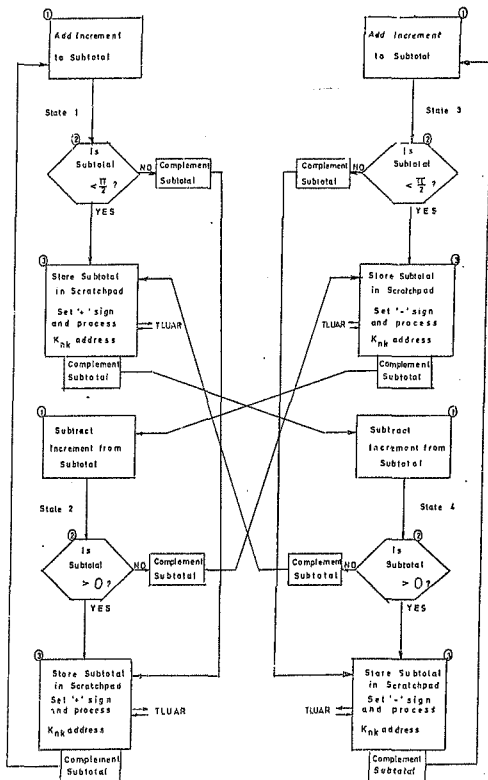


Fig. A 3.10 Case 4 $\frac{3\pi}{2} < \text{inc.} < 2\pi$

A3.7 Expressing the Radian Arguments in Nova 1200 Machine Code

A knowledge of Nova 1200 machine code¹ is assumed and the Assembler program that implements the algorithm in A3.6 is described in A4.5. This section shows how the radian arguments are expressed in terms of machine code and how overflow (subtotals $> \frac{\pi}{2}$) or underflow can be detected using the CARRY bit of the machine. The resulting machine code values of K_{nk} are then modified to facilitate the addressing of the Stored Table of Values (STV).

A3.7.1 Machine Code

The Nova 1200 has a 16 bit word and a CARRY bit which changes state when overflow or underflow occurs. The radian angles are defined in terms of the machine code as follows:

$$0 \text{ rad} \equiv 0_8$$

$$\frac{\pi}{2} \text{ rad} \equiv 0_8 \text{ overflow CARRY bit changes state}$$

Thus taking the two's (2's) complement of a machine code number is equivalent to taking the $\frac{\pi}{2}$'s complement (A3.6.3). Confusion arises because 0 and $\frac{\pi}{2}$ have the same machine code value (ignoring the change of state of the carry bit). However, Fig.A3.4 (for $N = 128$) shows that this only occurs in 3 of the 9 sets of similar columns - in those sets that extract the even multiples of 4 harmonics. In these 3 sets both 0 and $\frac{\pi}{2}$ can occur in the same column. This is overcome by the definition of Y_{M-1} and the corresponding integration weight u_{M-1} in A1.2 which includes $\frac{\pi}{2}$ in the final quantising level. This is not correct mathematically as $\frac{\pi}{2}$ is the threshold of the

next quantising level Y_M . The algorithm in A3.6 does not take this into account and the simple modification is given later in this section.

Consider an N point DFTLU

$0 - 2\pi$ is divided into N steps

$0 - \frac{\pi}{2}$ is divided into $\frac{N}{4}$ steps

The 16 bit computer word must have $\frac{N}{4}$ steps. If $N = 128$ the machine code steps are:

$0_8, 4\ 000_8, 10\ 000_8, \dots, 174\ 000_8$

The final column in the set OTS/OH is:

$4\ 000_8, 14\ 000_8, 24\ 000_8, 34\ 000_8, \dots$

Clearly the starting value is $4\ 000_8$ and the incrementing value is $10\ 000_8$.

The layout of the STV is given in A3.10.2 and the K_{nk} values must be processed and signed to address the STV. This requires the K_{nk} values to be in integral multiples of 40_8 . There are 16 "sinusoidal quantising abscissas", and the K_{nk} output of the SAG must be in the form

$\pm 0_8, \pm 40_8, \pm 100_8, \dots, \pm 700_8, \pm 740_8$

This is done by truncating all but the 4 most significant bits (MSB) of the machine code and shifting the remaining 4 bits 7 places to the right.

eg. $14\ 000_8 = 0\ 001\ 100\ 000\ 000\ 000_2$

Truncating $0\ 001\ \underline{\hspace{2cm}}$

Shift right 7 X $0\ 000\ 000\ 000\ 100\ 000_2$

$= 40_8$

The machine code equivalent to $\frac{\pi}{2}$ is 0_8 overflow. This value must be converted into 740_8 in terms of the definition in A1.2.4. The algorithm takes the one's complement of 0_8 and then truncates and shifts it as before.

eg one's complement of 0_8	$= 1\ 111\ 111\ 111\ 111\ 111_2$
Truncating	$1\ 111\ \text{-----}$
Shift right 7X	$0\ 000\ 000\ 111\ 100\ 000_2$
	$= 740_8$

The cosine argument is obtained from the sine argument by taking the two's complement.

eg sine argument $4\ 000_8$	$= 0\ 000\ 100\ 000\ 000\ 000_2$
two's complement	$1\ 111\ 100\ 000\ 000\ 000_2$
	$= 174\ 000_8$

The result must still be truncated and shifted.

A3.8 Derivation of Starting and Incrementing Arguments of K_{nk} for SAG

Each column in each of the 9 sets of columns need 2 inputs:

- 1) The starting argument SH
- 2) The incrementing argument SI.

A3.8.1 The Starting Argument

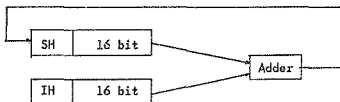
The DFTTLU for $N = 128$ is used as an example and consider the set of columns of arguments OTS/OH.

The starting arguments of each column in this set are listed in machine code.

4 000 ₈	14 000 ₈	24 000 ₈	34 000 ₈
44 000 ₈	54 000 ₈	64 000 ₈	74 000 ₈
104 000 ₈	114 000 ₈	124 000 ₈	134 000 ₈
144 000 ₈	154 000 ₈	164 000 ₈	174 000 ₈

The difference between each starting argument is 10 000₈. This difference is termed IH.

The values are derived in the following way



The value SH (in this case 4 000₈) is loaded into address SH.

The value IH (in this case 10 000₈) is loaded into address IH.

IH is added to SH and the result is placed in SH to form the next value of SH.

This is repeated until all the start addresses in the set OTS/OH have been generated.

There are 9 sets of columns and SH and IH are listed below for $N = 128$.

Table A3.3

OTS/OH	SH1	4 000 ₈	IH1	10 000 ₈
OTS/E4H	SH2	10 000 ₈	IH2	20 000 ₈
OTS/E4H	SH3	0 ₈	IH3	0 ₈
E4TS/OH	SH4	10 000 ₈	IH4	20 000 ₈
E4TS/E4H	SH5	20 000 ₈	IH5	40 000 ₈
E4TS/E4H	SH6	0 ₈	IH6	0 ₈
E4TS/OH	SH7	0 ₈	IH7	20 000 ₈
E4TS/E4H	SH8	0 ₈	IH8	40 000 ₈
E4TS/E4H	SH9	0 ₈	IH9	0 ₈

A3.8.2 The Incrementing Argument

Once again the DFTTLU for $N = 128$ used as an example.

Consider the set of columns of arguments OTS/OH. The incrementing arguments, SI, of each column in the set are listed in machine code.

10 000	30 000 ₈	50 000 ₈	70 000 ₈
110 000 ₈	130 000 ₈	150 000 ₈	170 000 ₈
*10 000 ₈	30 000 ₈	50 000 ₈	70 000 ₈
110 000 ₈	130 000 ₈	150 000 ₈	170 000 ₈

*The arguments exceed $\frac{\pi}{2}$ and the 'overflow' form is used.

The difference between these values is $20\,000_8$. This difference is termed II.

The derivation of these values is similar to the derivation for SH, in this case II is added to SI to generate the next value.

Table A3.4

The values of SI and II are listed below for $N = 128$

OTS/OH	SI1	$10\,000_8$	II1	$20\,000_8$
OTS/E4H	SI2	$20\,000_8$	II2	$40\,000_8$
OTS/E4H	SI3	$20\,000_8$	II3	$40\,000_8$
E4TS/OH	SI4	$40\,000_8$	II4	$40\,000_8$
E4TS/E4H	SI5	$40\,000_8$	II5	$100\,000_8$
E4TS/E4H	SI6	$40\,000_8$	II6	$100\,000_8$
E4TS/OH	SI7	0_8	II7	$40\,000_8$
E4TS/E4H	SI8	0_8	II8	$100\,000_8$
E4TS/E4H	SI9	0_8	II9	$100\,000_8$

The basic step value for $N = 128$ is $4\,000_8$.

All the above values are derived from $4\,000_8$ by shifting it the required number of places to the left.

ie. $4\,000_8 \rightarrow 10\,000_8 \rightarrow 20\,000_8 \rightarrow 40\,000_8 \rightarrow 100\,000_8$

All these starting and incrementing arguments are calculated in subprogram CCL which is covered in A4.8.

A3.8.3 The Starting and Incrementing Arguments and the SAG

Consider the case where the set of columns OTS/OH is being generated.

1) $SH1$, $IH1$, $S11$, $II1$ are calculated by the CCL subprogram and passed to the start/inc. argument generator.

2) The starting and incrementing arguments are generated and passed to the SAG.

3) The SAG generates a column of K_{nk} values which are processed with the shuffled I_n values to form 4 columns of address pairs.

4) After the column of K_{nk} values have been processed. The start/inc. argument generator generates the starting and incrementing argument of the next column (column 3) and the above steps are repeated.

A3.9 Shuffling Routine

A3.9.1 Introduction

The shuffling routine must sort out the 4 or 8 time samples associated with each column in each of the 9 sets of similar columns by implementing the formulae given in A3.5.3. If the DFTTLU for $N = 128$ is considered and the first column in the set OTS/OH is being generated the time samples associated with that column are I_1 , I_{63} , I_{65} and I_{127} . The next column in that set (column 3) is associated with time samples I_3 , I_{61} , I_{67} , I_{125} .

A3.9.2 The Algorithm

The time samples are stored in the I_n array as they are sampled. Their addresses in the array (designated MB) correspond to their position in time (ie. I_n is stored in address n in MB). The algorithm must address and extract the required 4 or 8 similar time samples and place these in 4 or 8 consecutive locations in a data block termed SB. At a later stage these values can be easily accessed by the Table Look Up and Accumulate Routine (TLUAR) (A3.10).

The algorithm need only generate the formulae in A3.5.3 and this is implemented as follows:

The Shuffling Routine must be given the first set of shuffled I_n values in each of the 9 sets of columns. (These shuffled I_n values are calculated by the CCL subprogram.)

Fig. 3.11

The First Group of Shuffled Time Samples

(cf A3.5.3)

Set	n
OTS/OH	$1, \frac{N}{2} - 1, \frac{N}{2} + 1, N - 1$
OTS/E $\bar{4}$ H	$1, \frac{N}{4} - 1, \frac{N}{4} + 1, \frac{N}{2} - 1, \frac{N}{2} + 1, \frac{3N}{4} - 1, \frac{3N}{4} + 1, N - 1$
OTS/E4H	$1, \frac{N}{4} + 1, \frac{N}{2} + 1, \frac{3N}{4} + 1$
E $\bar{4}$ TS/OH	$2, \frac{N}{2} - 1, \frac{N}{2} + 1, N - 2$
E $\bar{4}$ TS/E $\bar{4}$ H	$2, \frac{N}{4} - 2, \frac{N}{4} + 2, \frac{N}{2} - 2, \frac{N}{2} + 2, \frac{3N}{4} - 2, \frac{3N}{4} + 2, N - 2$
E $\bar{4}$ TS/E4H	$2, \frac{N}{4} + 2, \frac{N}{2} + 2, \frac{3N}{4} + 2$
E4TS/OH	$0, \frac{N}{2}, \frac{N}{2}, N$
E4TS/E $\bar{4}$ H	$0, \frac{N}{4}, \frac{N}{2}, \frac{3N}{4}$
E4TS/E4H	$0, \frac{N}{4}, \frac{N}{2}, \frac{3N}{4}$

For example, if the numbers are required for the *second* column in the set OTS/OH.

2 would be added to the first element in the column

ie. $1 + 2$

2 would be subtracted from the second element in the column.

ie. $(\frac{N}{2} - 1) - 2$

2 would be added to the third element in the column.

ie. $(\frac{N}{2} + 1) + 2$

2 would be subtracted from the fourth element in the column.

in $(N - 1) - 2$

The Assembler program is given in A4.4

A3.10 Table Look Up and Accumulate Routine TLUAR

A3.10.1 Introduction

This routine performs 2 steps.

- 1) Derives the STV address from the time sample, I_n , and the signed address, K_{nk} .
- 2) Obtains the contents of that address and adds/ subtracts its to/from its corresponding Accumulator, depending on the signum function.

It must be noted each of the two outputs of the SAG (the sine and cosine arguments) is associated with 4 or 8 shuffled time samples and 8 or 16 address pairs are passed to the TLUAR. The TLUAR stores the cosine K_{nk} address and first processes the sine address pairs. It then retrieves the cosine address and processes it. The format of the STV can be manipulated to simplify the addressing of the STV and the derivation of the signum function. This allows the signum function to be manipulated to take account of the similar columns of K_{nk} addresses. (ie. columns with the same magnitudes but opposite signs.)

A3.10.2 The Format of the STV

The STV is a two dimensional (2 - D) array $S(I_n K_{nk})$ where I_n and K_{nk} are the two addresses needed to specify any location in the array. The LADC output, I_n , has 19 levels and a sign bit. (ie. 19 positive levels symmetric with 19 negative levels). The SAG output is quantised into 16 levels and a sign bit (ie. 16 positive levels symmetric with 16 negative levels.)

The sign bits contribute to the signum function and the level addresses are associated with the 19×16 2 - D array in Fig.A3.12.

$\begin{smallmatrix} I \\ \backslash \\ K \end{smallmatrix}$	0	1	2	3		15
0						
1						
2						
...						
...						
...						
18						

Fig.A3.12 The Two Dimensional Array

In the computer core, 2 - D arrays are transposed into 1 - D arrays (ie. data blocks). The columns of the 2 - D array are placed successively in the core as in Fig.A3.13.

I	K	Contents
0	0	
1	0	
2	0	
.	.	
.	.	
18	0	
0	1	
1	1	
2	1	
.	.	
.	.	
18	1	
-	-	
-	-	
-	-	
0	15	
1	15	
2	15	
.	.	
.	.	
18	15	

Fig.A3.13 2 - D array transposed into 1 - D array.

If the contents of location (3,2) are required from the 1 - D array (ie. $I_n = 3$, $K_{nk} = 2$), the location is $3 + (2 \times 19) = 41_{10}$ locations from the first location. The machine code for 19 is

OCTAL COMPUTER ADDRESS	I OCTAL	K OCTAL	STV CONTENTS
0	0	0	
1	1	0	
:	:	:	
22	22	0	
:	:	:	
37	37	0	Waste
40	0	1	
41	0	1	
:	:	:	
62	22	1	
:	:	:	
77	37	1	Waste
100	0	2	
101	1	2	
:	:	:	
:	:	:	
:	:	:	
:	:	:	
737	37	16	
740	0	17	
741	1	17	
:	:	:	
762	22	17	
:	:	:	
777	37	17	Waste

Fig.A 3.14 1-D Array. 40₆ Format

10011_2 which is not an easy number for the computer to manipulate. The next largest and easily manipulated number is 32_{10} ie. $100\ 000_2$ and this is chosen as the basis of the 1 - D array. The K_{nk} addresses are thus expressed as integral multiples of 32_{10} ie. 40_8 . This results in a waste of core between locations 20_{10} and 32_{10} which are empty. The core is formatted as in Fig.A3.14.

Another method to overcome the problem of the 19 locations in a column of the array is to modify the I_n value instead of the K_{nk} value. The I_n values would be $\pm 0, \pm 16_{10}, \pm 32_{10}, \dots, \pm 288_{10}$. The K_{nk} values would still have to be manipulated to have values between 0_{10} and 15_{10} . Thus both I_n and K_{nk} would have to be manipulated and it was decided rather to waste the core space and manipulate one of the address pair components.

The two address pair components are added using the normal two's complement arithmetic. The magnitude of the result gives the STV location and the sign bit of the result gives the result of the signum function. If the STV is loaded from location X, X is also added to the address pair total to give the STV address.

A3.10.3 Incorporating the Similar Columns of K_{nk} Values into the Signum Function

This is best explained with the aid of the example for $N = 128$, Fig.A3.5 and the flowchart in Fig.A3.16. The OTS/OH set is considered with the sine K_{nk} value.

The shuffling routine has loaded SB with I_1, I_{63}, I_{65} and I_{127} . The SAG has generated a sine and cosine K_{nk} which are

I_n Sign Bit	K_n Sign Bit	Address Pair Sign Bit	Accumulator Operation
0	0	0	Add
0	1	1	Subtract
1	0	1	Subtract
1	1	0	Add

0 $\equiv$ Positive

1 $\equiv$ Negative

Fig.A 3.15 Signum Function

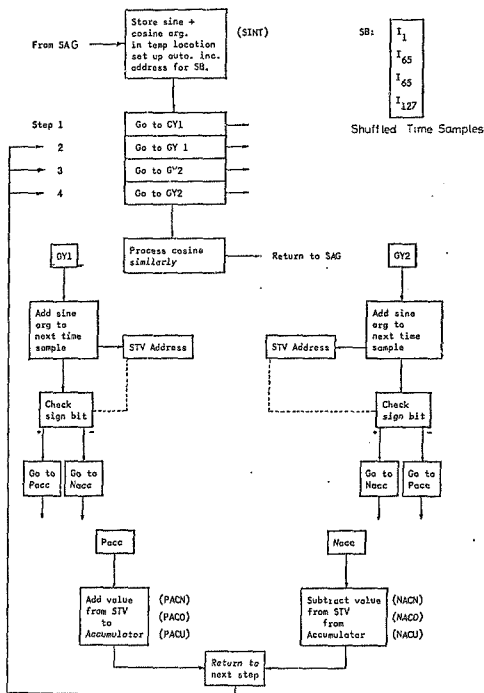


Fig.A3.1.6 Generation and Modification of Sine Function

stored in a temporary location as they must not be destroyed during the calculation.

It is added to the sine K_{nk} via path GY1. If the sign bit of the result is positive, the value in the STV, addressed by the magnitude of the result, is added to the Accumulator via path 'PACC'. If the sign bit is negative the STV value is subtracted from the Accumulator via path 'NACC'. The routine proceeds to step 2 and the process is repeated for I_{63} . The next time sample, I_{65} , has a column of K_{nk} arguments with opposite signs. At step 3, I_{65} is added to the sine K_{nk} via path GY2. If the sign bit of the result is positive, the STV constant, addressed by the magnitude of the result, is subtracted from the Accumulator via path 'NACC'. If the sign bit is negative, the STV constant is added to the Accumulator via path 'PACC'. The remaining step is processed similarly. The cosine K_{nk} has the order of the steps changed to GY1, GY2, GY2, GY1.

The step sequences for the remaining sets of columns are given in Fig.A3.5 where '+' and '-' correspond to GY1 and GY2 respectively.

A3.10.4 Accumulating the STV Constant and Checking for Overflow (OVF) or Underflow (UNF)

The STV constants and the Accumulator contents can be either positive or negative numbers. (The particular integration weights used to derive the STV constants are positive in this case but the algorithm is written for the general case.) Checks must

be made for OVF or UNF when addition or subtraction occurs. It must be noted that the STV constant is added to or subtracted from the Accumulator. Table A3.5 lists the checks that must be made.

Table A3.5

OVF and UNF Check

Sign Accumulator	Sign STV	Arith. Operation	Check
+	+	Add	OVF
+	-	Add	OK
-	+	Add	OK
-	-	Add	UNF
+	+	Sub	OK
+	-	Sub	OVF
-	+	Sub	UNF
-	-	Sub	OK

Before addition or subtraction can take place, two checks must be made.

1) Are the sign bits of the Accumulator and STV constant the same?

2) Is the Accumulator sign bit positive?

The first check is made using the 'Exclusive OR' routine.

The subprogram that implements the routine can be found in section A4.7.5.

A3.10.5 The Format and Addressing of the Accumulators

The accumulators are divided into 6 blocks.

- | | | | |
|----|--------------------------------|----|---------------------------|
| 1a | Odd Imaginary Harmonics | 1b | Odd Real Harmonics |
| 2a | $E\bar{4}$ Imaginary Harmonics | 2b | $E\bar{4}$ Real Harmonics |
| 3a | $E4$ Imaginary Harmonics | 3b | $E4$ Real Harmonics |

The auto incrementing address function⁺ is used extensively to address the Accumulators. The auto-incrementing addresses are set up in the program that generates the start and incrementing arguments (A4.6). On entering the TLUAR, the auto incrementing location addresses the required Accumulator and stores its contents in a temporary location (see A4.7.6). The 4 or 8 STV constants are added to or subtracted from the temporary location according to the routine described in A3.10.3. The contents of the temporary location are then returned to the correct Accumulator. The method of obtaining the STV address is covered in A3.10.3 and the Assembler program is covered in A4.7.1.

A3.10.5 Calculating the Resultant Harmonics

The format of the Accumulator blocks in the core is given in Fig.A3.17. The real harmonic component and the imaginary harmonic component are denoted a_k and b_k respectively. The harmonics are not in order but are sorted into groups of odd numbered, even multiples of four and the remaining even numbered harmonics. The routine must extract the harmonic components from the Accumulator block in the correct sequence and calculate the

resultant (see A4.9).

$$\text{ie. } F_k \propto \sqrt{a_k^2 + b_k^2}$$

The resultant must still be divided by 7 and adjusted by the overall scale factor (see Chapter 4.4)

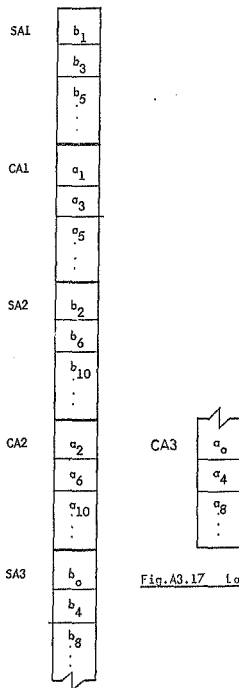


Fig.A3.17 Layout of Accumulators

A4 The Assembler Programme

A4.1 Introduction

The Assembler programme consists of a number of subprograms each covering an aspect of the algorithm presented in Appendix A3. Each subprogram can be run separately with simulated input data so that programming errors can be detected and the subprogram can be modified or corrected without affecting the remaining subprograms. Most of the algorithms in A3 (eg. the SAG) are implemented with nine similar subprograms; one for each set of columns of arguments. This results in a large number of similar, but simple, subprograms which is not efficient programming but it does ease detection of errors.

The subprograms perform the following tasks.

1. Initialize the Accumulator data blocks, ie. load zero into the Accumulator.
2. Calculate constants and the first group of shuffled time sample addresses. (CCL)
3. Sample the signal with the analog to digital converter and store the outputs in the arrays.
4. Shuffle the order of the time samples.

5. Generate the K_{nk} arguments with the signed address generator routine.

6. Combine the K_{nk} and I_n values to form the address pairs of the constant in the STV; obtain the constant and add/subtract it to/from the correct Accumulator.

7. Display or analyse the resulting harmonics.

The Run Program (A4.12) sets the number of bits that represent a constant in the STV and then calls CCL to calculate the constants and addresses for a given N. The Run Program then calls MCN (A4.11), the main control program, which completes the Discrete Fourier Transform.

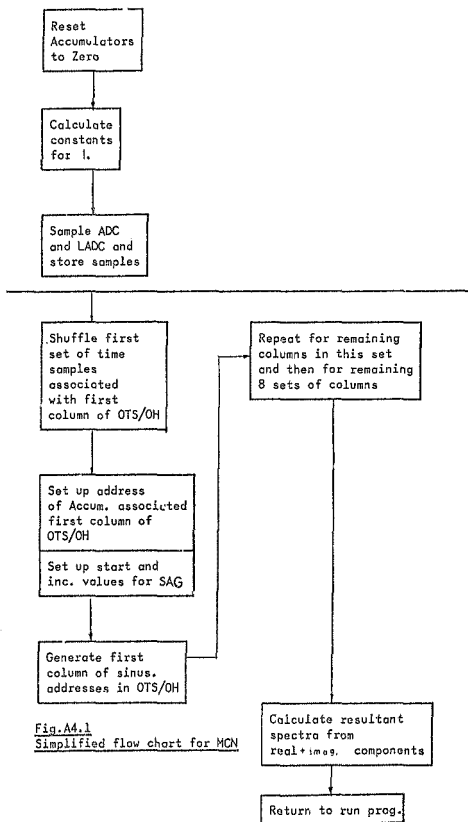


Fig.A4.1
Simplified flow chart for MCN

A4.2 Subprogram to Reset Accumulators

This subprogram loads zero into each location in the Accumulator blocks SA1, CA1, SA2, CA2, SA3, CA3. The number of locations in each block is given by CT1, CT2 and CT3, where CT1 is associated with SA1 and CA1, CT2 with SA2 and CA2, and CT3 with SA3 and CA3. CT1, CT2, and CT3 are calculated in the CCL subprogram.

```

P21:   STA 3,RP21      Save return.

        LDA 2,.CT1 )
        STA 2,.CT1 )   Set up index

        LDA 2,SA1      Load address of SA1 block
                        in auto inc. location.
        STA 2,20
        LDA 2,CA1      Load address of CA1 block.
                        in auto inc. location.
        STA 2,21
        LDA 1,Z         Load zero into register 1

P211:  STA 1,@20        Store zero into next location in SA1
                        block.
        STA 1,@21        Store zero into next location in CA1
                        block.

        DSZ .CT1         Decrement index
        JMP P211         If index is zero skip this instruction;
                        if greater than zero go to P211 and
                        initialize next pair of locations in
                        SA1 and CA1.

```

```

      .TITL  .P21
      .ENT   SP21
      .EXTD  SP21,PA2,PA3,CAL,CAL,CAL,CAL
      .EXTD  CTA,CT2,CT2
      .SPCL
      .LOC   164

SP21:  P21
      .NREL
P21    STA   1,SP21
      LDA   2,CT1
      STA   2,CT1
      LDA   2,PA1
      STA   2,20
      LDA   2,CAL
      STA   2,21
      LDA   1,Z
P211:  STA   1,020
      STA   1,021
      DSE   CT1
      JMP   P211
      LDA   2,CT2
      STA   2,CT2
      LDA   2,PA2
      STA   2,20
      LDA   2,CAL
      STA   2,21
      LDA   1,Z
P212:  STA   1,020
      STA   1,021
      DSE   CT2
      JMP   P212
      LDA   2,CT2
      STA   2,CT2
      LDA   2,PA2
      STA   2,20
      LDA   2,CAL
      STA   2,21
      LDA   1,Z
P213:  STA   1,020
      STA   1,021
      DSE   CT2
      JMP   P213
      JMP   07H21

CT1:   0
CT2:   0
CT3:   0
Z       0
SP21:   0
END

```

A4.3 The Sampling Subprogram

This sampling subprogram is used in the error analysis (A6) and it controls both the ADC and the LADC. Normally the LADC is used and the sections of the program that control the ADC are deleted. The detailed description of the ADC and the LADC is given in references 11 and 10 respectively. Both the ADC and the LADC are triggered simultaneously by an external pulse and the linearly quantised and logarithmically quantised values of the signal are stored in blocks R1 and MB respectively.

LDA 2,MB25	)	Set the auto inc. address for block
STA 2,22	)	MB
LDA 2,N		Set the number of pairs of samples
STA 2,.N		to be taken.
LDA 0,C		Send out control signal to
DOA 0,21		ADC.
LDA 2,R1		Set the auto. inc. address for
STA 2,21		block R1
P251: SKPDN 21	)	Wait until the ADC has processed
JMP .-1	)	a sample
DIAC 1,21		Load the encoded sample value into
		reg. 1.
STA 1,@21		Store contents of reg. 1 via auto.

	inc. address in R1.
SKPDN 22	Wait until the LADC has processed
JMP .-1	a sample.
DIAC 1,22	Load the encoded sample value into
	reg. 1.
STA 1,@22	Store the contents of reg.1 via auto.
	inc. address in MB.
DSZ .N	Reduce N by 1. If N is zero return
	to MCN program.
JMP P251	If N is not zero, go to P251:
JMP @RP25	Return to MCN.

```

          .VITL      .P25
          .ENT       SP25
          .EXTD      N, R1
          .EXTN      .MB
          .ZREL
          .LOC       166
SP25:    P25
P25:     STR        NFEL
          3, PF25
          LDA        2, MC25
          STA        2, 22
          LDA        2, N
          STA        2, N
          LDA        0, C
          DOR        0, 21
          LDA        2, R1
          STA        2, 21
P251:    SKFDN      21
          JMP        .-1
          DIAC       1, 21
          STA        1, 021
          SKFDN      22
          JMP        .-1
          DIAC       1, 22
          STA        1, 022
          DSZ        .N
          JMP        P251
          JNP        0PF25
C:       00
MB25:    .MB
.N:      0
PF25:    0
.END

```

A4.4 The Shuffling Subprograms

There are nine subprograms numbered from P31 to P39, each providing a set of shuffled I_n values for each of the nine sets of similar columns of K_{nk} values. 4 or 8 I_n values are shuffled out of MB and are placed consecutively in SB before the starting and incrementing arguments are generated for the column of K_{nk} values. The program has 2 entry points, P3 X 1 and P3 X 2

(X = 1 9) and is initially called through P3 X 1. The subsequent shuffled I_n values are obtained by calling P3 X 2.

Subprogram P37 contains a modification as I_0 , $I_{N/4}$, $I_{N/2}$ and $I_{3N/4}$ are not similar - I_0 and $I_{N/2}$ are similar and $I_{N/4}$ and $I_{3N/4}$ are similar.

The subprogram P31 is explained (set OTS/OH)

```

P311:  STA 3,RP31      Save return

        LDA 3,SB31    } Set auto. inc. address of
        STA 3,20      } block SB.

        LDA 2,MB5      Get the address of the first
                        shuffled time sample ( $I_1$ )

        STA 2,MB5      Store this address in a temporary
                        location

        LDA 0,0,2      Load the value of  $I_1$  into reg. 0.

        STA 0,@20      Store contents of reg. 0 into first
                        location in SB.

```

Locations MB5, MB14, MB7 and MB16 in program CCL contain the addresses of the first set of shuffled time samples is I_1 , $I_{N/2-1}$, $I_{N/2+1}$ and I_{N-1} . These addresses are stored in temporary locations .MB5, .MB14, .MB7 and .MB16. In part P312 these addresses are processed according to the formulae in A3.5.3.

```

P312:  STA 3, RP31      Save return

        LDA 1,N2.        Load reg 1 with N2. N2. corresponds
                        to 2 which is either added to or
                        subtracted from the shuffled address
                        to obtain the next shuffled address.

        LDA 3,SB31 )     Set auto. inc. address of
                      )
        STA 3,20  )     block SB.

        LDA 2,.MB       Get the first shuffled address
                        stored in the temporary location

        ADDZ 1,2        Add 2 to obtain next shuffled
                        address.

        STA. 2,. MB     Save new address in temporary
                        location.

        LDA 0,0,2       Load reg. 0 with the contents of the
                        new shuffled address.

        STA 0,@20       Store reg. 0. contents in first
                        location in SB.

```

.MB5 now contains the address of I_{1+2} .

LDA 2, .MB14

SUBO 1,2. Subtract 2 to obtain the next
shuffled address.

STA 2, .MB14

LDA 0,0,2.

STA 0,@20 Store the reg. 0. contents in
second location in SB.

.MB14 now contains address $I_{N/2-1-2}$.

The remaining two shuffled addresses are processed and SB
will contain the following time sample values.

SB: I_{1+2}

$I_{N/2-1-2}$

$I_{N/2+1+2}$

I_{N-1-2} .

in that order.

```

      .TITLE .PIL
      .ENV SP11,SP12
      .EXTN .SB
      .EXTD NEG,ME1, ME7,ME16
      .EFEL
      .LOC 200

SP11:  P11
SP12:  P12

      .MPEL
P11:   STA 3.FP11      JMP 0FF11
      LDA 3.FP11      .ME5 0
      STA 3.10        .ME14 0
                        .ME7 0
                        .ME16 0
                        N2 2
                        SP11 .SB
                        .END
                        ---
      LDA 2.ME14
      STA 2.ME14
      LDA 0.0.2
      STA 0.020

      LDA 2.ME7
      STA 2.ME7
      LDA 0.0.2
      STA 0.020

      LDA 2.ME16
      STA 2.ME16
      LDA 0.0.2
      STA 0.020

      JMP 0FF11

P12:   STA 3.FP11
      LDA 1.N2
      LDA 3.FP11
      STA 3.10

      LDA 2.ME5
      ADD2 1.2
      STA 2.ME5
      LDA 0.0.2
      STA 0.020

      LDA 2.ME14
      SUBO 1.2
      STA 2.ME14
      LDA 0.0.2
      STA 0.020

      LDA 2.ME7
      ADD2 1.2
      STA 2.ME7
      LDA 0.0.2
      STA 0.020

      LDA 2.ME16
      SUBO 1.2
      STA 2.ME16
      LDA 0.0.2
      STA 0.020

```

```

      .TITL .P12
      .ENT  SP21,SP22
      .EXTN  .SB
      .EXTD  MB3,MB13,MB2,MB14,MB7,MB15,MB6,MB16
      .ZREL
      .LOC   202

SP21:  P121
SP22:  P122

P121:  STA 3.RP32
      LDA 3.SB32
      STA 3.20

      LDA 2.MB5
      STA 2.MB5
      LDA 0.0.2
      STA 0.020

      LDA 2.MB13
      STA 2.MB13
      LDA 0.0.2
      STA 0.020

      LDA 2.MB6
      STA 2.MB6
      LDA 0.0.2
      STA 0.020

      LDA 2.MB14
      STA 2.MB14
      LDA 0.0.2
      STA 0.020

      LDA 2.MB7
      STA 2.MB7
      LDA 0.0.2
      STA 0.020

      LDA 2.MB15
      STA 2.MB15
      LDA 0.0.2
      STA 0.020

      LDA 2.MB3
      STA 2.MB3
      LDA 0.0.2
      STA 0.020

      LDA 2.MB16
      STA 2.MB16
      LDA 0.0.2
      STA 0.020

      JMP @PP32

P122:  STA 3.RP32
      LDA 1.1.2
      LDA 3.SB32
      STA 3.20

      LDA 2.MB5
      ADDZ 1.2
      STA 2.MB5
      LDA 0.0.2
      STA 0.020

      LDA 2.MB13
      LDA 1.2
      STA 2.MB13
      LDA 0.0.2
      STA 0.020

      LDA 2.MB6
      ADDZ 1.2
      STA 2.MB6
      LDA 0.0.2
      STA 0.020

      LDA 2.MB14
      SUBO 1.2
      STA 2.MB14
      LDA 0.0.2
      STA 0.020

      LDA 2.MB7
      ADDZ 1.2
      STA 2.MB7
      LDA 0.0.2
      STA 0.020

      LDA 2.MB15
      SUBO 1.2
      STA 2.MB15
      LDA 0.0.2
      STA 0.020

      LDA 2.MB3
      ADDZ 1.2
      STA 2.MB3
      LDA 0.0.2
      STA 0.020

      LDA 2.MB16
      ADDZ 1.2
      STA 2.MB16
      LDA 0.0.2
      STA 0.020

      JNP @PP32

```

		.TITL	.P33		
		.ENT	SP331, SP332		
		.EXTH	.SB		
		.EXTD	MB3, MB6, MB7, MB8		
		.CFEL			
		.LOC	204		
SP331:	P331				
SP332:	P332				
		.NFEL		JMP	SP333
P331:	STA	3, RP33	SP33:	0	
	LDA	3, SB33	MB5:	0	
	STA	3, 20	MB6:	0	
			MB7:	0	
	LDA	2, MB5	MB8:	0	
	STA	2, MB5	N2:	2	
	LDA	0, 0, 2	SE33:	SE	
	STA	0, 020	END		

	LDA	2, MB6	---		
	STA	2, MB6			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB7			
	STA	2, MB7			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB8			
	STA	2, MB8			
	LDA	0, 0, 2			
	STA	0, 020			
	JMP	SP333			
P332:	STA	3, RP33			
	LDA	1, N2			
	LDA	3, SE33			
	STA	3, 20			
	LDA	2, MB5			
	ADDZ	1, 2			
	STA	2, MB5			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB6			
	ADDZ	1, 2			
	STA	2, MB6			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB7			
	ADDZ	1, 2			
	STA	2, MB7			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB8			
	ADDZ	1, 2			
	STA	2, MB8			
	LDA	0, 0, 2			
	STA	0, 020			

```

      .TITL    .F34
      .ENT     SP341, SP342
      .EXTN     EE
      .EXTD     MB3, MB10, MB11, MB20
      .ZREL     .LOC      205

SP341:  PI41
SP342:  PI42

      .NREL
      JMP     @RP34

PI41:   STA     1, RP34      RP34:  0
      LDA     2, EE34      .MB3:  0
      STA     3, 20        .MB10: 0
                        .MB11: 0
      LDA     2, MB3      .MB20: 0
      STA     2, MB3      NJ      4
      LDA     0, 0, 2      EE34:  .SB
      STA     0, 020      .END
                        ---
      LDA     2, MB10
      STA     2, .MB10
      LDA     0, 0, 2
      STA     0, 020

      LDA     2, MB11
      STA     2, .MB11
      LDA     0, 0, 2
      STA     0, 020

      LDA     2, MB20
      STA     2, .MB20
      LDA     0, 0, 2
      STA     0, 020

      JMP     @RP34

PI42:   STA     1, RP34
      LDA     1, M4
      LDA     3, SB34
      STA     3, 20

      LDA     2, MB3
      ADD2    1, 2
      STA     2, MB5
      LDA     0, 0, 2
      STA     0, 020

      LDA     2, MB10
      SUB0    1, 2
      STA     2, MB13
      LDA     0, 0, 2
      STA     0, 020

      LDA     2, MB11
      ADD2    1, 2
      STA     2, MB11
      LDA     0, 0, 2
      STA     0, 020

      LDA     2, MB20
      SUB0    1, 2
      STA     2, MB20
      LDA     0, 0, 2
      STA     0, 020

```

```

      .TITL      .P35
      .ENT       SP351, SP352
      .EXTH      EB
      .EXTD      ME9, ME17, ME10, ME13, ME11, ME15, ME12, ME20
      .ZREL
      .LOC       210

SP351:  P351
SP352:  P352

P351:   STA     3, RF35
      LDA     2, SE25
      STA     3, 20

      LDA     2, ME9
      STA     2, ME9
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME17
      STA     2, ME17
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME10
      STA     2, ME10
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME13
      STA     2, ME13
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME11
      STA     2, ME11
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME19
      STA     2, ME19
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME12
      STA     2, ME12
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME20
      STA     2, ME20
      LDA     0, 0.2
      STA     0, 020

      JNP     ORF35

P352:   STA     3, RF35
      LDA     1, M4
      LDA     3, SE25
      STA     3, 20

      LDA     2, ME9
      RCOZ     1, 2
      STA     2, ME9
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME17
      SUBO     1, 2
      STA     2, ME17
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME10
      RCOZ     1, 2
      STA     2, ME10
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME13
      SUBO     1, 2
      STA     2, ME13
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME11
      RCOZ     1, 2
      STA     2, ME11
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME19
      SUBO     1, 2
      STA     2, ME19
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME12
      SUBO     1, 2
      STA     2, ME12
      LDA     0, 0.2
      STA     0, 020

      LDA     2, ME20
      RCOZ     1, 2
      STA     2, ME20
      LDA     0, 0.2
      STA     0, 020

      JNP     ORF35

```

```

      .TITL  .P36
      .ENY   SP161, SP162
      .EXTN   SB
      .EXTD   MB9, MB10, MB11, MB12
      .ZREL   212
      .LOC    212

SP161: P361
SP162: P362

      .NREL      SP16: 0      JMP      0SP16
P361:  STA      3, RP16      .MB9: 0
      LDA      3, SB16      .MB10: 0
      STA      3, 20        .MB11: 0
                               .MB12: 0
                               N4      4
      LDA      2, MB9      .SB16: .SB
      STA      2, .MB9      .END
      LDA      0, 0, 2      .END
      STA      0, 020
      .
      LDA      2, MB10
      STA      2, .MB10
      LDA      0, 0, 2
      STA      0, 020
      .
      LDA      2, MB11
      STA      2, .MB11
      LDA      0, 0, 2
      STA      0, 020
      .
      LDA      2, MB12
      STA      2, .MB12
      LDA      0, 0, 2
      STA      0, 020
      .
      JMP      0SP16

P362:  STA      3, RP36
      LDA      1, N4
      LDA      3, SB16
      STA      3, 20
      .
      LDA      2, .MB9
      ADDC     1, 2
      STA      2, .MB9
      LDA      0, 0, 2
      STA      0, 020
      .
      LDA      2, .MB10
      ADDC     1, 2
      STA      2, .MB10
      LDA      0, 0, 2
      STA      0, 020
      .
      LDA      2, .MB11
      ADDC     1, 2
      STA      2, .MB11
      LDA      0, 0, 2
      STA      0, 020
      .
      LDA      2, .MB12
      ADDC     1, 2
      STA      2, .MB12
      LDA      0, 0, 2
      STA      0, 020

```

```

TITLE P37
ENT SP37L,SP372
,ENTN .56
,EXTG MBL,M61,M621
,REL
LOC 214

SP371: P371
SP372: P372

P371: STA 3,RP37 JMF
LDA 3,SB37 ,MB1: 0
STA 3,20 ,MB3: 0
,MB21: 0
LDA 2,MB1 M4: 4
STA 2,MB1 SB37: .56
LDA 0,0,2 END
STA 0,020 ---
LDA 2,MB3 ---
STA 2,MB3 ---
LDA 0,0,2
STA 0,020
LDA 2,MB3
STA 2,MB3
LDA 0,0,2
STA 0,020
LDA 2,MB21
STA 2,MB21
LDA 0,0,2
STA 0,020
JMF 0RP37

P372: STA 3,RP37
LDA 1,M4
LDA 3,SB37
STA 3,20
LDA 2,MB1
ADD 1,2
STA 2,MB1
LDA 0,0,2
STA 0,020
LDA 2,MB3
SUB 1,2
STA 3,MB2
LDA 0,0,2
STA 0,020
LDA 2,MB3
ADD 1,2
STA 2,MB3
LDA 0,0,2
STA 0,020
LDA 2,MB21
SUB 1,2
STA 2,MB21
LDA 0,0,2
STA 0,020

```

		TITLE	. F33		
		ENT	SP131, SP132		
		. EXTN	. 50		
		. EXT0	MB1, MB2, MB3, MB4		
		. ZREL			
		. LOC	216		
SP131:	P131				
SP132:	P132				
		NREL		JMP	GRP35
P131:	STA	2, RP36	RP36:	0	
	LDA	3, SB38	. MB1:	0	
	STA	3, 20	. MB2:	0	
			. MB3:	0	
	LDA	2, MB1	. MB4:	0	
	STA	2, MB1	N4:	4	
	LDA	0, 0, 2	SB38:	. 50	
	STA	0, 020	. END		

	LDA	2, MB2	----		
	STA	2, MB2			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB3			
	STA	2, MB3			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB4			
	STA	2, MB4			
	LDA	0, 0, 2			
	STA	0, 020			
	JMP	GRP38			
P132:	STA	3, RP38			
	LDA	1, N4			
	LDA	3, SB38			
	STA	3, 20			
	LDA	2, MB1			
	AD02	1, 2			
	STA	2, MB1			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB2			
	AD02	1, 2			
	STA	2, MB2			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB3			
	AD02	1, 2			
	STA	2, MB3			
	LDA	0, 0, 2			
	STA	0, 020			
	LDA	2, MB4			
	AD02	1, 2			
	STA	2, MB4			
	LDA	0, 0, 2			
	STA	0, 020			

		TITL	.PI9	
		ENT	SP191, SP192	
		EXTN	.SE	
		EXTD	MB1, MB2, MB3, MB4	
		EREL		
		.LOC	220	
SP191:	PI91			
SP192:	PI92			
		EREL	FF19:	JMP 0FF19
PI91:	STA	3, FF19	MB1:	0
	LDA	3, SB19	MB2:	0
	STA	3, 20	MB3:	0
			MB4:	0
	LDA	2, MB1	MB:	4
	STA	2, MB1	SB19:	.SB
	LDA	0, 0, 2	END	
	STA	0, 020	--	
	LDA	2, MB2		
	STA	2, MB2		
	LDA	0, 0, 2		
	STA	0, 020		
	LDA	2, MB3		
	STA	2, MB3		
	LDA	0, 0, 2		
	STA	0, 020		
	LDA	2, MB4		
	STA	2, MB4		
	LDA	0, 0, 2		
	STA	0, 020		
	JMP	0FF19		
PI92:	STA	3, FF19		
	LDA	1, MB		
	LDA	3, SB19		
	STA	3, 20		
	LDA	2, MB1		
	ADD2	1, 2		
	STA	2, MB1		
	LDA	0, 0, 2		
	STA	0, 020		
	LDA	2, MB2		
	ADD2	1, 2		
	STA	2, MB2		
	LDA	0, 0, 2		
	STA	0, 020		
	LDA	2, MB3		
	ADD2	1, 2		
	STA	2, MB3		
	LDA	0, 0, 2		
	STA	0, 020		
	LDA	2, MB4		
	ADD2	1, 2		
	STA	2, MB4		
	LDA	0, 0, 2		
	STA	0, 020		

A4.5 Signed Address. Generator Subprogram (K_{nk})

This subprogram follows the flowchart in A3.6.4. The following values are passed to this subprogram from the Initialize SAC subprogram (A4.6).

- .H5 the start argument.
- .I5 the increment argument
- .C5 the number of K_{nk} addresses in a column of K_{nk} addresses.

CSR, MSK1, MSK2 are calculated by the CCL subprogram (A4.9) and modify the K_{nk} values into a multiple of 40₈. Table A4.1 lists the names of the SAC subprograms and is derived as follows.

1) The numbers in the name (ie 61, 62, 63, 64, 611, 612) give the entry point of the TLJAR (A4.7).

ie. this statement in a SAC subprogram, X.61 ($X = A, B$).

JSR @A61

means that the particular column of arguments being generated have a sign pattern.

sine +, +, -, -

cosine +, -, -, +

(See fig. A3.5)

Table A41 SAG Subprogram Names

SET	$0 < inc < \frac{H}{2}$	$\frac{H}{2} < inc < 77$	$77 < inc < \frac{2H}{2}$	$\frac{2H}{2} < inc < 2H$	$inc = 0$	$inc = \frac{H}{2}$	$inc = 77$	$inc = \frac{2H}{2}$
OTS OH	A61	B61						
OTS ECH	A62	B62						
OTS ECH	C64	D64	E64	F64				
E4TS OH	A61	B61						
E4TS ECH	A62	B62						
E4TS ECH	C64	D64	E64	F64				
E4TS OH	A61	B61			I611	J61	K612	
E4TS ECH	A63	B63	G63	H63	I63	J63	K63	L63
E4TS ECH	C64	D64	E64	F64	I64	M64	N64	O64

Table A42 SAG Increment and Output Values

TYPE	INCREMENT	K_{nk} OUTPUT EQUIVALENT TO
A	$0 < \text{inc} < \frac{\pi}{2}$	K_{nk} has all values except those equivalent to 0 and $\frac{\pi}{2}$ radians
B	$\frac{\pi}{2} < \text{inc} < \pi$	
G	$\pi < \text{inc} < \frac{3\pi}{2}$	
H	$\frac{3\pi}{2} < \text{inc} < 2\pi$	
C	$0 < \text{inc} < \frac{\pi}{2}$	K_{nk} has all values
D	$\frac{\pi}{2} < \text{inc} < \pi$	
E	$\pi < \text{inc} < \frac{3\pi}{2}$	
F	$\frac{3\pi}{2} < \text{inc} < 2\pi$	
I	$\text{inc} = 0$	$\text{sine } K_{nk} = 0 \quad \text{cosine } K_{nk} = \frac{\pi}{2}$
J	$\text{inc} = \frac{\pi}{2}$	$K_{nk} = \frac{\pi}{4}$
K	$\text{inc} = \pi$	$K_{nk} = 0 \text{ or } \frac{\pi}{4}$
L	$\text{inc} = \frac{3\pi}{2}$	$K_{nk} = \frac{\pi}{4}$
M	$\text{inc} = \frac{\pi}{2}$	$K_{nk} = 0 \text{ or } \frac{\pi}{2}$
N	$\text{inc} = \pi$	$\text{sine } K_{nk} = 0 \quad \text{cosine } K_{nk} = \frac{\pi}{2}$
O	$\text{inc} = \frac{3\pi}{2}$	$K_{nk} = 0 \text{ or } \frac{\pi}{2}$

The Assembler codes for program types ABGH are given first. Types CDEF are explained next. The final group, MNO are simple programs that have outputs equivalent to 0 on $\frac{\pi}{2}$ radians.

A4.5.1 Types ABGH

The instructions for state 1 are discussed and the differences between state 1 and the remaining states are listed.

Case 1 State 1

A61:	STA	3,RA61	Save return to MCN
	LDA	0,.H5	Load start argument (arg) into 'scratch pad' memory.
	JMP	OUPP	Go to output process. This corresponds to step 3 in flowchart
SUPP:	LDA	2,.I5	Get inc. arg.
	LDA	0,.H5	Get current subtotal.
1	ADDZ	2,0, SNC	Add inc to the subtotal to form the new current subtotal
			If CARRY bit is non zero skip next instruction (overflow occurs).
	JMP	OUPP	Go to output process (state 1).
	NEGZ	0,0	Carry bit was non zero ie. $\arg > \frac{\pi}{2}$
2	JMP	ODNP	Go to output process of state 2.
OUPP:	STA	0,.H5	Store current K_{nk} subtotal in scratch pad.
	MOVZ	0,1	Move K_{nk} into reg 1 for processing

	NEGZ 0,2	Add $\frac{\pi}{2}$ to $\sin K_{nk}$ to obtain cosine K_{nk} . Store in reg 2.
	LDA 3,MSK1	Load reg 3 with truncating mask
	ANDZ 3,1	Truncate sine K_{nk}
	JSR SR	This subroutine shifts the sine and cosine K_{nk} 6 places to the right
3	MOVZR 1,1 MOVZR 2,2	Set the sign bit in the CARRY bit and shift once more to the right.
	JSR @SP61	Go to TLUAR
	DSZ .C5	Return from TLUAR here. Decrement control counter and skip next instruction if .C5 is zero.
4	JMP SUPP	Go to state 1 and generate the next K_{nk} value.
	JMP .OTP	Return to MCN as the required number of K_{nk} values have been generated.

The marked statements, numbered from 1 to 4, change in the remaining states. The changes are listed below.

Case 1 State 2

1	SUBO 2,0, SNC	Subtract inc from subtotal. Go to state 2 output process.
	JMP ODNP	

2	JMP	OUPN	Go to state 3 output process.
3	MOVZR	1,1	Set sine sign bit positive
	MOVZR	2,2	Set cosine sign bit negative
4	JMP	SDNP	Go to beginning of state 2

Case 1 State 3

1	ADDZ	2,0,SNC	Add increment to K_{nk} subtotal
	JMP	OUPN	Go to state 3 output process
2	JMP	ODNN	Go to state 4 output process
3	MOVOR	1,1	Set sine sign bit negative
	MOVOR	2,2	Set cosine sign bit negative
4	JMP	SUPN	Go to beginning of state 3

Case 1 State 4

1	SUPN	2,0,SNC	Subtract inc from K_{nk} sub-total
			Go to state 4 output process
2	JMP	OUPP	Go to state 1 output process
3	MOVOR	1,1	Set sine sign bit positive
	MOVZR	2,2	Set cosine sign bit negative
4	JMP	SDNN	Go to beginning of state 4

Case 2

The incrementing argument has values between $\frac{\pi}{2}$ and π

The 'overflowed form' of the increment is used in this case. (see

A3.8.2) The marked statements 2 and 3 are the same as before.

Case 2 State 1

1	NEGZ	0,0	Add $\frac{\pi}{2}$ to current K_{nk} subtotal.
	ADDZ	2,0 SNC	Add inc to subtotal to form next
			K_{nk} value.
	JMP	OUPP	
4	JMP	SDNP	Go to beginning of state 2.

Case 2 State 2

1	NEGZ	0,0	Subtract $\frac{\pi}{2}$ from current K_{nk} subtotal .
	SUBO	2,0, SNC	Subtract inc from subtotal to form
			next K_{nk} value.
	JMP	ODNP	
4	JMP	SUPN	Go to beginning of state 3.

Case 2 State 3

1	NEGZ	0,0	Add $\frac{\pi}{2}$ to current K_{nk} subtotal
	ADDZ	2,0, SNC	
	JMP	OUPN	
4	JMP	SDNN	Go to beginning of state 4

Case 2 State 4

1	NEGZ	0,0	Subtract $\frac{\pi}{2}$ from current K_{nk} subtotal
	SUBO	2,0, SNC	
	JMP	ODNN	
4	JMP	SUPP	Go to beginning of state 1

Case 3

The incrementing argument has values between π and $\frac{3\pi}{2}$.

The 'overflowed' form of the incrementing argument is used. π is added by simply skipping one state.

Case 3 State 1

4 JMP SUPN Go to beginning of state 3.

Case 3 State 2

4 JMP SDNN Go to beginning of state 4

Case 3 State 3

4 JMP SUPP Go to beginning of state 1

Case 3 State 4

JMP SDNP Go to beginning of state 2

Case 4

The incrementing arguments have values between $\frac{3\pi}{2}$ and 2π

The 'overflowed' form of the incrementing argument is used. $\frac{3\pi}{2}$ is added by skipping two states.

Case 4 State 1

1 NEGZ 0,0 Add $\frac{3\pi}{2}$ to current K_{nk} subtotal.
 ADDZ 2,0,SNC Add increment to K_{nk} subtotal
 JMP OUPP

4 JMP SDNN Go to beginning of state 4.

Case 4 State 2

1 NEGZ 0,0 Subtract $\frac{3\pi}{2}$ from current K_{nk} subtotal
 SUBO 2,0,SNC Subtract increment from K_{nk} subtotal
 JMP ODNP
 4 JMP SUPP Go to beginning of state 1

Case 4 State 3

1 NEGZ 0,0 Add $\frac{3\pi}{2}$ to current K_{nk} subtotal
 ADDZ 2,0,SNC Add increment to current K_{nk} subtotal
 JMP OUPN
 4 JMP SDNP Go to beginning of state 2

Case 4 State 4

1 NEGZ 0,0 Subtract $\frac{3\pi}{2}$ from current K_{nk} subtotal
 SUBO 2,0,SNC Subtract increment from current K_{nk}
 subtotal
 JMP ODNN
 4 JMP SUPN Go to beginning of state 3

A4.5.2 Programs Types CDEF

These programs are similar to types ABGH but K_{nk} can have values equivalent to 0 radians and $\frac{\pi}{2}$ radians. The machine code equivalent to 0 and $\frac{\pi}{2}$ radians is 0_8 and 177777_8 (see definition A1.2.3). 0 radians occurs in states 2 and 4 because of the

properties of the machine code, but, by definition, 0 radians is the first K_{nk} argument in states 1 and 3. Thus the instruction to output 0 radians (positive) is in state 4 and the instruction for 0 radians (negative) is in state 2. This problem does not occur with $\frac{\pi}{2}$ radians and the method for dealing with this is given in A3.7.1.

The statements that differ from those in types ABEH are explained.

Case 1 State 1

C64:	STA	3,RC64	Save return to MCN.
	LDA	0,.H5	Load starting arg. into scratch pad memory
	JMP	TDNN	Go to state 4 output routine (start arg $\equiv$ 0 rad.)
SUPP:	LDA	2,.I5	
	LDA	0.H5	
	ADDZ	2,0,SNC	Add inc. to current K_{nk} . Skip next statement if OVF.
	JMP	OUPP	Go to state 1 output routine.
	MOVZ	0,QSNR	Overflow took place. Check whether subtotal is either $> \frac{\pi}{2}$ or $= \frac{\pi}{2}$ Skip next instruction if result is $> \frac{\pi}{2}$

JMP	TUPP	Result is equal to $\frac{\pi}{2}$ Go to special routine.
NEGZ	ODNP	Go to state 2 output process
TUPP: COMZ	0,1	Take one's complement of K_{nk} argument
MOVZ	0,2	Cosine K_{nk} is the same as the uncomplemented $K_{nk} \equiv \frac{\pi}{2}$
LDA	3,MSK2	Load special truncating mask
ANDZ	3,1	Mask out bits in positions
ANDZ	3,2	6,7,8
MOVZR	1,1	Set sine sign bit positive
MOVOR	2,2	Set cosine sign bit negative
JSP	@SP64	Go to TLUAR
DSZ	.C5	Decrement control index and skip next instruction is result is zero.
JMP	FUPP	
JMP	OTP	Return to MCN
FUPP: LDA	0,.I5	Reg. 0 contains the current K_{nk} argument which is zero. Adding the increment is implemented by loading it into reg. 0.
NEGZ	0,0	The result of this 'addition' always > $\frac{\pi}{2}$ and the 2^5 complement must be taken
JMP	ODNP	Go to state 2 output process.

OUPP: This set of instructions is the same as in A4.5.1.

Case 1 State 2

SDNP: LDA 2,I5
 LDA 0,.H5
 SU30 2,0,SNC

Subtract the increment from the current sine K_{nk} argument. If the sign bit is non zero (result negative) skip the next instruction.

JMP ZDNP
 NEGZ 0,0
 JMP OUPN

Result is negative. Take the 2^5 complement and go to the state 3 output process

ZDNP: MOVZ 0,QSZR

Check whether subtotal is ≥ 0 .

If equal to zero skip next instruction.

JMP ODNP

If subtotal ≥ 0 go to state 2 output process.

TDNP: MOVZ 0,1
 COMZ 0,2

sine K_{nk} arg $\equiv 0$ rad

Add $\frac{\pi}{2}$ to sine K_{nk} to derive.

cosine K_{nk} . Here sine $K_{nk} \equiv 0$ and

the one's complement is taken to

derive the machine code , 740₈.

LDA 3,MSK2

Load special truncating mask

ANDZ 3,1 }
 ANDZ 3,2 }

Mask out bits in positions 6,7,8

MCVOR 1,1

Set sine sign bit negative

MOVOR 2,2

Set cosine sign bit negative

JSR	@SP64	Go to TLUAR
DSZ	.CS	
JMP	FDNP	
JMP	OTP	
FDNP:	LDA 0,.I5	Same explanation as FUPP.
	JMP OUPN	Go to state 3 output process
LDNP:		Same as ODNP in A5.4.1.

The remaining 2 state and 3 cases are not explained as they follow a similar pattern to the previous cases in A5.4.1.

```

      TITL  .A61
      .ENT  SAG1
      .EXT0  .H5, I3, CS
      .EXTD  HSK1, CSR, SP61
      .ZFEL
      .LOC  300

SAG1:  A61
      NREL
A61:   STA  2, A61
      LDA  0, H5
      JMP  OUPF
SUPP:  LDA  2, I3
      LDA  0, H5
      ADDZ  2, 0, SNC
      JMP  OUPF
      NEGZ  0, 0
      JMP  ODNF
OUPF:  STA  0, H5
      MOVZ  0, 1
      NEGZ  0, 2
      LDA  3, HSK1
      ANDZ  3, 1
      ANDZ  3, 2
      JSR  SR
      MOVZ  1, 1
      MOVZ  2, 2
      JSR  06F61
      DSZ  .CS
      JMP  SUPP
      JMP  OTP

SONP:  LDA  2, I3
      LDA  0, H5
      SUBO  2, 0, SNC
      JMP  ODNF
      NEGZ  0, 0
      JMP  OUPN
ODNF:  STA  0, H5
      MOVZ  0, 1
      NEGZ  0, 2
      LDA  3, HSK1
      ANDZ  3, 1
      ANDZ  3, 2
      JSR  SR
      MOVZ  1, 1
      MOVZ  2, 2
      JSR  06F61
      DSZ  .CS
      JMP  SONP
      JMP  OTP

SUPN:  LDA  2, I3
      LDA  0, H5
      ADDZ  2, 0, SNC
      JMP  OUPN
      NEGZ  0, 0
      JMP  ODNF
OUPN:  STA  0, H5
      MOVZ  0, 1
      NEGZ  0, 2
      LDA  3, HSK1
      ANDZ  3, 1
      ANDZ  3, 2
      JSR  SR
      MOVZ  1, 1
      MOVZ  2, 2
      JSR  06F61
      DSZ  .CS
      JMP  SUPN
      JMP  OTP

SONN:  LDA  2, I3
      LDA  0, H5
      SUBO  2, 0, SNC
      JMP  ODNF
      NEGZ  0, 0
      JMP  OUPF
ODNF:  STA  0, H5
      MOVZ  0, 1
      NEGZ  0, 2
      LDA  3, HSK1
      ANDZ  3, 1
      ANDZ  3, 2
      JSR  SR
      MOVZ  1, 1
      MOVZ  2, 2
      JSR  06F61
      DSZ  .CS
      JMP  SONN
      JMP  OTP

OTP:   JMP  06A61

SR:    STA  3, PSR
      LDA  3, CSR
      STA  3, CS
PI:    MOVZ  1, 1
      MOVZ  2, 2
      DSZ  CS
      JMP  FI
      JMP  06F61

PA61:  0
CS:    0
PSR:   0
      END
      ---

```

```

      .TITL .B61
      .ENT  SB61
      .EXTD  .HS., IS., CS
      .EXTD  MEML, CSR, SP61
      .EFEL
      .LOC  301

SB61:  B61
      NPFL

B61:   STA  D, B61
      LDA  0., H5
      JMP  OUF:

SUPP:  LDA  2., IS
      LDA  0., H5
      NEGZ 0., 0
      ADDZ 2., 0, SNC
      JMP  OUP:
      NEGZ 0., 0
      JMF  OONP
      STA  0., H5
      MOVZ 0., 1
      NEGZ 0., 2
      LDA  3., MSK1
      ANDZ 3., 1
      ANDZ 3., 2
      JSP  SR
      MOVOR 1., 1
      MOVOR 2., 2
      JSR  B61
      CSZ  .CS
      JMP  SONP
      JMP  OTP

SONP:  LDA  2., IS
      LDA  0., H5
      NEGZ 0., 0
      SUBO 2., 0, SNC
      JMF  OONP
      NEGZ 0., 0
      JMP  OUP:
      STA  0., H5
      MOVZ 0., 1
      NEGZ 0., 2
      LDA  3., MSK1
      ANDZ 3., 1
      ANDZ 3., 2
      JSP  SR
      MOVOR 1., 1
      MOVOR 2., 2
      JSR  B61
      CSZ  .CS
      JMF  EUPN
      JMP  OTP

OONP:  STA  0., H5
      MOVZ 0., 1
      NEGZ 0., 2
      LDA  3., MSK1
      ANDZ 3., 1
      ANDZ 3., 2
      JSP  SR
      MOVOR 1., 1
      MOVOR 2., 2
      JSR  B61
      CSZ  .CS
      JMF  EUPN
      JMP  OTP

EUPN:  LDA  2., IS
      LDA  0., H5
      NEGZ 0., 0
      ADDZ 2., 0, SNC
      JMP  OUPN
      NEGZ 0., 0
      JMF  OONN
      STA  0., H5
      MOVZ 0., 1
      NEGZ 0., 2
      LDA  3., MSK1
      ANDZ 3., 1
      ANDZ 3., 2
      JSP  SR
      MOVOR 1., 1
      MOVOR 2., 2
      JSR  B61
      CSZ  .CS
      JMF  EUPN
      JMP  OTP

OUPN:  STA  0., H5
      MOVZ 0., 1
      NEGZ 0., 2
      LDA  3., MSK1
      ANDZ 3., 1
      ANDZ 3., 2
      JSP  SR
      MOVOR 1., 1
      MOVOR 2., 2
      JSR  B61
      CSZ  .CS
      JMF  SONP
      JMP  OTP

OONN:  STA  0., H5
      MOVZ 0., 1
      NEGZ 0., 2
      LDA  3., MSK1
      ANDZ 3., 1
      ANDZ 3., 2
      JSP  SR
      MOVOR 1., 1
      MOVOR 2., 2
      JSR  B61
      CSZ  .CS
      JMF  SUPP
      JMP  OTP

OTP:   JMF  B61

SR:    STA  3., CSR
      LDA  3., CS
      STA  3., CS

P1:    MOVOR 1., 1
      MOVOR 2., 2
      CSZ  .CS
      JMF  P1
      JMP  B61

B61:   0
CS:    0
B61:   0
      .END

```

```

      .TITL      .I611
      .ENT       S1611
      .EXTD      H3, I3, C5
      .EXTD      MSK2, SP611
      .ZFEL
      .LOC       320

S1611:  I611
        NPEL
I611:   STA     3, R1611
TUPP:   LDA     0, H5
        MOVZ    0, 1
        COMZ    0, 2
        STA     0, H5
        LDA     3, MSK2
        ANDZ    3, 1
        ANDZ    3, 2
        MOVER   1, 1
        MOVER   2, 2
        JSR     @SP611
        OSZ     C5
        JMP     TUPP
        JMP     OTP
OTP:    JMP     @R1611
R1611:  0
      .END
      -----

```

```

      .TITL      .K612
      .ENT       SK612
      .EXTD      H3, I3, C5
      .EXTD      MSK2, SP612
      .ZFEL
      .LOC       322

SK612:  K612
        NPEL
K612:   STA     3, RK612
TONP:   LDA     0, H5
        COMZ    0, 1
        MOVZ    0, 2
        STA     0, H5
        LDA     3, MSK2
        ANDZ    3, 1
        ANDZ    3, 2
        MOVZP   1, 1
        MOVZP   2, 2
        JSR     @SP612
        OSZ     C5
        JMP     TDNN
        JMP     OTP
TDNN:   LDA     0, H5
        COMZ    0, 1
        MOVZ    0, 2
        STA     0, H5
        LDA     3, MSK2
        ANDZ    3, 1
        ANDZ    3, 2
        MOVZP   1, 1
        MOVZP   2, 2
        JSR     @SP612
        OSZ     C5
        JMP     TDNP
        JMP     OTP
OTP:    JMP     @RK612
RK612:  0
      .END
      -----

```

```

TITL      J61
ENT       SJS1
EXTD      .40. 15. C5
EXTD      15-1. C5R. SP61
JFEL
LOC       221

SUB1:     J61
J61:      STA 3.8JS1
        LDA 0. .H5
        JMP OUFF
BUFF:     LDA 2. .15
        LDA 0. .H5
        NEGZ 0.0
        ADDZ 2.0. SMC
        JMP OUFF
        NEGZ 0.0
        JMP ODNF
OUFF:     STA 0. .H5
        MOVZ 0.1
        NEGZ 0.2
        LDA 3. MSK1
        ANDZ 3.1
        ANDZ 3.2
        JSR SR
        MOVZF 1.1
        MOVZF 2.2
        JSR ASFE1
        DSZ C5
        JMP SONP
        JMP OTP

SONP:     LDA 2. .15
        LDA 0. .H5
        NEGZ 0.0
        SUBZ 2.0. SMC
        JMP ODNF
        NEGZ 0.0
        JMP OUFN
ODNF:     STA 0. .H5
        MOVZ 0.1
        NEGZ 0.2
        LDA 3. MSK1
        ANDZ 3.1
        ANDZ 3.2
        JSR SR
        MOVZF 1.1
        MOVZF 2.2
        JSR ASFE1
        DSZ C5
        JMP SUB1
        JMP OTP

SUBN:     LDA 2. .15
        LDA 0. .H5
        NEGZ 0.0
        SUBZ 2.0. SMC
        JMP ODNF
        NEGZ 0.0
        JMP OUFF
ODNF:     STA 0. .H5
        MOVZ 0.1
        NEGZ 0.2
        LDA 3. MSK1
        ANDZ 3.1
        ANDZ 3.2
        JSR SR
        MOVZF 1.1
        MOVZF 2.2
        JSR ASFE1
        DSZ C5
        JMP SUBN
        JMP OTP

OTF:      JMP 0FJ61

DR:       STA 3.8JS1
        LDA 3. C5R
        STA 1. C5
R1:       MOVZF 1.1
        MOVZF 2.2
        DSZ C5
        JMP F1
        JMP 0F5R

RJS1:     0
R5R:      0
C5:       0
END

```

		ASZ		SUPN.	LDA	2. 15
	ENT	FA62			LDA	0. 15
	EXTD	15. 15. C5			MOVB	2. 0. SNC
	EXTD	MSK1, CSR, SP62			JMP	OUFN
	ZFEL				NEGZ	0. 0
	LOC	302			JMP	OCNN
SP62:	ASZ			OUFN.	STA	0. 15
	MFEL				MOVZ	0. 1
ASZ:	STA	3. FA62			NEGZ	0. 2
	LDA	0. 15			LDA	3. MSK1
	JMP	OUFP			ANDZ	3. 1
SUPP:	LDA	2. 15			ANDZ	3. 2
	LDA	0. 15			JSP	SR
	MOVB	2. 0. SNC			MOVOR	1. 1
	JMP	OUFP			MOVOR	2. 2
	NEGZ	0. 0			JSP	SP62
	JMP	OCNN			DSZ	. C5
OUFP:	STA	0. 15			JMP	SUPN
	MOVZ	0. 1			JMP	OTP
	NEGZ	0. 2				
	LDA	3. MSK1			SCNN:	LDA
	ANDZ	3. 1				LDA
	ANDZ	3. 2				SUBO
	JSP	SR				JMP
	MOVOR	1. 1				NEGZ
	MOVOR	2. 2				JMP
	JSP	SP62			OCNN:	STA
	DSZ	. C5				MOVZ
	JMP	SUPP				NEGZ
	JMP	OTP				LDA
						ANDZ
OCNN:	LDA	2. 15				ANDZ
	LDA	0. 15				JSP
	SUBO	2. 0. SNC				MOVOR
	JMP	OCNN				MOVOR
	NEGZ	0. 0				JSP
	JMP	OUFN				DSZ
	STA	0. 15				JMP
	MOVZ	0. 1				JMP
	NEGZ	0. 2				
	LDA	3. MSK1			OTP:	JMP
	ANDZ	3. 1				
	ANDZ	3. 2			SR:	STA
	JSP	SR				LDA
	MOVOR	1. 1				STA
	MOVOR	2. 2				MOVZ
	JSP	SP62			P1:	MOVZ
	DSZ	. C5				DSZ
	JMP	OCNN				JMP
	JMP	OTP				JMP
					FA62:	0
					C5:	0
					SP62:	0
					END	

```

      .TITL  .B62
      .ENT   SB62
      .EXTD  .H3. .15. .C5
      .EXTD  MSK1, CSP, SP62
      ZPEL
      .LOC   303

SB62:  B62      .NREL
      B62      STA 3, PB62
      LDA 0. .H5
      JMP OUPF
SUPP:  LDA 2. .15
      LDA 0. .H5
      NEGZ 0. 0
      ADDZ 2. 0. SNC
      JMP OUPF
      NEGZ 0. 0
      JMP OONP
OUPF:  STA 0. .H5
      MOVZ 0. 1
      NEGZ 0. 2
      LDA 3, MSK1
      ANDZ 3. 1
      ANDZ 3. 2
      JSP SR
      MOVZ 1. 1
      MOVZ 2. 2
      JSP QSF62
      DSZ .C5
      JMP SDNP
      JMP OTP

SDNP:  LDA 2. .15
      LDA 0. .H5
      NEGZ 0. 0
      SUBO 2. 0. SNC
      JMP OONP
      NEGZ 0. 0
      JMP OUPF
      STA 0. .H5
      MOVZ 0. 1
      NEGZ 0. 2
      LDA 3, MSK1
      ANDZ 3. 1
      ANDZ 3. 2
      JSP SP
      MOVZ 1. 1
      MOVZ 2. 2
      JSP QSF62
      DSZ .C5
      JMP SUFN
      JMP OTP

SUFN:  LDA 2. .15
      LDA 0. .H5
      NEGZ 0. 0
      ADDZ 2. 0. SNC
      JMP OUPF
      MOVZ 0. 1
      MOVZ 2. 2
      JSP QSF62
      DSZ .C5
      JMP SDNN
      JMP OTP

SDNN:  LDA 2. .15
      LDA 0. .H5
      NEGZ 0. 0
      SUBO 2. 0. SNC
      JMP OONN
      NEGZ 0. 0
      JMP OUPF
OONN:  STA 0. .H5
      MOVZ 0. 1
      NEGZ 0. 2
      LDA 3, MSK1
      ANDZ 3. 1
      ANDZ 3. 2
      JSP SR
      MOVZ 1. 1
      MOVZ 2. 2
      JSP QSF62
      DSZ .C5
      JMP SUFP
      JMP OTP

OTP:  JMP QSF62

SR:  STA 3, ASP
      LDA 3, CSP
      STA 3, C5
P1:  MOVZ 1. 1
      MOVZ 2. 2
      DSZ C5
      JMP P1
      JMP QSF62

P62:  0
C5:  0
RSP:  0
      .END

```

		.TITL	.R63		SUPN.	LDA	2. IS
		.ENT	SAB3			LDA	0. HS
		.EXT0	H3. IS. C5			ANDZ	2.0. SNC
		.EXT0	MSK1. CSR. SF63			JMP	ODNN
		.ZFEL				JMP	NEIZ
		.LOC	110			JMP	ODNN
SAB3.	R63				QUPN.	STA	0. HS
		.AREL				MOVZ	0.1
MS3.	STA	3. R63				NEGZ	0.2
	LDA	0. HS				LDA	3. MSK1
	JMP	QUPN				ANDZ	1.1
SUPP.	LDA	2. IS				ANDZ	1.2
	LDA	0. HS				JSR	SR
	ADDZ	2.0. SNC				MOVOP	1.1
	JMP	QUPN				MOVOP	2.2
	NEGZ	0.0				JSR	BF63
	JMP	ODNN				OSZ	C5
QUPN.	STA	0. HS				JMP	SUPN
	MOVZ	0.1				JMP	OTF
	NEGZ	0.2					
	LDA	3. MSK1			SDNN.	LDA	2. IS
	ANDZ	1.1				LDA	0. HS
	ANDZ	1.2				SUBO	2.0. SNC
	JSR	SR				JMP	ODNN
	MOVOP	1.1				NEGZ	0.0
	MOVOP	2.2				JMP	QUPN
	JSR	BF63			ODNN.	STA	0. HS
	OSZ	C5				MOVZ	0.1
	JMP	SUPP				NEGZ	0.2
	JMP	OTF				LDA	3. MSK1
						ANDZ	1.1
SDNN.	LDA	2. IS				ANDZ	1.2
	LDA	0. HS				JSR	SR
	SUBO	2.0. SNC				MOVOP	1.1
	JMP	ODNN				MOVOP	2.2
	NEGZ	0.0				JSR	BF63
	JMP	QUPN				OSZ	C5
ODNN.	STA	0. HS				JMP	SDNN
	MOVZ	0.1				JMP	OTF
	NEGZ	0.2					
	LDA	3. MSK1			OTF.	JMP	BF63
	ANDZ	1.1					
	ANDZ	1.2			SR.	STA	3. R63
	JSR	SR				LDA	3. CSR
	MOVOP	1.1				STA	3. C5
	MOVOP	2.2			P1.	MOVOP	1.1
	JSR	BF63				MOVOP	2.2
	OSZ	C5				OSZ	C5
	JMP	SDNN				JMP	1
	JMP	OTF				JMP	OTF
					FACE.	0	
					C5.	0	
					R63.	0	
					ENG		


```

      .TITL      G63
      .ENT       SG63
      .ENTO      HS, IS, CS
      .ENTO      MSK1, CSF, SP63
      .REL
      .LOC       112

SC 3:  G63
      NREL
      SUPN.     LDR      2, IS
      G63:     STA      3, SG62
               LDR      0, HS
               JMF      00NF
      SUPP:     LDR      2, IS
               LDR      0, HS
               ADDZ     2, 0, SNC
               JMF      00NF
               NEGZ     0, 0
               JMF      00NF
      OUPF:     STA      0, HS
               MOVZ     0, 1
               NEGZ     0, 2
               LDR      3, MSK1
               ANDZ     3, 1
               ANDZ     7, 2
               JFR      SF
               MOVZF    1, 1
               MOVZF    2, 2
               JFR      SP63
               DSZ      CS
               JMF      SUPN
               JMF      0TP

      SCNF:     LDR      2, IS
               LDR      0, HS
               SUBO     2, 0, SNC
               JMF      00NF
               NEGZ     0, 0
               JMF      00NF
      00NF:     STA      0, HS
               MOVZ     0, 1
               NEGZ     0, 2
               LDR      3, MSK1
               ANDZ     3, 1
               ANDZ     7, 2
               JFR      SF
               MOVZF    1, 1
               MOVZF    2, 2
               JFR      SP63
               DSZ      CS
               MOVZF    1, 1
               MOVZF    2, 2
               JFR      SP63
               DSZ      CS
               JMF      SCNF
               JMF      0TP

      OTR:      JMF      0SG63

      SP:       STA      3, CSF
               LDR      3, CSF
               STA      3, CS
               MOVZF    1, 1
               MOVZF    2, 2
               DSZ      CS
               JMF      P1
               JMF      0TR

      P0:       0
      P1:       0
      CS:       0
      .END
      =====

```

		TITL	H63		SUPN:	LDA	2. 15
		.ENT	SH63			LDA	0. 15
		.EXTD	H63, 15. C5			NEGZ	0. 0
		.EXTD	H63, 15. C5P, SP63			ANDZ	2. 0 SNC
		.ZFEL				JMP	OUFN
		.LOC	311			NEGZ	0. 0
SH63:	H63					JMP	OUFN
		.NREL				STA	0. 15
H63:	STA	1. PH63			OUFN:	MOVE	0. 1
	LDA	0. 15				NEGZ	0. 2
	JMP	OUFN				LDA	1. MSK1
SUPP:	LDA	2. 15				ANDZ	3. 1
	LDA	0. 15				ANDZ	3. 2
	NEGZ	0. 0				JMP	SP
	MOVZ	2. 0. SNC				MOVZ	1. 1
	JMP	OUFN				MOVZ	2. 2
	NEGZ	0. 0				JMP	9SP63
	JMP	OUFN				OSZ	C5
OUFN:	STA	0. 15				JMP	SOUN
	MOVZ	0. 1				JMP	OTP
	NEGZ	0. 2					
	LDA	1. MSK1			EDNN:	LDA	2. 15
	ANDZ	3. 1				LDA	0. 15
	ANDZ	3. 2				NEGZ	0. 0
	JMP	SP				SUBO	2. 0. SNC
	MOVZ	1. 1				JMP	OUFN
	MOVZ	2. 2				NEGZ	0. 0
	JMP	9SP63				JMP	OUFN
	OSZ	C5				STA	0. 15
	JMP	SOUN			EDNN:	MOVZ	0. 1
	JMP	OTP				NEGZ	0. 2
						LDA	1. MSK1
ENNF:	LDA	2. 15				ANDZ	1. 1
	LDA	0. 15				ANDZ	1. 2
	NEGZ	0. 0				JMP	SP
	SUBO	2. 0. SNC				MOVZ	1. 1
	JMP	OUFN				MOVZ	2. 2
	NEGZ	0. 0				JMP	9SP63
	JMP	OUFN				OSZ	C5
OUFN:	STA	0. 15				JMP	SOUN
	MOVZ	0. 1				JMP	OTP
	NEGZ	0. 2					
	LDA	1. MSK1			OTP:	JMP	9SP63
	ANDZ	3. 1					
	ANDZ	3. 2			SP:	STA	1. 15
	JMP	SP				LDA	1. C5P
	MOVZ	1. 1				STA	1. C5
	MOVZ	2. 2			P1:	MOVZ	1. 1
	JMP	9SP63				MOVZ	2. 2
	OSZ	C5				OSZ	C5
	JMP	SOUN				JMP	P1
	JMP	OTP				JMP	9SP63
					PH63	0	
					SP	0	
					C5	0	
					SNC		

```

          TITL      163
          ENT       5163
          EXT0      40, 15, C5
          EXT0      MSK2, SP83
          EFEL
          LCC       314
5163:      163
          MREL
163:      STA      3, R163
TUFF:      LDA      0, H5
          MOVE      0, 1
          COMZ      0, 2
          STA      0, H5
          LDA      1, MSK2
          ANDZ      1, 1
          ANDZ      1, 2
          MOWEP     1, 1
          MOWEP     2, 2
          JEP       0, SP83
          DZ2       C5
          JMP       TUFF
          JMF       QTP
QTP:      JMF       0, R163
FIS3:      0
END

```

[illegible]

R. J. 0
 H. F. 0
 C. S. 0
 END

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```

TITL      M63
ENT       SP62
EXTD      M63 ID.05
EXTD      M63 SP62
LTEL      L00      116
LOC

SH62:     M63      M63L
M63      STA      3.0063
TEND      LDA      0.45
          COM2      0.1
          MOVE      0.2
          STA      0.45
          LDA      3.0062
          AND2      3.1
          AND2      3.2
          MOW2      1.1
          MOW2      2.2
          JEP      SP62
          GZ       CS
          JMP      TEND
          JMP      OFF
TEND      LDA      0.45
          COM2      0.1
          MOVE      0.2
          STA      0.45
          LDA      3.0062
          AND2      3.1
          AND2      3.2
          MOW2      1.1
          MOW2      2.2
          JEP      SP62
          GZ       CS
          JMP      TEND
          JMP      OFF
OFF       JMP      SP62
R662      0
END

```

		TITL	LE3		
		ENT	SL3		
		EXTD	H3	IS	13
		EXTD	MSL	CF	SP3
		DREL			
		LOC	217		
SL3:	LE3				
		INFL			
LE3:	STA	0.0	FL3		
	LDA	0.0	H3		
	JMP	0.0	CF		
SVFF:	LDA	2.0	IS		
	LDA	0.0	H3		
	NEGZ	0.0			
	ADCC	2.0	ENC		
	JMP	0.0	CF		
	NEGZ	0.0			
	JMP	0.0	CF		
OVFF:	STA	0.0	H3		
	MOVZ	0.1			
	NEGZ	0.2			
	LDA	2.0	MSL		
	ANDZ	2.1			
	ANDZ	2.2			
	JEP	2.3			
	MOVZ	2.4			
	MOVZ	2.5			
	JEP	2.6	SP3		
	DSZ	2.7	CF		
	JMP	2.8	CF		
	JMP	2.9	CF		
OVFF:	LDA	2.0	IS		
	LDA	0.0	H3		
	NEGZ	0.0			
	SUBO	2.0	ENC		
	JMP	0.0	CF		
	NEGZ	0.0			
	JMP	0.0	CF		
	STA	0.0	H3		
	MOVZ	0.1			
	NEGZ	0.2			
	LDA	2.0	MSL		
	ANDZ	2.1			
	ANDZ	2.2			
	JEP	2.3			
	MOVZ	2.4			
	MOVZ	2.5			
	JEP	2.6	SP3		
	DSZ	2.7	CF		
	JMP	2.8	CF		
	JMP	2.9	CF		

SVFF:	LDA	2.0	IS
	LDA	0.0	H3
	NEGZ	0.0	
	ADCC	2.0	ENC
	JMP	0.0	CF
	NEGZ	0.0	
	JMP	0.0	CF
OVFF:	STA	0.0	H3
	MOVZ	0.1	
	NEGZ	0.2	
	LDA	2.0	MSL
	ANDZ	2.1	
	ANDZ	2.2	
	JEP	2.3	
	MOVZ	2.4	
	MOVZ	2.5	
	JEP	2.6	SP3
	DSZ	2.7	CF
	JMP	2.8	CF
	JMP	2.9	CF
OVFF:	LDA	2.0	IS
	LDA	0.0	H3
	NEGZ	0.0	
	SUBO	2.0	ENC
	JMP	0.0	CF
	NEGZ	0.0	
	JMP	0.0	CF
OVFF:	STA	0.0	H3
	MOVZ	0.1	
	NEGZ	0.2	
	LDA	2.0	MSL
	ANDZ	2.1	
	ANDZ	2.2	
	JEP	2.3	
	MOVZ	2.4	
	MOVZ	2.5	
	JEP	2.6	SP3
	DSZ	2.7	CF
	JMP	2.8	CF
	JMP	2.9	CF
OVFF:	JMP	2.9	CF
ER:	STA	2.0	SP3
	LDA	2.0	CF
	STA	2.0	CF
FI	MOVZ	2.0	
	MOVZ	2.1	
	DSZ	2.2	
	DSZ	2.3	
	JMP	2.4	
	JMP	2.5	
PL3:	0		
SR	0		
CS	0		
END			

		TITL	CF4		
		ENT	SC44		
		ENTC	MS. 17. CT		
		ENTD	MSK1. MSK2. CIP. SP44		
		REFL			
		LOC	104		
SC44	CF4				
		REFL			
CF4:	STA	0. SC44			
	LDA	0. MS			
	JMP	TOWN			
EUFF:	LDA	2. IS			
	LDA	0. MS	SC44	LDA	2. IS
	ADDZ	2. 0. ENC		LDA	0. MS
	JMP	CUFF		EJED	2. 0. ENC
	MOVE	0. 0. ENR		JMP	EDNP
	JMP	TUFF		NEGZ	0. 0
	NEGZ	0. 0		JMP	CUPN
	JMP	ODNP	EDNP	MOVE	0. 0. SZP
TUFF:	CONZ	0. 1		JMP	ODNP
	MOVE	0. 1	TONE	MOVE	0. 1
	LDA	1. MSK2		CONZ	0. 1
	ANDZ	1. 1		LDA	1. MSK2
	ANDZ	1. 1		ANDZ	1. 1
	MOVOR	1. 1		ANDZ	1. 1
	MOVOR	2. 2		MOVOR	1. 1
	JEP	SP44		MOVOR	2. 2
	DEZ	CS		JEP	SP44
	JMP	FUFF		DEZ	CT
	JMP	OTR		JMP	EDNP
FUFF:	LDA	0. IS		JMP	OTR
	NEGZ	0. 0	FCNP	LDA	0. IS
	JMP	ODNP		JMP	CUPN
CUFF:	STA	0. MS	ODNP	STA	0. MS
	MOVE	0. 1		MOVE	0. 1
	NEGZ	0. 1		NEGZ	0. 1
	LDA	1. MSK1		LDA	1. MSK1
	ANDZ	1. 1		ANDZ	1. 1
	ANDZ	1. 1		ANDZ	1. 1
	JEP	SR		JEP	SR
	MOVOR	1. 1		JEP	SR
	MOVOR	2. 2		MOVOR	1. 1
	JEP	SP44		MOVOR	2. 2
	DEZ	CS		JEP	SP44
	JMP	FUFF		DEZ	CS
	JMP	OTR		JMP	EDNP
				JMP	OTR

```

OTP:    JMP      BRCS4
RC64:   0

EUPN:   LDA      2, 15
        LDA      0, 15
        ADDZ     2, 0, SNC
        JMP      OUPN
        MOVZ     0, 0, SNE
        JMP      TUPN
        NEGZ     0, 0
        JMP      OONN
TURN:   COMZ     0, 1
        MOVZ     0, 2
        LDA      2, MEM2
        ANDZ     3, 1
        ANDZ     3, 2
        MOVOP    1, 1
        MOVOP    2, 2
        JEF      @SF64
        DSZ      1, CS
        JMF      FUPN
        JMF      OTF
FUPN:   LDA      0, 15
        NEGZ     0, 0
        JMP      OONN
OUPN:   STA      0, 15
        MOVZ     0, 1
        NEGZ     0, 2
        LDA      2, MEM1
        ANDZ     3, 1
        ANDZ     3, 2
        JEF      SF
        MOVOP    1, 1
        MOVOP    2, 2
        JEF      @SF64
        DSZ      1, CS
        JMF      EUPN
        JMF      OTF

EDNN:   LDA      2, 15
        LDA      0, 15
        SUBO     2, 0, ENC
        JMP      EDNN
        NEGZ     0, 0
        JMP      OUPP
EDNN:   MOVZ     0, 0, SZF
        JMP      OONN
TONN:   MOVZ     0, 1
        COMZ     0, 2
        LDA      2, MEM2
        ANDZ     3, 1
        ANDZ     3, 2
        MOVOP    1, 1
        MOVOP    2, 2
        JEF      @SF64
        DSZ      1, CS
        JMP      EDNN
        JMF      OTF
EDNN:   LDA      0, 15
        JMP      OUPP
OONN:   STA      0, 15
        MOVZ     0, 1
        NEGZ     0, 2
        LDA      2, MEM1
        ANDZ     3, 1
        ANDZ     3, 2
        JEF      SF
        MOVOP    1, 1
        MOVOP    2, 2
        JEF      @SF64
        DSZ      1, CS
        JMP      EDNN
        JMF      OTF

SF:     STA      2, @SF
        LDA      3, CSF
        STA      3, CS
        MOVZ     1, 1
        MOVZ     2, 2
        DSZ      CS
        JMF      FL
        JMF      @RSP
CS:     0
REF:    0
END

```

```

      .TITL  E64
      .ENT   SE64
      .EXTD  HS, IS, CS
      .EXTD  MSK1, MSK2, CS, ZF64
      .EFEL
      .LOC   306

SE64:  E64
      .NREL
E64:   STA  3, SE64
      LDA  0, HS
      JMP  TONP
SUPP:  LDA  2, IS
      LDA  0, HS
      ADD2  2, 0, SNC
      JMP  OUPP
      MOV2  0, 0, JNR
      JMP  TUPP
      NEG2  0, 0
      JMP  OONP
TUPP:  COM2  0, 1
      MOV2  0, 2
      LDA  2, MSK2
      AND2  3, 1
      AND2  3, 2
      MOVR  1, 1
      MOVR  2, 2
      JEP  SEP64
      DSZ  CS
      JMP  FUPP
      JMP  OTP
FUPP:  LDA  0, IS
      NEG2  0, 0
      JMP  OONN
OUPP:  STA  0, HS
      MOV2  0, 1
      NEG2  0, 2
      LDA  2, MSK1
      AND2  3, 1
      AND2  3, 2
      JEP  SP
      MOVR  1, 1
      MOVR  2, 2
      JEP  SEP64
      DSZ  CS
      JMP  SUPN
      JMP  OTP

SONP:  LDA  2, IS
      LDA  0, HS
      SUB2  2, 0, SNC
      ZONP
      JMP  OUPN
      MOV2  0, 0, JNR
      JMP  OONP
TONP:  MOV2  0, 1
      COM2  0, 2
      LDA  2, MSK2
      AND2  3, 1
      AND2  3, 2
      MOVR  1, 1
      MOVR  2, 2
      JEP  SEP64
      DSZ  CS
      JMP  FONP
      JMP  OTP
FONP:  LDA  0, IS
      JMP  OUPP
OONP:  STA  0, HS
      MOV2  0, 1
      NEG2  0, 2
      LDA  2, MSK1
      AND2  3, 1
      AND2  3, 2
      JEP  SP
      MOVR  1, 1
      MOVR  2, 2
      JEP  SEP64
      DSZ  CS
      JMP  SUPN
      JMP  OTP

```

```

OTF: JMF 000004
R004: 0

SUFN: LDA 0.15
      LDA 0.45
      ADD 0.0-ENR
      JMF 000004
      MOV 0.0-ENR
      JMF 000004
      NEG 0.0
      JMF 000004
      COM 0.1
      MIN 0.1
      LIA 0.1-ENR
      AND 0.1
      AND 0.1
      MOV 0.1
      MOV 0.1
      JMF 000004
      DEC 0.0
      JMF 000004
      JMF 000004

FUFN: LDA 0.15
      NEG 0.0
      JMF 000004
      STA 0.1-ENR
      MOV 0.1
      NEG 0.1
      LIA 0.1-ENR
      AND 0.1
      AND 0.1
      JMF 000004
      MOV 0.1
      MOV 0.1
      JMF 000004
      DEC 0.0
      JMF 000004
      JMF 000004

QUN: LDA 0.15
      NEG 0.1
      LIA 0.1-ENR
      AND 0.1
      AND 0.1
      JMF 000004
      MOV 0.1
      MOV 0.1
      JMF 000004
      DEC 0.0
      JMF 000004
      JMF 000004

EDN: LDA 0.15
      SUB 0.0-ENR
      JMF 000004
      NEG 0.0
      JMF 000004
      MOV 0.0-ENR
      JMF 000004
      COM 0.1
      LDA 0.1-ENR
      AND 0.1
      AND 0.1
      MOV 0.1
      JMF 000004
      DEC 0.0
      JMF 000004
      JMF 000004

F00N: LDA 0.15
      JMF 000004
      QUN: STA 0.1-ENR
      MOV 0.1
      NEG 0.1
      LDA 0.1-ENR
      AND 0.1
      AND 0.1
      JMF 000004
      MOV 0.1
      MOV 0.1
      JMF 000004
      DEC 0.0
      JMF 000004
      JMF 000004

SR: STA 0.1-ENR
      LDA 0.0-ENR
      STA 0.0-ENR
      MOV 0.1
      MOV 0.1
      DEC 0.0
      JMF 000004
      JMF 000004

CS 0
REP 0
END

```

		TITLE	PC4		
		ENT	SP44		
		EXTD	HD, IS, CS		
		EXTD	MSB1, MSB2, CSB, SP44		
		REFL			
		LOC	DOX		
SP44:	PC4				
		NREL			
PC4:	STA	1 SP44	SP44:	LDA	2, 15
	LDA	0, HS		LDA	0, HT
	JMR	TMR		NEGZ	0, 0
SUPP:	LDA	2, 15		SUBG	2, 0, SP44
	LDA	0, HS		JMR	SP44
	NEGZ	0, 0		NEGZ	0, 0
	ADDZ	2, 0, SP44		JMR	OPN
	JMR	CSB	SP44:	MOVZ	0, 0, SP44
	MOVZ	0, 0, SP44		JMR	OPN
	JMR	TMR	TMR:	MOVZ	0, 1
	NEGZ	0, 0		COMZ	0, 2
	JMR	OPN		LDA	2, MSB1
TUFF:	COMZ	0, 1		ANDZ	1, 1
	MOVZ	0, 1		ANDZ	1, 2
	LDA	2, MSB2		MOVOR	1, 1
	ADDZ	1, 1		MOVOR	1, 1
	ADDZ	1, 1		JST	SP44
	MOVOR	1, 1		SEZ	CS
	MOVOR	1, 1		JMR	OPN
	JST	SP44		JMR	OTR
	SEZ	CS	POINT:	LDA	0, 15
	JMR	OPN		NEGZ	0, 0
	JMR	OTR		JMR	OPN
PURF:	LDA	0, 15	QNF:	STA	0, HS
	JMR	OPN		MOVZ	0, 1
	STA	0, HS		NEGZ	0, 2
	NO, 0	0, 1		LDA	2, MSB1
	NEGZ	0, 2		ANDZ	1, 1
	LDA	2, MSB1		ANDZ	1, 2
	ANDZ	1, 1		JST	SP
	ANDZ	1, 2		MOVOR	1, 1
	JST	SP		MOVOR	1, 1
	MOVOR	1, 1		JST	SP44
	MOVOR	1, 1		SEZ	CS
	JST	SP44		JMR	OPN
	SEZ	CS		JMR	OTR
	JMR	OPN			
	JMR	OTR			

```

QTP:      JMP      @SF64
RF64:      0

SUPN:      LDA      2, 15
          LDA      0, H5
          NEGZ      0, 0
          ADDZ      2, 0, ENC
          JMP      OUPN
          MOVZ      0, 0, ENR
          JMP      TUPN
          NEGZ      0, 0
          JMP      OQNN

TUPN:      COMZ      0, 1
          MOVZ      0, 2
          LDA      3, MSK'2
          ANDZ      3, 1
          ANDZ      3, 2
          MOVOP      1, 1
          MOVOP      2, 2
          JSR      @SF64
          DSE      CS
          JMP      FUPN
          JMP      QTP

FUPN:      LDA      0, 15
          JMP      OUPN

OUPN:      STA      0, H5
          MOVZ      0, 1
          NEGZ      0, 2
          LDA      3, MSK'1
          ANDZ      3, 1
          ANDZ      3, 2
          JSR      SP
          MOVOP      1, 1
          MOVOP      2, 2
          JSR      @SF64
          DSE      CS
          JMP      EDNF
          JMP      QTP

EDNN:      LDA      2, 15
          LDA      0, H5
          NEGZ      0, 0
          SUBO      2, 0, ENC
          JMP      EDNN
          NEGZ      0, 0
          JMP      OUPF

ZDNN:      MOVZ      0, 0, SEP
          JMP      OQNN

TDNN:      MOVZ      0, 1
          COMZ      0, 2
          LDA      3, MSK'2
          ANDZ      3, 1
          ANDZ      3, 2
          MOVZF      1, 1
          MOVZF      2, 2
          JSR      @SF64
          DSE      CS
          JMP      FQNN
          LDA      0, 15
          NEGZ      0, 0
          JMP      OQNN

OQNN:      STA      0, H5
          MOVZ      0, 1
          NEGZ      0, 2
          LDA      3, MSK'1
          ANDZ      3, 1
          ANDZ      3, 2
          JSR      SP
          MOVOP      1, 1
          MOVOP      2, 2
          JSR      @SF64
          DSE      CS
          JMP      SUPN
          JMP      QTP

SF:      STA      3, ESP
          LDA      3, CSF
          STA      3, CS

R1:      MOVOP      1, 1
          MOVOP      2, 2
          DSE      CS
          JMP      R1
          JMP      @R3F

CS:      0
RSP:      0
END
-----
-----
-----

```

```

                                TITLE      I64
                                .ENT       $I64
                                .EXTD      HD, 13, 05
                                .EXTD      MS12, $F64
                                .FREL
                                .LOC       121

SI64:  I64
                                .NREFL
IT:     STA      1, $I64
TU#     LDA      0, HD
                                MOVE      0, 1
                                CUMC      0, 2
                                STA      0, H5
                                LDA      1, MS12
                                ANDC      1, 1
                                ANDC      1, 2
                                NOVER      1, 1
                                NOVER      2, 2
                                JF#       @F64
                                DEZ       .05
                                JMP       TUFF
                                J#F       QTF
OTF:    JMP      @RI64
RI64    0
END
-----
-----
-----

```

```

      .TITLE      H64
      .ENT        SH64
      .EXTD       HG. 15. 00
      .EXTD       H642 SH64
      .LREL       L61      124

SM64.  H64
      UNEL
H64.   STA      1. H644
TUFF  LDA      0. H6
      MOVE      0. 1
      COMP      0. 2
      STA      0. H6
      LDA      1. H642
      ANDC      1. 1
      ANDC      1. 2
      MONOP     1. 1
      MONOP     2. 2
      JSP       00P64
      DEC       . 00
      JNF       T6NF
      JMF       0TF
T6NF:  LDA      0. H6
      COMP      0. 1
      MOVE      0. 2
      STA      0. H6
      LDA      1. H642
      ANDC      1. 1
      ANDC      1. 2
      MONOP     1. 1
      MONOP     2. 2
      JSP       00P64
      DEC       . 00
      JNF       T6FN
      JMF       0TF
T6FN:  LDA      0. H6
      COMP      0. 1
      COMP      0. 2
      STA      0. H6
      LDA      1. H642
      ANDC      1. 1
      ANDC      1. 2
      MONOP     1. 1
      MONOP     2. 2
      JSP       00P64
      DEC       . 00
      JNF       T6NF
      JMF       0TF
T6NF:  LDA      0. H6
      COMP      0. 1
      MOVE      0. 2
      STA      0. H6
      LDA      1. H642
      ANDC      1. 1
      ANDC      1. 2
      MONOP     1. 1
      MONOP     2. 2
      JSP       00P64
      DEC       . 00
      JNF       TUFF
      JMF       0TF
O6P:   JMF      00P64
P664   0
END

```

```

      .TITL   .N64
      .ENV    SN64
      .EXTD   .H5, 10, C5
      .EXTD   H5N2 SP64
      .ZFEL
      .LOC    225

SN64:  N64
      N64:    STR      3, RN64
      TUFF:   LDA      0, H5
      MOVZ    0, 1
      COMZ    0, 2
      STR     0, H5
      LDA     3, MSK2
      ANDZ    3, 1
      ANDZ    3, 2
      MOVZ    1, 1
      MOVZ    2, 2
      JSR     @SP64
      DEZ     .C5
      JMF     TUFF
      JMF     OTP
      TUFF:   LDA      0, H5
      MOVZ    0, 1
      COMZ    0, 2
      STR     0, H5
      LDA     3, MSK2
      ANDZ    3, 1
      ANDZ    3, 2
      MOVZ    1, 1
      MOVZ    2, 2
      JSR     @SP64
      DEZ     .C5
      JMF     TUFF
      JMF     OTP

      OTP:    JMF      @RN64
      RN64:   @
      END
      ---
      ---
      ---

```

```

      .TITL   004
      .ENV    8064
      .EXTD   .AD. ID. CS
      .EXTD   MEM2.SP64
      .ESEL
      .LOC    026

8064: 004      .ESEL
004    STP     1.RO64
TURN:  LDA     0.45
      MOVZ    0.1
      COMZ    0.2
      STA     0.45
      LDA     1.MEM2
      ANDZ    1.1
      ANDZ    1.2
      MOVZF   1.1
      MOVZF   2.2
      JZF     @SP64
      DSE     CS
      JMP     TURN
      JMP     OTF
      LDA     0.45
      COMZ    0.1
      COMZ    0.2
      STA     0.45
      LDA     1.MEM2
      ANDZ    1.1
      ANDZ    1.2
      MOVZF   1.1
      MOVZF   2.2
      JZF     @SP64
      DSE     CS
      JMP     TURN
      JMP     OTF
      LDA     0.45
      COMZ    0.1
      COMZ    0.2
      STA     0.45
      LDA     1.MEM2
      ANDZ    1.1
      ANDZ    1.2
      MOVZF   1.1
      MOVZF   2.2
      JZF     @SP64
      DSE     CS
      JMP     TURN
      JMP     OTF

OTF:   JMP     @SP64
RO64   0
END

```

A4.6 Subprogram to Generate Starting and Incrementing Arguments for the S-G

There are nine subprograms numbered from Q41 to Q49, each program providing starting and incrementing arguments for each of the nine sets of columns of K_{nk} arguments. The subprogram is executed before a column of K_{nk} arguments is generated. The subprogram is initially entered through SP4X1 ($X = 1, \dots, 9$) and subsequently entered through SP4X2 for the remaining starting and incrementing arguments. The auto incrementing address locations of the Accumulators, which are needed by the TLUAR, are also set up by the subprogram. Subprogram Q41 is only explained as the remaining subprograms are similar.

P411:	STA	3,RP41	Save return to MCN
	LDA	1,SH1	Set first start arg. (calculated by CCL).
	LDA	2,SI	Get first inc. arg. (calculated by CCL).
	JMP	P410	Go to statement P410.
P412:	STA	3,RP41	Save return to MCN
	LDA	1,.SH1	Get current start arg.
	LDA	3,IH1)	Generate next current start arg.
	ADDZ	3,1)	
	LDA	2,.SI1	Get current inc. arg.
	LDA	0,II1)	Generate next current inc. arg.
	ADDZ	0,2)	

P410 :	STA	1,.SHI	store current start arg.
	STA	2,.SII	store current inc. arg.
	STA	1,.H5	pass current start arg. to SAG
	STA	2,.I5	pass current inc. arg. to SAG.
	LDA	1,SA1	These instructions set
	STA	1,20	the auto. inc. address
	STA	1,21	Locations of the Accumulators
	LDA	1,CA1	which will be used by
	STA	1,22	the TLUAR.
	STA	1,23	
	LDA	1,CT1	Pass the number of
	STA	1,.C5	K_{nk} arg. that must be generated
			to the SAG.
	JMP	@RP41	Return to MCN.
.SH1 Current starting arg. scratch pad memory.			
.SII Current inc arg. scratch pad memory.			
RP41 Location of return address.			

```

                                TITL      Q41
                                .ENT      SF411, SF412
                                .EXTD     HQ, IS, CS
                                .EXTD     SH1, IM1, S11, I11, CT1, SA1, CA1
                                .EXEL
                                .LOC      223

SF411:  P411
SF412:  P412

                                TITL      Q42
                                .ENT      SF421, SF422
                                .EXTD     HQ, IS, CS
                                .EXTD     SH2, IM2, I12, I12
                                .EXEL     242, SA2, CA2
                                .LOC      224

P411:   STA      1, PP41
        LDA      1, SH1
        LDA      2, S11
        JMP      P420

P412:   STA      3, PP41
        LDA      1, SH1
        LDA      3, IM1
        ADDC     3, 1
        LDA      2, S11
        LDA      0, I11
        ADDC     0, 1

P413:   STA      1, SH1
        STA      2, S11
        STA      1, H3
        STA      2, I5

        LDA      1, SA1
        STA      1, 10
        STA      1, 21
        LDA      1, CA1
        STA      1, 22
        STA      1, 22

        LDA      1, CT1
        STA      1, CS

        JMP      QFF41

. SH1:  0
. S11:  0
PP41:   0
END

                                TITL      Q43
                                .ENT      SF431, SF432
                                .EXTD     HQ, IS, CS
                                .EXTD     SH3, IM3, I13, I13
                                .EXEL
                                .LOC      225

P421:   STA      3, PP42
        LDA      1, SH2
        LDA      3, IM2
        ADDC     3, 1
        LDA      2, S12
        LDA      0, I12
        ADDC     0, 2

P422:   STA      1, SH2
        STA      2, S12
        STA      1, H3
        STA      2, I5

        LDA      1, SA2
        STA      1, 20
        STA      1, 21
        LDA      1, CA2
        STA      1, 22
        STA      1, 23

        LDA      1, CT2
        STA      1, CS

        JMP      QFF42

. SH2:  0
. S12:  0
PP42:   0
END

```

```

-----
                                .TITLE  P43
                                .ENT    SP431, SP432
                                .EXTD    140, 15, 05
                                .EXTD    SP43, 140, S14, S15, S16, S17, S18, S19, S20
                                .FSEL    LOC
                                220

SP431:  P431
SP432:  P432

                                .TITLE  P44
                                .ENT    SP441, SP442
                                .EXTD    147, 17, 05
                                .EXTD    SP44, 147, S14, S15, S16, S17, S18, S19, S20
                                .FSEL    LOC
                                230

P431:   STA  1, SP43
        LDA  1, S40
        LDA  1, S15
        JMP  P430

P432:   STA  1, SP43
        LDA  1, S40
        LDA  1, S15
        ADD  0.1
        LDA  1, S15
        LDA  0, S15
        ADD  0.2

P433:   STA  1, S40
        STA  1, S15
        STA  1, S15
        STA  1, S15
        LDA  1, S40
        STA  1, S15
        STA  1, S15
        STA  1, S15
        STA  1, S15
        LDA  1, S40
        STA  1, S15
        JMP  SP441

S40:    0
S15:    0
SP43:    0
END

                                .TITLE  P441
                                .ENT    SP441, SP442
                                .EXTD    147, 17, 05
                                .EXTD    SP44, 147, S14, S15, S16, S17, S18, S19, S20
                                .FSEL    LOC
                                230

P441:   STA  1, SP44
        LDA  1, S40
        LDA  1, S14
        JMP  P440

P442:   STA  1, SP44
        LDA  1, S40
        LDA  1, S14
        ADD  0.1
        LDA  1, S14
        LDA  0, S14
        ADD  0.2

P443:   STA  1, S40
        STA  1, S14
        STA  1, S15
        STA  1, S15
        LDA  1, S40
        STA  1, S14
        STA  1, S15
        STA  1, S15
        LDA  1, S40
        STA  1, S14
        STA  1, S15
        STA  1, S15
        LDA  1, S40
        STA  1, S14
        STA  1, S15
        STA  1, S15
        JMP  SP441

S40:    0
S14:    0
SP44:    0
END

```

```

TITL      045
ENT       SP451, SP452
EXTD      HS, IS, CS
EXTD      SH5, IH5, S15, I15, CT2, SA2, CA2
ZFEL
LOC       234

```

```

SP451:    P451
SP452:    P452

```

```

P451:     STA     3, PP45
          LDA     1, SH5
          LDA     2, S15
          JMP     P450

```

```

P452:     STA     3, PP45
          LDA     1, SH5
          LDA     2, IH5
          ADDZ    2, 1
          LDA     2, S15
          LDA     0, I15
          ADDZ    0, 2

```

```

P453:     STA     1, SH5
          STA     2, S15
          STA     1, HS
          STA     2, IS
          LDA     1, SP2
          STA     1, 20
          STA     1, 21
          LDA     1, CA2
          STA     1, 22
          STA     1, 23
          LDA     1, CT2
          STA     1, CS

```

```

          JMP     @PP45
          .SH5    0
          .S15    0
          .PP45   0
          .END

```

```

TITL      045
ENT       SP451, SP452
EXTD      HS, IS, CS
EXTD      SH5, IH5, S15, I15, CT2, CA2, SA2
ZFEL
LOC       232

```

```

SP451:    P451
SP452:    P452

```

```

P451:     STA     3, PP45
          LDA     1, SH5
          LDA     2, S15
          JMP     P450

```

```

P452:     STA     3, PP45
          LDA     1, SH5
          LDA     2, IH5
          ADDZ    2, 1
          LDA     2, S15
          LDA     0, I15
          ADDZ    0, 2

```

```

P453:     STA     1, SH5
          STA     2, S15
          STA     1, HS
          STA     2, IS

```

```

          LDA     1, SP2
          STA     1, 20
          STA     1, 21
          LDA     1, CA2
          STA     1, 22
          STA     1, 23

```

```

          LDA     1, CT2
          STA     1, CS

```

```

          JMP     @PP45

```

```

          .SH5    0
          .S15    0
          .PP45   0
          .END

```

```

      .TITL      .O43
      .ENT       SP421, SP432, SP461
      .EXTD      HD, ID, CS
      .EXTD      SH2, IH2, SI2, I12, CT2, SA2, CA2
      .ZFEL
      .LOC       240

SP451:  P451
SF452:  P452
SP461:  P461

      .NFEL
P451:   STA     1, PF45
      LDA     1, SH2
      LDA     2, SI2
      JMF     P450

P452:   STA     1, PF45
      LDA     1, SH2
      LDA     2, IH2
      SUEO
      JMF     P454

P452:   STA     1, PF45
      LDA     1, SH2
      LDA     2, IH2
      ADDC
      LDA     2, SI2
      LDA     0, I12
      ADDC
      LDA     0, I12
      ADDC
      STA     1, SH2
      STA     2, SI2
      STA     1, HS
      STA     2, I12

      LDA     1, SA2
      STA     1, 20
      STA     1, 21
      LDA     1, CA2
      STA     1, 22
      STA     1, 23

      LDA     1, CT2
      STA     1, CS
      JMF     SP445

      .SH2:  0
      .SI2:  0
      .PF45: 0
      .END
      .
      .
      .

      .TITL      .O47
      .ENT       SP471, SP472
      .EXTD      HD, ID, CS
      .EXTD      SH7, IH7, SI7, I17, CT7
      .ZFEL
      .LOC       216

SP471:  P471
SF472:  P472

      .NFEL
P471:   STA     1, PF47
      LDA     1, SH7
      LDA     2, SI7
      JMF     P470

P472:   STA     1, PF47
      LDA     1, SH7
      LDA     2, IH7
      ADDC
      LDA     2, SI7
      LDA     0, I17
      ADDC
      STA     1, SH7
      STA     2, SI7
      STA     1, HS
      STA     2, I15

      LDA     1, SA1
      STA     1, 20
      STA     1, 21
      LDA     1, CA1
      STA     1, 22
      STA     1, 23

      LDA     1, CT1
      STA     1, CS
      JMF     SP447

      .SH7:  0
      .SI7:  0
      .IH7:  0
      .END
      .
      .
      .

```

```

      .TITL      049
      .EXT      SP491,SP492
      .EXTD     HQ, 10, CS
      .EXTD     SP4 1M3 113 112 CYS EAS,CAS
      .NREL
      .LOC      140

SP491.  F491
SP492.  F492

      .NREL

F491.   STA      1. SP49
      LDA      1. SP4
      LDA      2. S19
      JMP      F490

F492.   STA      1. SP49
      LDA      1. SP4
      LDA      1. 1M3
      ADDC     1. 1
      LDA      2. S19
      LDA      0. 115
      ADDC     0. 2

F490.   STA      1. SP4
      STA      2. S19
      STA      1. HQ
      STA      2. 15

      LDA      1. EAC
      STA      1. 20
      STA      1. 21
      LDA      1. CAS
      STA      1. 22
      STA      1. 21

      LDA      1. CYS
      STA      1. CS

      JMP      GRR43

      SHP.      0
      S19.      0
      SP49.     0
      .END
      -----

```

A4.7 The Table Look Up and Accumulate Routine TLUAR

The subprogram is called by the SAG subprogram to process the sine and cosine K_{nk} values. After the TLUAR has performed its tasks, detailed in A3.10, control is returned to the SAG subprogram.

The TLUAR consists of the following subroutines.

- 1) CINT/SINT
- 2) GY1/GY2
- 3) PACC/NACC

as well as the main routine.

In A3.10.2 the STV address is simply calculated by adding the two components of the address pair I_n and K_{nk} and the address of the first location in the STV. Subroutine SINT performs the first part of this addition by adding the address of the first location in the STV to the sine K_{nk} (argument) value. CINT adds the cosine K_{nk} to the address of the first location in the STV. This partial sum is termed the base address (BTU). GY1/GY2 adds the LADC output to the base address to form the final STV address (see A3.10.4). PACC/NACC adds/subtracts the STV constant to/from the required Accumulator.

The main routine consists of six parts, each part corresponding to entry points described in A4.6. (ie part is associated with a sign pattern in Fig.A3.5).

The main routine performs the following tasks.

- 1) Store the return address of the SAG.
- 2) Calls SINT

- 3) Stores the contents of the particular Accumulator being processed in a temporary location.
- 4) Calls GY1/GY2 in the required order and increments or decrements the contents of the temporary location according to the value of the signum function
- 5) Returns the contents of the temporary location to the Accumulator.

These steps are then repeated for the cosine K_{nk} values.

A4.7.1 Subroutine SINT

SINT: STA	3,RINT	Save main routine return address
STA	1,SC	Store sine K_{nk} in scratch pad.
STA	2,CC	Store cosine K_{nk} in scratch pad
LDA	3,SB6)	Set auto inc. address for SB.
STA	3,24)	
LDA	3,TLU	Get address of first location of STV
LDA	1,SC	Get sine K_{nk} from scratch pad
ADDZ	3,1	Add sine K_{nk} address to first location address of STV to obtain base address
STA	1,BTLU	Store base address
JMP	@RINT	Return to main routine

A4.7.2 Subroutine CINT

This is similar to SINT but sets up the base address for the cosine K_{nk} .

A4.7.3 Subroutine CINT2 and SINT2

These are similar to CINT and SINT and are used for the special case in P37.

A4.7.4 Subroutines GY1 and GY2

These subroutines generate the signum function and modify it for the 'opposite signs' case.

GY1:	STA	3, RGY	Save return to main routine
	STA	0, TAC	Store Accumulator contents in temporary location
	LDA	3, @24	Get the next shuffled I_n value from SB
	LDA	1, BTLU	Get base address of STV
	ADDZL	1, 3, SNC	Calculate final STV address and check sign bit
	JMP	PACC	If sign bit is positive go to incrementing subroutine
	JMP	NACC	If sign bit is negative go to decrementing routine

GY2 has the last two instructions swapped

ie.	ADDZL	1, 2, SNC	
	JMP	NACC	If sign bit is positive go to decrementing routine
	JMP	PACC	If sign bit is negative go to incrementing routine.

Register 3 contains the STV address and the signum function sign bit which have been shifted one place to the left so as to check the sign bit. PACC and NACC must first restore this address by shifting it one place to the right and destroying the sign bit as it has served its purpose.

A4.7.5 Subroutines PACC and NACC

These subroutines perform the following tasks

- 1) Restore the final STV address
- 2) Check the sign bits of the STV constant and Accumulator contents to check for overflow (OVF) underflow (UNF)
- 3) Add or subtract the STV constant to or from the Accumulator value
- 4) Write an error message if OVF/UNF occurs

PACC: MOVZR	3,3	Restore STV address and eliminate the sign bit.
LDA	1,0,3	Get the STV constants and load them into reg. 1.
STA	1,T1D	Load STV constants into a temporary location
LDA	2,MSK	Get mask that will extract sign bits of STV constant and Accumulator value
LDA	0,TAC	Get Accumulator value which is stored in a temporary location.
AND	2,0	Get Accumulator sign bit
AND	2,1	Get STV sign bit

MOV	1,2	}	Exclusive OR of sign bits
ANDZL	0,2		
ADD	0,1		
SUB	2,1, SZR		

JMP	PACN	sign bits are different
		There is no risk of OVF/UNF
MOVZL#	0,0, SZC	The sign bits are the same. Check the Accumulator sign bit
JMP	PACU	Accumulator sign bit negative.
		UNF <u>could</u> take place.
JMP	PACO	Accumulator sign bit positive OVF <u>could</u> take place

PACU is a subroutine that adds TID (STV constant) to TAC (Accumulator value) and checks for underflow. PACO is a subroutine adds TID to TAC and checks for overflow. PACN adds TID to TAC and does not check for overflow or underflow as neither will occur in this case.

PACN:	LDA	2,TID	Get STV constant
	LDA	0,TAC	Get Accumulator value
	ADDZ	2,0	Add
	JMP	@RCY	Return to main routine
PACO:	LDA	2,TID	
	LDA	0,TAC	
	ADDZL	2,0, SZC	Add, Shift left and check CARRY bit.
			If zero, no OVF and skip next instruction

JMP	OVFP	OVF. Go to error flag routine.
MC/R	0,0	Restore result
JMP	@RGY	
PACU: LDA	2,TID	
LDA	0,TAC	
ADDZL	2,0,SNC	Add. Shift left and check CARRY
		bit. If one (negative result), no
		UNF and skip next instruction
JMP	UNFP	UNF. Go to error flag routine
MOVR	0,0	Restore result
JMP	@RGY	

The NACC subroutine is similar to the PACC subroutines but subtraction instead of addition takes place. The sign bits of the Accumulator and the STV constant are also exclusively ORed and the subroutine chooses one of three subtraction routines NACN (no OVF/UNF check necessary), NACD (check OVF) and NACU (check underflow) to decrement the Accumulator.

A4.7.6 The Main Routine

The main routine has to entry points P61, P62, P63, P64, P611 and P612, one for each of the 6 sign patterns in Fig.A3.5. Consider the routine for the set OTS/OH.

P61: STA	3,RP6	Save the SAG return
JSR	SINT	See A4.7.1

LDA	Q@20	Get the contents of the Accumulator that has its address set in Q41 and load them into reg 0. The second statement in GY1/GY2 stores the contents of reg 0 in a temporary location.
JSR	GY1)	This is equivalent to the sign pattern associated with the set OTS/OH.
JSR	GY1)	
JSR	GY2)	
JSR	GY2)	
STA	O,@21	Reg. 0 contains the incremented or decremented Accumulator value. The contents of reg. 0 are returned to the Accumulator block.

The cosine main routine follows a similar pattern.

JSR	CINT	
LOA	O,@22	Get Accumulator value
JSR	GY1)	sign pattern for cosine OTS/OH.
JSR	GY2)	
JSR	GY2)	
JSR	GY1)	
STA	O,@23	Return the incremented or decremented Accumulator value to the Accumulator block
JMP	@RP6	Return to SAG

P63:	STA	3, RPS	SINT:	STA	3, RINT
	JSR	SINT		STA	1, SC
	LDA	0, 020		STA	2, CC
	JSR	GV1		LDA	3, SE6
	JSR	GV2		STA	3, 24
	JSR	GV1		LDA	3, TLU
	JSP	GV2		LDA	1, SC
	STA	0, 021		ADDE	3, 1
				STA	1, BTLU
	JSE	CINT		JMP	0RINT
	LDA	0, 022	CINT:	STA	3, RINT
	JSR	GV1		LDA	3, SE6
	JSR	GV2		STA	3, 24
	JSR	GV1		LDA	3, TLU
	JSP	GV2		LDA	1, CC
	STA	0, 021		ADDE	3, 1
				STA	1, BTLU
	JMP	0RPS		JMP	0RINT
P64:	STA	3, FPS	SINT2:	STA	3, RINT
	JSR	SINT		STA	1, SC
	LDA	0, 020		STA	2, CC
	JSR	GV1		LDA	3, SE6
	JSR	GV1		INC	3, 1
	JSR	GV1		STA	3, 24
	JSP	GV1		LDA	3, TLU
	STA	0, 021		LDA	1, SC
				ADDE	3, 1
	JSE	CINT		STA	1, BTLU
	LDA	0, 022		JMP	0RINT
	JSR	GV1	CINT2:	STA	3, RINT
	JSR	GV1		LDA	3, SE6
	JSP	GV1		INC	3, 1
	STA	0, 021		STA	3, 24
				LDA	3, TLU
	JMP	0RPS		LDA	1, CC
				ADDE	3, 1
				STA	1, BTLU
				JMP	0RINT
GV1:	STA	3, RGV	FACC:	MOVPS	3, 1
	STA	0, TAC		LDA	1, 0, 1
	LDA	3, 024		STA	1, YID
	LDA	1, BTLU		LDA	2, MSK
	ADDECL	1, 1, SMC		LDA	0, TAC
	JMP	FACC		AND	2, 0
	JMP	MACC		AND	2, 1
				MOV	1, 2
				ANDCL	0, 2
				ADD	0, 1
				SUB	2, 1, SSK
GV2:	STA	3, RGV		JMP	FACN
	STA	0, TAC		MOVCL4	0, 0, SSC
	LDA	3, 024		JMP	FACU
	LDA	1, BTLU		JMP	FACU
	ADDECL	1, 1, SMC			
	JMP	FACC			
	JMP	FACC			

```

NACC:  MOV#  2/0
      LDA  1/0.1
      STA  1/TID
      LDA  2/NS
      LDA  0/TAC
      AND  2/0
      AND  2/1

      MOV#  1/2
      ANDCL 0/2
      ADD  0/1
      SUB  2/1, ENF

      JNF  NACH
      MOV#  0/0, EDC
      JNF  NACU
      JNF  NACC

FACH:  LDA  2/TID
      LDA  0/TAC
      ADD  2/0
      JNF  GRGV

FACU:  LDA  2/YID
      LDA  0/TAC
      ADDCL 2/0, EDC
      JNF  OVER
      MOV#  0/0
      JNF  GRGV

PACU:  LDA  2/YID
      LDA  0/TAC
      ADDCL 2/0, ENF
      JNF  UNFF
      MOV#  0/0
      JNF  GRGV

NACH:  LDA  2/YID
      LDA  0/TAC
      SUB  2/0
      JNF  GRGV

NACC:  LDA  2/TID
      LDA  0/TAC
      SUB  2/0, EDC
      JNF  OVER
      MOV#  0/0
      JNF  GRGV

NACU:  LDA  2/TID
      LDA  0/TAC
      SUB  2/0, ENF
      JNF  UNFF
      MOV#  0/0
      JNF  GRGV

SC:  0
CC:  0
TAC:  0
TID:  0
BTLU:  0
MSK:  100000
RGV:  0
RINT:  0
OVER:  LDA  1/A1
      JSR  0B0
      JNF  00A
      JNF  1/A2
      JSR  0B0
      JNF  00A
      JNF  1/A3
      JSR  0B0
      JNF  00A
      JNF  1/A4
      JSR  0B0
      JNF  00A
      LDA  1/20
      JSR  0B0
      LDA  1/21
      JSR  0B0
      LDA  1/22
      JSR  0B0
      LDA  1/23
      JSR  0B0
      JNF  0BTLU

ED:  0B00
A1:  7
A2:  115
A3:  1411
A4:  17141
      END

```

A4.8 The CCL Subroutine

This subroutine calculates all the constants for the DFTTLU for a given value of N (ie. $N = 128, 256, 512, 1024$) and will stop if N is not one of these values. The subprogram calculates the numbers of columns of K_{nk} values that fall into each of the four cases. These numbers are listed as C16, C161, C32, C321, C64 and C641. It then calculates the numbers of K_{nk} values in a column which are listed as CT1, CT2 and CT3. MB0, MB1 ... MB21 contain the first group of addresses of the shuffled time samples. These addresses are needed by the Shuffling Subprogram. The subprogram calculates the first set of starting and incrementing arguments required by the Q41 - Q49 subprograms ie SH1, S11, IH1, 111 ... II9.

COAL:	STA	1, RF11		MOVCL	1, 1		LDA	1, ME
	LDA	1, N		LDA	2, N2		LDA	0, ISF
			A2:	STA	2, N2		ADDC	0, 1
	LDA	2, M1		STA	1, 020		STA	1, NEW
	ANDZ	1, 2, SZR		OSZ	N2		JSR	FI10
	JMP	+2		JMP	A2		OSZ	N2
	JMP	A128					JSR	FI10
	JSP	0SF6		MOVCL	1, 1			
	LDA	2, M2	A3:	LDA	2, N2		LDA	1, ME15
	ANDZ	1, 2, SZR		STA	2, N2		INC	1, 1
	JMP	+2		STA	1, 020		STA	1, MS21
	JMP	A256		OSZ	N2		JMP	0SF11
				JMP	A2			
	JSP	0SF6		MOVCL	1, 1	P110:	STA	1, RF110
	LDA	2, M2		LDA	2, M4		LDA	2, M4
	ANDZ	1, 2, SZR	A4:	STA	2, M4		STA	2, M4
	JMP	+2		STA	1, 020		LDA	1, ME1
	JMP	A512		OSZ	N4		LDA	0, ISF
				JMP	A4		JMP	FI11
	JSP	0SF6		LDA	1, N	P112:	ADDC	0, 1
	LDA	2, M4		MOVWF	1, 1	P111:	STA	1, 020
	ANDZ	1, 2, SZR		MOVWF	1, 1		OSZ	N4
	JMP	+2		STA	1, CT1		JMP	FI12
	JMP	A1024		STA	1, ISF		JMP	0SF116
				MOVWF	1, 1	M1:	177577	
	LDA	2, M5		STA	1, CT2	M2:	177577	
	ANDZ	1, 2, SZR		STA	1, CT2	M3:	176577	
	HALT			MOVWF	1, 1	M4:	176577	
	JMP	A2048		STA	1, CT2	M5:	176577	
				STA	1, CT2	M6:	176577	
A128:	LDA	1, N4		STA	1, CT2	M7:	176577	
	JMP	SRI		OSZ	C151	M8:	4	
				MOVWF	1, 1	M9:	5	
A256:	LDA	1, N5		STA	1, CT2	M10:	6	
	JMP	SRI		STA	1, CT2	M11:	7	
				OSZ	C121	M12:	10	
A512:	LDA	1, N6		MOVWF	1, 1	DNZ	0	
	JMP	SRI		STA	1, CT4	N2	0	
				STA	1, CT4	N4	0	
				OSZ	C841	N5	0	
A1024:	LDA	1, N7				ISF	0	
	JMP	SRI		LDA	1, CT1	RF110:	0	
				LDA	2, CT2	ME7:	0	
A2048:	LDA	1, N8		LDA	1, CT2	SE6:	STA	3, SET
	JMP	SRI		ADDC	1, 2		LDA	2, TBI
				ADDC	2, 2		MOVWF	2, 3
SRI:	STA	1, DN2		STA	3, M4		STA	3, TBI
	LDA	1, T19					JMP	0SET
	MOVWF	1, 1		LDA	1, ME1	FEY	END	
.SRI:	MOVWF	1, 1		STA	2, 20	----		
	OSZ	DN2				----		
	JMP	SRI		LDA	1, ME	----		
	STA	1, SH1		STA	1, ME1	----		
	LDA	2, T15H		LDA	1, N2			
	STA	2, 20		STA	1, N2			
	LDA	1, SH1	B:	LDA	1, ME1			
	MOVCL	1, 1		INC	1, 1			
	LDA	2, M4		STA	1, ME1			
	STA	2, M4		JSP	FI10			
A1:	STA	1, 020		OSZ	N2			
	OSZ	N4		JSP	E			
	JMP	A1						

A4.9 Calculation of the Resultant Harmonics

Fig.A3.17 shows the format of the Accumulator block in the core. This subprogram extracts the corresponding real and imaginary components in the correct sequences, calculates the resultant and divides it by 7 (see 4.4). Data General Software⁴ is used to perform the multiplication, double word addition and division. Reference 18 gives a routine that computes the square root of a double word. The resulting harmonics are used by the error analysis described in A5. This subprogram is also used to compute the resultant harmonics of the FFT routine used in the error analysis.

Subroutine STR extracts the harmonic components in the correct order ie E4H, OH, E4H,OH ... and subroutine PTG calculates

the resultant, divides it by 7, and stores it in block RB. The resultant harmonics in RB are in the correct sequence and are readily available for analysis by the error program.

LDA	1,SA1	
STA	1,20	The addresses of the first
LDA	1,CA1	locations in the
STA	1,21	Accumulator blocks are
LDA	1,SA2	loaded into the auto-
STA	1,22	incrementing address
LDA	1,CA2	locations
STA	1,23	
LDA	1,SA3	
STA	1,24	
LDA	1,CA3	
STA	1,25	
LDA	1,RB	
STA	1,26	
LDA	1,NH	The index i set up.
STA	1,NH	NH is the number of harmonics
		that will be processed.
		NH is decremented by one as each
		resultant harmonic is processed.
		When NH is zero control is returned
		to MCN.

JSR	@CPB	This instruction is included if the harmonics are being plotted. CPB positions the zero at $(X,Y) = (-1000_8, -1000_8)$ and makes a small vertical mark.
STR: LDA	1,@24	Get imaginary E4 component
LDA	2,@25	Get real E4 component
JSR	PTG	Go to resultant calculating routine
LDA	1,@20	Get imaginary odd numbered component
LDA	2,@21	Get real odd numbered component
JSR	PTG	
LDA	1,@22	Get imaginary E4 component.
LDA	2,@23	Get real E4 component
JSR	PTG	
LDA	1,@20	Get imaginary odd-numbered component
LDA	2,@21	Get real odd numbered component
JSR	PTG	
JMP	STR	

NH is decremented and tested for zero in PTG. The resultant is calculated using the Pythagorus Theorem. The squaring of the component is carried out by subroutine MPY, the addition by DADD and the square root, DSQR. The result of MPY is a double word, the high order bits are stored in reg. 0 and the low order in reg. 1.

PTG: STA 3,RPTG	Save return to STR.
STA 2,TC	store the real component in a temporary location.
MOV 1,2	Duplicate the imaginary component. in reg. 2
JSR @MPY	Square imaginary component
STA 0,HS	Store high order bits in HS.
STA 1,LS	Store low order bits in LS.
LDA 1,TC	Get real component from temporary location.
LDA 2,TC	Luplicate real component in reg 2.
JSR @MPY	Square real component.
JSR @DADD	Add squared real and imaginary component.
AHS: HS	This statement gives the location of the squared imaginary components to DADD
LDA 3,CKK	The double word sum must be less than 2^{29} . If greater than 2^{29} , the square root of the double word sum will cause a 2^{16} 's complement 16 bit word to overflow. If the double word is greater than 2^{29} , control is given to subroutine OSQR which prints an error message '66' and then gives control to subroutine STLU. (A4.12)
AND 0,3,SZR	
JMP OSQR.	

JSR	@DSQR	Take the square root of the double word sum.
LDA	2,C17	Load 7 into divisor register
JSR	@DIVI	Divide square root result by 7.
STA	1,@26	Store the answer in RB.

If the result is to be plotted, the following 2 instructions are included.

JSR	@SRTB	) See A4.13
JSR	@DOR	
DSZ	.NH	Decrement NH by one and test for zero.
JMP	@RPTG	NH not zero. Return to STR for next harmonic.
JSR	@CPE	NH is zero. This statement is included if the results are plotted.
		The pen in positions at (X,Y) = (0, -1000 _g) and makes a small vertical mark.
JMP	@RP75	Return to MCN.

		TITLE	PTG:	STA	3. RPTG
		1. RPTG			
		2. RPTG			
		3. RPTG			
		4. RPTG			
		5. RPTG			
		6. RPTG			
		7. RPTG			
		8. RPTG			
		9. RPTG			
		10. RPTG			
		11. RPTG			
		12. RPTG			
		13. RPTG			
		14. RPTG			
		15. RPTG			
		16. RPTG			
		17. RPTG			
		18. RPTG			
		19. RPTG			
		20. RPTG			
		21. RPTG			
		22. RPTG			
		23. RPTG			
		24. RPTG			
		25. RPTG			
		26. RPTG			
		27. RPTG			
		28. RPTG			
		29. RPTG			
		30. RPTG			
		31. RPTG			
		32. RPTG			
		33. RPTG			
		34. RPTG			
		35. RPTG			
		36. RPTG			
		37. RPTG			
		38. RPTG			
		39. RPTG			
		40. RPTG			
		41. RPTG			
		42. RPTG			
		43. RPTG			
		44. RPTG			
		45. RPTG			
		46. RPTG			
		47. RPTG			
		48. RPTG			
		49. RPTG			
		50. RPTG			
		51. RPTG			
		52. RPTG			
		53. RPTG			
		54. RPTG			
		55. RPTG			
		56. RPTG			
		57. RPTG			
		58. RPTG			
		59. RPTG			
		60. RPTG			
		61. RPTG			
		62. RPTG			
		63. RPTG			
		64. RPTG			
		65. RPTG			
		66. RPTG			
		67. RPTG			
		68. RPTG			
		69. RPTG			
		70. RPTG			
		71. RPTG			
		72. RPTG			
		73. RPTG			
		74. RPTG			
		75. RPTG			
		76. RPTG			
		77. RPTG			
		78. RPTG			
		79. RPTG			
		80. RPTG			
		81. RPTG			
		82. RPTG			
		83. RPTG			
		84. RPTG			
		85. RPTG			
		86. RPTG			
		87. RPTG			
		88. RPTG			
		89. RPTG			
		90. RPTG			
		91. RPTG			
		92. RPTG			</

[illegible]

A4.10 The Data Blocks

The data blocks are required to store the large number of values in consecutive locations. These values can be easily addressed using the auto incrementing address facility. To save core, certain areas of core are overwritten with new data, eg. the I1 block associated with the FFT is also used for the DFTTLU accumulators.

MB: N time samples - output of LADC.

RI: N time samples - output of ADC.

I1: N imaginary time samples - set to zero.

The results of the FFT are loaded in RI and I1.

RI: N Real FFT harmonic components

I1: N Imaginary FFT harmonic components.

SA1: $\frac{N}{4}$ Imaginary FFT harmonic components

SA1: $\frac{N}{4}$ Imaginary odd numbered DFTTLU harmonic components.

CA1: $\frac{N}{4}$ Real odd numbered DFTTLU harmonic components.

SA2: $\frac{N}{8}$ Imaginary even numbered (not multiples of 4) DFTTLU harmonic components.

CA2: $\frac{N}{8}$ Real even numbered (not multiples of 4) DFTTLU harmonic components.

SA3: $\frac{N}{8}$ Imaginary remaining even numbered DFTTLU harmonic components.

CA3: $\frac{N}{8}$ Real remaining even numbered DFTTLU harmonic components.

RB: $\frac{N}{2}$ Resultant DFTTLU harmonics.

SB: Current shuffled I_n values.

		TIME	FILE
		DAY	NO.
1	1	1	1
2	2	2	2
3	3	3	3
4	4	4	4
5	5	5	5
6	6	6	6
7	7	7	7
8	8	8	8
9	9	9	9
10	10	10	10
11	11	11	11
12	12	12	12
13	13	13	13
14	14	14	14
15	15	15	15
16	16	16	16
17	17	17	17
18	18	18	18
19	19	19	19
20	20	20	20
21	21	21	21
22	22	22	22
23	23	23	23
24	24	24	24
25	25	25	25
26	26	26	26
27	27	27	27
28	28	28	28
29	29	29	29
30	30	30	30
31	31	31	31
32	32	32	32
33	33	33	33
34	34	34	34
35	35	35	35
36	36	36	36
37	37	37	37
38	38	38	38
39	39	39	39
40	40	40	40
41	41	41	41
42	42	42	42
43	43	43	43
44	44	44	44
45	45	45	45
46	46	46	46
47	47	47	47
48	48	48	48
49	49	49	49
50	50	50	50
51	51	51	51
52	52	52	52
53	53	53	53
54	54	54	54
55	55	55	55
56	56	56	56
57	57	57	57
58	58	58	58
59	59	59	59
60	60	60	60
61	61	61	61
62	62	62	62
63	63	63	63
64	64	64	64
65	65	65	65
66	66	66	66
67	67	67	67
68	68	68	68
69	69	69	69
70	70	70	70
71	71	71	71
72	72	72	72
73	73	73	73
74	74	74	74
75	75	75	75
76	76	76	76
77	77	77	77
78	78	78	78
79	79	79	79
80	80	80	80
81	81	81	81
82	82	82	82
83	83	83	83
84	84	84	84
85	85	85	85
86	86	86	86
87	87	87	87
88	88	88	88
89	89	89	89
90	90	90	90
91	91	91	91
92	92	92	92
93	93	93	93
94	94	94	94
95	95	95	95
96	96	96	96
97	97	97	97
98	98	98	98
99	99	99	99
100	100	100	100

A4.11 The Main Control Program MCN

The main control program calls the subprograms in the required order. The program first resets the Accumulators by loading zero into the Accumulator. It then calls the sampling subprogram.

```
JSR  @SP21      Zero Accumulators
JSR  @SP25      Sample outputs of LADC and (ADC)
```

The first column in each of the nine sets of columns is solved separately as some of the subprograms are entered at a special point (eg. SP3 X 1, SP4 X 1). The subprogram associated with the OTS/OH is explained.

```
Q1.1: JSR  @SP311      Shuffle time samples.
      JSR  @SP411      Get starting and incrementing
                        arguments.
      JSR  @SA61      Generate first column of  $K_{nk}$  values.
      LDA  1,C161  }
      STA  1,CCNT  } Set up the index for the remaining
                        columns in case 1 ( $0 < inc < \frac{N}{2}$ )
Q1.2: JSR  @SP312      Get next group of shuffled time
                        samples
      JSR  @SP412      Get next starting and incrementing
                        arguments
      JSR  @SA61      Generate next column of  $K_{nk}$  addresses
      DSZ  CCNT      } Repeat for all the columns in case 1
      JMP  Q1.2      }
```

The following 3 cases are treated similarly and the pattern is repeated for the remaining eight sets of columns.

A4.12 The Run Program

This program links the DFTTLU and the FFT programs so that an analysis of the differences between the two methods can be made.

The Run program performs the following tasks.

- 1) Sets the number of bits representing a constant in the STV (see 4.4).
- 2) Runs the DFTTLU by calling MCN.
- 3) Runs the FFT routine.
- 4) Adjusts the scale of the FFT harmonics to that of the DFTTLU.
- 5) Analyses the differences between the two sets of harmonics.
- 6) Repeats the above steps a specified number of times.

A4.12.1 Setting the STV

The STV is programmed with the maximum number of bits representing a constant. The number of bits is reduced by shifting each constant one place to the right (ie. divide by 2). The number of times that constant is divided by 2 is set on the console switches of the computer and is loaded into location SR 5. The computer duplicates this value by writing it into RS and is printed at the end of each run.

Subroutine STLU performs the same task when overflow or underflow of the Accumulators occurs or when the resultant harmonics in PTG(A4.9) overflows. In these cases, control is passed to STLU which halves each constant in the STV and notes

this in location RS by increasing its value by 1. Control is passed to Q1.1 in MCN and the time samples are reprocessed.

A4.12.2 Calling the DFTTLU

After the STV has been set the following instructions are executed.

JSR @CCAL	Call the CCL subprogram (A4.8).
JSR @MCN	Call the MCN subprogram (A4.11)
LDA 1,RS)	Print RS
JSR @BD)	
HALT	Stops minicomputer
JMP @S7	When the 'CONTINUE' switch on the console is pressed this instruction is executed.
	S7 is the start of the FFT program.

A4.12.3 Calling the FFT

The following Assembler Code is used.

.S7: LDA 2,N	These instructions load zero into
STA 2,.N	the I1 input block of the FFT.
LDA 2,I1	
STA -2,20	
LDA 1,Z	
S4: STA 1,@20	
DSZ .N	
JMP S4	

LDA 2,N	N is passed to the FFT
STA 2,NN	program
JSR @CFTST	Call the FFT program
A: 0	The FFT program reads A. If A is zero a forward FFT is executed.
.NN:	The FFT program reads N here.
.R1: .BLK	N location input block (Real values)
.I1: .BLK	N location input block (Imaginary values). This block has been set to zero.

The .I1 block is also used as the Accumulator block. The total number of locations in all the Accumulator blocks is also N.

The addresses of the blocks are listed as follows.

```

R1: .R1 - 1
I1: .I1 - 1
SAL: .SAL - 1
etc.

```

The -1 term is included to adjust for the auto-incrementing address. This first increments the address and then executes it.

A4.12.4 Adjusting the Scale of the FFT Harmonics

The real and imaginary harmonic components of the FFT are loaded into .R1 and .I1 respectively. Subroutine PTG, (similar to the subroutine PTG in A4.9) calculates the resultant harmonics. The scale of the harmonics is adjusted while the harmonic is in its squared form and the harmonic is shifted double the required

number of times to the right. The following instructions are included in PTG.

JSR @DADD

AHS: HS

The resultant harmonic has its high order bits in reg 0 and its low order bits in reg.1.

LDA 3,SRS. Get the doubled number of shifts and
store them in

STA 3,.SRS .SRS.

S1: MOVZ 0,0 These instructions perform the
MOVR 1,1 double word shift.

DSZ .SRS

JMP S1

JMP @DSQR Take the square root.

A4.12.5 Calculating the FFT Scale Factors

The FFT has its own scale factor SCNT which depends on the value of the partial sums in the FFT. To avoid overflow every partial sum is halved if the machine code is greater than 31463_8 and the number of times that this occurs is stored in SCNT. Assuming that no overflow occurred, the FFT harmonics would still have to be scaled down by a constant MAN. If overflow does occur the final scale factor is (MAN - SCNT). This value is doubled and stored in location SRS (A4.12.4). If subroutine STLU is called (A4.12.1), (MAN - SCNT) is increased by one to keep the scales of the DFTTLU and FFT equal.

ASCNT:SCNT		ASCNT contains the address of SCNT.
LDA	1,ASCNT	} Print the contents of SCNT
JSR	@BD	
LDA	1,ASCNT	
LDA	2,MAN	
SUBO	1,2	Calculate MAN - SCNT
MOVZL	2,2	Double the result
STA	2,SRS	Store this value - the number of shifts to the right - in SRS
MOV	2,1	} Print SRS
JSR	@BD	

A4.12.6 Plotting the Differences between the DFTTLU and FFT Harmonics

The format of the plot is given in Fig.5.1 in chapter 5.3.1. A subroutine similar to STR in A4.9 is used to retrieve the FFT harmonics components from R1 and I1 and the resultant harmonic is calculated and scaled. The corresponding DFTTLU harmonic is retrieved from block RB and is subtracted from the FFT harmonic. The result is multiplied by four and plotted with its DFTTLU harmonic which has been halved. Thus the scale of the difference between the harmonics is eight times that of the DFTTLU harmonics.

LDA	0,R1	Set auto inc. address for
STA	0,20	real (R1) and imaginary (I1)
LDA	0,I1	FFT harmonic components
STA	0,21	

LDA 0,RB	Set auto inc. address for
STA 0,22	resultant DFTTLU harmonics.
LDA 0,N)	Set index for $N/2$ harmonics
MOVZR 0,0)	
STA 0,.NH)	
JSR @CPB	Position plotter pen at
	$(X,Y) = (-512, -512)_{10}$
STR: LDA 1,@20	Get real component
LDA 2,@21	Get imaginary component
JSR PTG	Calculate and scale resultant
LDA 2,@22	Get corresponding DFTTLU
	resultant harmonic.
SUBO 2,1	Subtract DFTTLU from FFT harmonic.
MOVZL 1,1)	
MOVZL 1,1)	Multiply difference by 4.
JSR @SRTC)	
JSR @DOR)	Plot difference (A4.13).
DSZ .NH	Decrement index.
JMP STR	If index is greater than $\frac{N}{2}$ process
	next harmonic.
JSR @CPE	All harmonics plotted. Mark end of
	plot with pen.
HALT	End of test.

```

      .TITL      .B128
      .ENT       STLU, PB
      .ENT       R1, SA1, CAL, SA2, CA2, SA3, CA3
      .EXTD      CPE, CPE, DOR, SPTS, SRTC
      .EXTD      CFST, MCON, CCAL, N
      .EXTN      .DAD%, MPY%, DSDR, BDEC, SCNT, TLUG
      .EXTN      Q1, 1
      .ZREL
      .LOC       250

STLU:  .STLU
XR:    Q1, 1
BD:    .BDEC
ASCHT: SCNT
R1:    .R1-1
I1:    .SA1-1
.N:    0
RB:    .RB-1
S7:    .S7
      .LOC       371

SA1:   .SA1-1
SA2:   .SA2-1
SA3:   .SA3-1
CA1:   .CA1-1
CA2:   .CA2-1
CA3:   .CA3-1

      .NREL
      LDA       1, S5
      STA       1, S5
B2:    LDA       1, ATLU
      STA       1, 20
      STA       1, 21
      LDA       1, NTLU
      STA       1, NTLU
B3:    LDA       1, 020
      MOVZB     1, 1
      STA       1, 021
      DSZ       .NTLU
      JMP       B3
      LDA       1, RS
      INC       1, 1
      STA       1, RS
      DSZ       .S5
      JMP       B2
      JSR       @CCAL
      JSR       @MCON
      LDA       1, RS
      JSR       @ED
      HALT
      JMP       0S7

      .STLU:  LDA       1, ATLU
      STA       1, 20
      STA       1, 21
      LDA       1, NTLU
      STA       1, NTLU
B1:    LDA       1, 020
      MOVZB     1, 1
      STA       1, 021
      DSZ       .NTLU
      JMP       B1
      LDA       1, RS
      INC       1, 1
      STA       1, RS
      JMP       044

```

```

ATLU:  .TLUD
NTLU:  764
RS:    0
SS:    4
Z:     0
RB:    .BLK    100

S7:    LDA    2,N
      STA    2,N
      LDA    2,I1
      STA    2,20
      LDA    1,Z
S4:    STA    1,020
      DSZ    .N
      JMP    S4

      LDA    2,N
      STA    2,NN
      JSR    @CFTST
A:     0
NN:    0
R1:    .BLK    200
SA1:   .BLK    40
CA1:   .BLK    40
SA2:   .BLK    20
CA2:   .BLK    20
SA3:   .BLK    20
CA3:   .BLK    20

      LDA    1,@ASCNT
      JSR    @ED
      LDA    1,@ASCNT
      LDA    2,MAN
      SUBO    1,2
      MOVZL   2,2
      STA    2,SFS
      MOV     2,1
      JSR    @ED
      LDA    0,R1
      STA    0,20
      LDA    0,I1
      STA    0,21
      LDA    0,RB
      STA    0,22
      LDA    0,N
      MOVZR   0,0
      STA    0,NH
      JSR    @CFB

STR:    LDA    1,020
      LDA    2,021
      JSR    PTG
      LDA    2,022
      SUBO    2,1
      MOVZL   1,1
      MOVZL   1,1
      JSR    @SRTC
      JSR    @DOP
      DSZ    .NH
      JMP    STR
      JSR    @CPE

XX:     HALT
PTG:    STA    3,RPTG
      STA    2,TC

      MOV     1,2
      JSR    @MPY
      STA    0,HS
      STA    1,LS

      LDA    1,TC
      LDA    2,TC
      JSR    @MPY

      JSR    @DADD
AHS:    HS
      LDA    3,SFS
      STA    3,SRS
S1:     MOVZR   0,0
      MOVZR   1,1
      DSZ    .SRS
      JMP    S1

      JSR    @DSOR
      JMP    @RPTG

TC:     0
HS:     0
LS:     0
RPTG:   0
NH:     0
MPY:    .MPY
DADD:   .DADD
SRS:    0
.SRS:   0
MAN:    4
DSOR:   .DSOR
END

```

```

      .TITL      .B256
      .ENT       STLU, PB
      .ENT       R1, SA1, CA1, SA2, CA2, SA3, CA3
      .EXTB      CPB, CPE, DOR, EPTB, SRTC
      .EXTD      CFTST, HCON, CCAL, N
      .EXTN      .DADD, .MPY, .DSOR, .BDEC, SCNT, .TLUD
      .EXTN      Q1, 1
      .ZREL
      .LOC       250

STLU:  .STLU
XR:    Q1, 1
BD:    .BDEC
ASCNT: SCNT
R1:    .R1-1
I1:    .SA1-1
.N:    0
RB:    .RB-1
S7:    .S7

      .LOC       371

SA1:   .SA1-1
SA2:   .SA2-1
SA3:   .SA3-1
CA1:   .CA1-1
CA2:   .CA2-1
CA3:   .CA3-1

      .NREL
      LDA       1, S5
      STA       1, S5
B2:    LDA       1, ATLU
      STA       1, 20
      STA       1, 21
      LDA       1, NTLU
      STA       1, NTLU
B3:    LDA       1, 020
      MOVZR     1, 1
      STA       1, 021
      DSZ       .NTLU
      JMP       B3
      LDA       1, RS
      INC       1, 1
      STA       1, RS
      DSZ       .S5
      JMP       B2
      JSR       @CCAL
      JSR       @HCON
      LDA       1, FS
      JSR       @BD
      HALT
      JMP       057

      .STLU: LDA       1, ATLU
      STA       1, 20
      STA       1, 21
      LDA       1, NTLU
      STA       1, NTLU
B1:    LDA       1, 020
      MOVZR     1, 1
      STA       1, 021
      DSZ       .NTLU
      JMP       B1
      LDA       1, FS
      INC       1, 1
      STA       1, FS
      JMP       @NP

```

```

ATLU: .TLUD
NTLU: 764
.NTLU: 0
RS: 0
SS: 5
.SS: 0
.RW: .BLK 200
Z: 0

.S7: LDA 2.N
STA 2.N
LDA 2.I1
STA 2.20
LDA 1.2
S4: STA 1.020
DSZ .N
JMP S4

LDA 2.N
STA 2.NN
JSR @CFTST
A: 0
.NN: 0
.R1: .BLK 400
.SA1: .BLK 100
.CA1: .BLK 100
.SA2: .BLK 40
.CA2: .BLK 40
.SA3: .BLK 40
.CA3: .BLK 40

LDA 1.0ASCNT
JSR @EQ
LDA 1.0ASCNT
LDA 2.MAN
SUBO 1.2
MOVZL 2.2
STA 2.SRS
MOV 2.1
JSR @BD
LDA 0.R1
STA 0.20
LDA 0.11
STA 0.21
LDA 0.FB
STA 0.22
LDA 0.N
MOVZL 0.0
STA 0.NH
JSR @CPB

STR: LDA 1.020
LDA 2.021
PTG
LDA 2.022
SUBO 2.1
MOVZL 1.1
MOVZL 1.1
JSR @SRTC
JSR @DOR
DSZ .NH
JMP STR
JSR @CPE

XX: HALT
PTG: STA 3.RPTG
STA 2.TC

MOV 1.2
JSR @MPY
STA 0.HS
STA 1.LS

LDA 1.TC
LDA 2.TC
JSR @MPY

JSR @DADD
AHS: HS
LDA 3.SRS
STA 3.SRS
S1: MOVZL 0.0
MOVR 1.1
DSZ .SRS
JMP S1

JSR @DSAP
JMP @RPTG

TC: 0
HS: 0
LS: 0
RPT: 0
.NH: 0
MPV: .MPV
DADD: .DADD
SRS: 0
.SRS: 0
MAN: 5
DSOR: .DSOR
END

```

```

---
      .TITL      B512
      .ENT       STLU, RB
      .ENT       R1, SA1, 0, 1, SA2, CA2, SA3, CA3
      .EXTD      CPB, CPE, DOR, SRTB, SRTC
      .EXTD      CFTST, MCON, CCAL, N
      .EXTN      , DADD, , NPY, , DSR, , BDEC, SCNT, , TLUD
      .EXTN      6, 1
      .ZREL
      .LOC       250

STLU:  .STLU
XR:    01, 1
BD:    .BDEC
ASCNT: SCNT
R1:    .R1-1
I1:    .SA1-1
.N:    0
R0:    .RB-1
S7:    .S7
      .LOC       371

SA1:   .SA1-1
SA2:   .SA2-1
SA3:   .SA3-1
CA1:   .CA1-1
CA2:   .CA2-1
CA3:   .CA3-1

      .NREL
      LDA       1, S5
      STA       1, S5
B2:    LDA       1, ATLU
      STA       1, 20
      STA       1, 21
      LDA       1, NTLU
      STA       1, NTLU
B3:    LDA       1, 020
      MOVZP     1, 1
      STA       1, 021
      DSZ       .NTLU
      JMP       B3
      LDA       1, RS
      INC       1, 1
      STA       1, RS
      DSZ       .S5
      JMP       B2
      JSR       @CCAL
      JSR       @MCON
      LDA       1, RS
      JSR       @BD
      JMP       @S7

      .STLU: LDA     1, ATLU
      STA     1, 20
      STA     1, 21
      LDA     1, NTLU
      STA     1, NTLU
B1:    LDA     1, 020
      MOVZP   1, 1
      STA     1, 021
      DSZ     .NTLU
      JMP     B1
      LDA     1, RS
      INC     1, 1
      STA     1, RS
      JMP     @XR

```

```

ATLU: .TLUD
NTLU: 764
.NTLU: 0
RS: 0
SS: 6
.SS: 0
.RB: .BLK 400
Z: 0

.S7: LDA 2.N
STA 2.N
LDA 2.11
STA 2.20
LDA 1.2
S4: STA 1.020
DSZ .N
JMP 54

LDA 2.N
STA 2.NN
JSR @CFTST

A: 0
.NN: 0
.R1: .BLK 1000
.SR1: .BLK 200
.CA1: .BLK 200
.SA2: .BLK 100
.CA2: .BLK 100
.SA3: .BLK 100
.CA3: .BLK 100

LDA 1.0ASCNT
JSR @BD
LDA 1.0ASCNT
LDA 2.MAN
SUBO 1.2
MOVZL 2.2
STA 2.SRS
MOV 2.1
JSR @BD
LDA 0.01
STA 0.20
LDA 0.11
STA 0.1
LDA 0.1
STA 0.12
S6: LDA 0.N
MOVZL 0.0
MOVZL 0.0
MOVZL 0.0
STA 0.NH
JSR @CPB

STR: LDA 1.022
STA 1.TR
JSR @SPTB
JSR @DOR

LDA 1.020
LDA 2.021
JSR PTG
LDA 2.TR
SUBO 2.1
MOVZL 1.1
MOVZL 1.1
JSR @SRTC
JSR @DOR
.NH
JMP STR
JSR @CPE

XX: HALT
DSZ .N0
JMP 56
HALT
HALT

PTG: STA 3.RPTG
STA 2.TC

MOV 1.2
JSR @MPY
STA 0.HS
STA 1.LS

LDA 1.TC
LDA 2.TC
JSR @MPY

JSR @DADD
AHS: HS
LDA 3.SRS
STA 3.SRS
S1: MOVZL 0.0
MOVZL 1.1
DSZ .SRS
JMP S1

JSR @DSOR
JMP @RPTG

TC: 0
HS: 0
LS: 0
RPTG: 0
.NH: 0
MPY: .MPY
DADD: .DADD
SRS: 0
TR: 0
.N0: 4
.CRS: 0
MAN: 6
DSOR: .DSOR
END
---
```

```

      .TITL      B1024
      .ENT       STLU, RB
      .ENT       P1, S11, CA1, SA2, CA2, SA3, CA3
      .EXTD      CPE, CPE, DOP, SATB, SPTC
      .EXTD      CFTST, MCON, CCAL, N
      .EXTN      .DADD, .MPV, .DSOR, .BDEC, SCNT, .TLUD
      .EXTN      Q1, 1
      .ZREL
      .LOC       250

STLU:  .STLU
XR:    Q1, 1
BD:    .BDEC
ASCNT: SCNT
R1:    .R1-1
I1:    .SA1-1
.N:    0
RB:    .RB-1
S7:    .S7
      .LOC       371

SA1:   .SA1-1
SA2:   .SA2-1
SA3:   .SA3-1
CA1:   .CA1-1
CA2:   .CA2-1
CA3:   .CA3-1

      .NREL
      LDA       1, S5
      STA       1, S5
B2:    LDA       1, ATLU
      STA       1, 20
      STA       1, 21
      LDA       1, NTLU
      STA       1, .NTLU
B3:    LDA       1, 020
      MOVZP     1, 1
      STA       1, 021
      DSZ       .NTLU
      JMP       B3
      LDA       1, RS
      INC       1, 1
      STA       1, RS
      DSC       .S5
      JMP       B2
      JSR       @CCAL
      JSR       @MCON
      LDA       1, RS
      JSR       @B0
      JMP       @S7

      .STLU: LDA       1, ATLU
      STA       1, 20
      STA       1, 21
      LDA       1, NTLU
      STA       1, .NTLU
B1:    LDA       1, 020
      MOVZP     1, 1
      STA       1, 021
      DSC       .NTLU
      JMP       B1
      LDA       1, RS
      INC       1, 1
      STA       1, RS
      JMP       @S7

```

ATLU:	TLUD		LDA	1, 020
NTLU:	764		LDA	2, 021
NTLU:	0		JSR	PTG
RS:	0		LDA	2, TR
SS:	6		SUBO	2, 1
SS:	0		MOVZL	1, 1
RB:	BLK	1000	MOVZL	1, 1
Z:	0		JSR	05RTC
			JSR	0DOR
S7:	LDA	2, N	DSZ	NH
	STA	2, N	JMP	STR
	LDA	2, 11	JSR	0CPE
	STA	2, 20		
	LDA	1, Z		
S4:	STA	1, 020	XX:	HALT
	DSZ	N	DSZ	NQ
	JMP	S4	JMP	S6
			HALT	
			HALT	
	LDA	2, N	PTG:	STA
	STA	2, NN		3, RPTG
	JSR	0CFTST		2, TC
A:	0			
NN:	0		MOV	1, 2
R1:	BLK	2000	JSR	0MPY
SA1:	BLK	400	STA	0, H5
CA1:	BLK	400	STA	1, LS
SA2:	BLK	200		
CA2:	BLK	200	LDA	1, TC
SA3:	BLK	200	LDA	2, TC
CA3:	BLK	200	JSR	0MF
	LDA	1, 0ASCNT	JSR	0DADD
	JSR	0B0	HS	
	LDA	1, 0ASCNT	LDA	3, SRS
	LDA	2, 11AN	STA	3, SRS
	SUBO	1, 2	S1:	MOVZL
	MOVZL	2, 2		0, 0
	STA	2, SRS		1, 1
	MOV	2, 1		DSZ
	JSR	0ED		JMP
	LDA	0, R1		S1
	STA	0, 20	JSR	0DSQR
	LDA	0, 14	JMP	0RPTG
	STA	0, 21		
	LDA	0, 1B	TC:	0
	STA	0, 22	HS:	0
S6:	LDA	0, N	LS:	0
	MOVZL	0, 0	RPTG:	0
	MOVZL	0, 0	NH:	0
	MOVZL	0, 0	MPY:	MPY
	STA	0, NH	DADD:	DADD
	JSR	0CFB	SRS:	0
			TR:	0
			NQ:	4
			SRS:	0
STR:	LDA	1, 022	MAN:	6
	STA	1, TR	DSQR:	DSQR
	JSR	05RTC	ENC:	
	JSR	0DOR		

A4.12.7 Numerical Analysis of Errors - ESR Subroutine

The ESR subroutine implements the algorithm discussed in chapter 5.3. The routine sorts out which quantising level, H_p , accommodates F_k and then accumulates the magnitude of the error and the squared error in accumulators ET_p and ST_p respectively. The number of harmonics with magnitude within the limits of H_p is stored in location N_p . The limits of H_p in machine code are:

$$40000_8 \leq H_{14} < 77777_8$$

$$20000_8 \leq H_{13} < 37777_8$$

$$\vdots$$

$$4_8 \leq H_2 < 7_8$$

$$2_8 \leq H_1 < 3_8$$

$$H_0 = 1.$$

The most significant bit (MSB) of F_k is ANDed with 40000_8 , 20000_8 , 10000_8 , ..., 1_8 successively. eg. If the result of ANDing with 10000_8 is TRUE then F_k is in quantising level H_{12} and the magnitude of the error is added to ET_{12} , the squared error is added to ST_{12} and N_{12} is incremented by 1. ESR processes the remaining harmonics in a similar way.

LCK: 40000_8

.ESR: STA 3,RESR	Save return to STR.
LDA 2,TDF	Load F_k into TDF.
LDA 3,LCK	Load 40000 into LCK
AND 2,3,SZR	AND F_k and 40000_8 . If result is FALSE skip next instruction.

JMP L15	Result is TRUE Go to L15
MOVZR 3,3	Result is false. Halve 40000_8 .
AND 2,2,SZR	AND F_k and 20000_8

These steps are repeated for all H_p .

.
.
.

L15: LDA 2,ET15	Get current error magnitude subtotal from ET15.
ADD 1,2	Add error
STA 1,ET 15	Store new subtotal in ET15.
MOV 1,2)	
JSR @AMPY)	
LDA 2,ST15)	
ADD 1,2)	Add error squared to ST15
STA 2,ST15	
ISZ N15	Increment N_{15} , the number of harmonics with magnitudes in level H_{15} .
JMP L0	

L14: .
.
.
.
.
.
.

L0: JMP @RESR	Return to STR subroutine.
---------------	---------------------------

The STR routine is slightly modified.

STR: LDA 1,@20)	
LDA 2,@21)	Calculate FFT resultant harmonic
JSR PTG)	
LDA 2,@22	Get DFTLU resultant harmonic
STA 2,TDF	Store in TDF for ESR subroutine
SUBO 2,1	Calculate error.
MOVZL 1,1,SZC)	If sign is negative, take the two's
NEG 1,1)	complement, i.e. the magnitude of the
	error is required
JSR @ESR	Call ESR subroutine
DSZ .NH	Decrement index
JMP STR	Index not zero. Process next
	harmonic
DSZ .NR	Decrement program index (Set to 32)
JMP @S2	Index not zero. Process next transform
HALT	Index zero. 32 transforms processed.

On pressing the 'CONTINUE' switch on the console, the program writes

$ET_p, ST_p, N_p, p = 0 \dots 14$ from the accumulated results of 32 transforms and then returns to DDOS³ mode.

```

      .TITL  G128
      .ENT   STLU R
      .EX1N  .DIVI,PUTC
      .ENT   R1,SA1,CA1,SA2,CA2,SA3,CA3
      .EXTD  CFTST,MCON,CCAL,N
      .EXTN  .DADDV,HPV,DSGR,BDEC,SCNT,TLUD
      .EXTN  Q1.1
      .ZREL
      .LOC   250

STLU:  .STLU
XR:    Q1.1
BD:    .BDEC
ASCNT: SCNT
R1:    .R1-1
I1:    .SA1-1
.N:    0
RB:    .RB-1
S7:    .S7
      .LOC   371

SA1:   .SA1-1
SA2:   .SA2-1
SA3:   .SA3-1
CA1:   .CA1-1
CA2:   .CA2-1
CA3:   .CA3-1

      .NREL
      LDA   1,S5
      STA   1,S5
B2:     LDA   1,ATLU
      STA   1,20
      STA   1,21
      LDA   1,NTLU
      STA   1,NTLU
B3:     LDA   1,020
      MOVZR 1,1
      STA   1,021
      DSZ   .NTLU
      JMP   B3
      LDA   1,RS
      INC   1,1
      STA   1,RS
      DSZ   .S5
      JMP   .
      JSR   .AL
.S2:     JSR   .N
      LDA   .LD
      JSR   .LD
      JMP   057

.STLU:  LDA   1,ATLU
      STA   1,20
      STA   1,21
      LDA   1,NTLU
      STA   1,NTLU
B1:     LDA   1,020
      MOVZR 1,1
      STA   1,021
      DSZ   .NTLU
      JMP   B1
      LDA   1,RS
      INC   1,1
      STA   1,RS
      LDA   1,MAN
      INC   1,1
      STA   1,MAN
      JMP   0XR

```

ATLU: . TLUD				PTG: STA 3, RPTG
NTLU: 764		LDA 1, RET15		STA 2, TC
. NTLU: 0		LDA 2, AN15		
RS: 0		JSR 59		MOV 1, 2
SS: 3		LDA 1, RET10		JSR 0MPY
MAN: 3		LDA 2, AN10		STA 0, HS
. S5: 0		JSR 59		STA 1, LS
. RB: . BLK 100		LDA 1, RET5		
Z: 0		LDA 2, AN5		LDA 1, TC
		JSR 59		LDA 2, TC
		LDA 0, ASS		JSR 0MPY
. S7: LDA 2, N		JSR 0APUTC		
STA 2, N				JSR 0DADC
LDA 2, 11				
STA 2, 10		LDA 1, RET15		HS
LDA 1, 2		JSR 56		LDA 3, SRS
S4: STA 1, 020		LDA 1, RET10		STA 3, SRS
DSZ N		JSR 56		51: MOVZ 0, 0
JMP 54		LDA 1, RET5		MOV 1, 1
		JSR 56		DSZ . SRS
		LDA 0, ASS		JMP 51
		JSR 0APUTC		JSR 0DSQR
				JMP 0RPTG
		LDA 1, AST15		
A: 0		JSR 56		AMAN: MAN
. NN: 0		LDA 1, AST10		SRS: 0
. R1: . BLK 200		JSR 56		. SRS: 0
. SA1: . BLK 40		LDA 1, AST5		NN5: 5
. CR1: . BLK 40		JSR 56		. NN5: 0
. SA2: . BLK 20		LDA 0, ASS		. NH: 0
. CR2: . BLK 20		JSR 0APUTC		S2: . S2
. SA3: . BLK 20				RET15: ET15-1
. CR3: . BLK 20				RET10: ET10-1
		LDA 1, AN15		RET5: ET5-1
LDA 1, 0ASCNT		JSR 56		AST15: ST15-1
JSR 0BD		LDA 1, AN10		AST10: ST10-1
LDA 1, 0ASCNT		JSR 56		AST5: ST5-1
LDA 2, 0AMAN		LDA 1, AN5		AN15: N15-1
SUB0 1, 2		JSR 56		AN10: N10-1
MOVZL 2, 2				ANS: N5-1
STA 2, SRS		LDA 0, ASS		SRET: 0
MOV 2, 1		JSR 0APUTC		APUTC: PUTC
JSR 0BD		LDA 0, ASS		. NR: 40
LDA 0, R1		JSR 0APUTC		ESR: . ESR
STA 0, 20		JMP 0R105		TC: 0
LDA 0, 11				HS: 0
STA 0, 21		S9: STA 3, SRET		LS: 0
LDA 0, RB		STA 1, 20		RPTG: 0
STA 0, 22		STA 2, 21		MPV: . MPV
LDA 0, H		LDA 1, NN5		DIVI: . DIVI
MOVZ 0, 0		STA 1, NN5		DADC: . DADC
STA 0, . NH		LDA 1, 020		DSQR: . DSQR
		LDA 2, 021		TDF: 0
STR: LDA 1, 020		JSR 0DIVI		LCK: 40000
LDA 2, 021		JSR 0BD		RDOS: 37600
JSR PTG		DSZ . NN5		ASS: 0
LDA 2, 022		JMP 594		
STA 2, TDF		JMP 0SRET		
SUB0 2, 1				
MOVL# 1, 1, SZC		S6: STA 3, SRET		
NEG 1, 1		STA 1, 20		
JSR 0ESR		LDA 1, NN5		
DSZ . NH		STA 1, NN5		
JMP STP		LDA 1, 020		
DSZ . NR		JSR 0BD		
JMP 0S2		DSZ . NN5		
HALT		JMP 561		
		JMP 0SRET		

[illegible]

```

.L5:  LDA    2, ET5
      ADD    1, 2
      STA    2, ET5
      MOV    1, 2
      JSR    @AMPY
      LDA    2, ST5
      ADD    1, 2
      STA    2, ST5
      ISZ    N5
      JMP    L0
.L4:  LDA    2, ET4
      ADD    1, 2
      STA    2, ET4
      MOV    1, 2
      JSR    @AMPY
      LDA    2, ST4
      ADD    1, 2
      STA    2, ST4
      ISZ    N4
      JMP    L0
.L3:  LDA    2, ET3
      ADD    1, 2
      STA    2, ET3
      MOV    1, 2
      JSR    @AMPY
      LDA    2, ST3
      ADD    1, 2
      STA    2, ST3
      ISZ    N3
      JMP    L0
.L2:  LDA    2, ET2
      ADD    1, 2
      STA    2, ET2
      MOV    1, 2
      JSR    @AMPY
      LDA    2, ST2
      ADD    1, 2
      STA    2, ST2
      ISZ    N2
      JMP    L0
.L1:  LDA    2, ET1
      ADD    1, 2
      STA    2, ET1
      MOV    1, 2
      JSR    @AMPY
      LDA    2, ST1
      ADD    1, 2
      STA    2, ST1
      ISZ    N1
      JMP    L0
ET5:  0
ET4:  0
ET3:  0
ET2:  0
ET1:  0
ST5:  0
ST4:  0
ST3:  0
ST2:  0
ST1:  0
N5:   0
N4:   0
N3:   0
N2:   0
N1:   0
.END
---
```

```

---
      .TITL    G256
      .ENT     STLU, RB
      .EXTN    .DIVI, PUTC
      .ENT     R1, SA1, CA1, SA2, CA2, SA3, CA3
      .EXTD    CFTST, MOON, CCAL, N
      .EXTN    .DADC, .MPY, .DSAR, .BDEC, .CNT, .TLUD
      .EXTN    Q1, 1
      .ZREL
      .LOC     250

STLU:  .STLU
XR:    Q1, 1
BD:    .BDEC
ASCNT: SCNT
R1:    .R1-1
I1:    .SA1-1
.N:    0
RB:    .RB-1
S7:    .S7
      .LOC     371

SA1:   .SA1-1
SA2:   .SA2-1
SA3:   .SA3-1
CA1:   .CA1-1
CA2:   .CA2-1
CA3:   .CA3-1

      .NREL
      LDA     1, S5
      STA     1, S5
B2:     LDA     1, ATLU
      STA     1, 20
      STA     1, 21
      LDA     1, NTLU
      STA     1, NTLU
B3:     LDA     1, Q20
      MOVZR   1, 1
      STA     1, Q21
      DSZ     .NTLU
      JMP     B3
      LDA     1, RS
      INC     1, 1
      STA     1, RS
      DSZ     .S5
      JMP     B2
      JSR     @CCAL
      JSR     @MC'ON
      LDA     1, P5
      JSR     @ED
      JMP     @S7

      .STLU
      LDA     1, ATLU
      STA     1, 20
      STA     1, 21
      LDA     1, NTLU
      STA     1, NTLU
B4:     LDA     1, Q20
      MOVZR   1, 1
      STA     1, Q21
      DSZ     .NTLU
      JMP     R1
      LDA     1, RS
      INC     1, 1
      STA     1, RS
      LDA     1, MAN
      INC     1, 1
      STA     1, MAN
      JMP     @XP

```

ATLU:	. TLUD	LDA	1. PET15	PTG:	STA	3. RPTG
NTLU:	764	LDA	2. AN15		STA	2. TC
. NTLU:	0	JSR	S9			
RS:	0	LDA	1. RET10		MOV	1. 2
SS:	4	LDA	2. AN10		JSR	0MPY
MAN:	4	JSR	S9		STA	0. HS
. SS:	0	LDA	1. RET5		STA	1. LS
. RB:	. BLK 200	LDA	2. AN5			
Z:	0	JSR	S9		LDA	1. TC
		LDA	0. ASS		LDA	2. TC
		JSR	0APUTC		JSR	0MPY
. S7:	LDA 2. N	LDA	1. RET15		JSR	0DADD
	STA 2. N	JSR	S6	AHS:	HS	
	LDA 2. I1	LDA	1. RET10		LDA	3. SRS
	STA 2. 20	JSR	S6		STA	3. SRS
	LDA 1. 2	LDA	1. RET5	S1:	MOVZR	0. 0
S4:	STA 1. 020	JSR	S6		MOVZ	1. 1
	DSZ . N	LDA	0. ASS		DSZ	. SRS
	JMP 54	JSR	0APUTC		JMP	S1
					JSR	0DSOR
	LDA 2. N	LDA	1. AST15		JMP	0RPTG
	STA 2. NN	JSR	S6			
	JSR 0CFTST	LDA	1. AST10	AMAN:	MAN	
A:	0	JSR	S6		SRS:	0
. NN:	0	LDA	1. AST5		. SRS:	0
. R1:	. BLK 400	JSR	S6		NN5:	5
. SA1:	. BLK 100	LDA	0. ASS		NN5:	0
. CA1:	. BLK 100	JSR	0APUTC		. NH:	0
. SA2:	. BLK 40	LDA	1. AN15		S2:	. S2
. CA2:	. BLK 40	JSR	S6		RET15:	ET15-1
. SA3:	. BLK 40	LDA	1. AN10		RET10:	ET10-1
. CA3:	. BLK 40	JSR	S6		RET5:	ET5-1
		LDA	1. AN5		AST15:	ST15-1
	LDA 1. 0ASCNT	JSR	S6		AST10:	ST10-1
	JSR 0BD	LDA	0. ASS		AST5:	ST5-1
	LDA 1. 0ASCNT	JSR	0APUTC		AN15:	N15-1
	LDA 2. 0AMAN	LDA	0. ASS		AN10:	N10-1
	SUBO 1. 3	JSR	0APUTC		AN5:	N5-1
	MOVZL 2. 2	LDA	0. ASS		SRET:	0
	STA 2. SRS	JSR	0APUTC		APUTC:	PUTC
	MOV 2. 1	LDA	0. ASS		. NR:	40
	JSR 0BD	JSR	0RDS		ESR:	. ESR
	LDA 0. R1	JMP			TC:	0
	STA 0. 20				HS:	0
	LDA 0. I1	SS	STA 3. SPET		LS:	0
	STA 0. 21		STA 1. 20		RPTG:	0
	LDA 0. PB		STA 2. 21		MPV:	. MPV
	STA 0. 22		LDA 1. NN5		DIVI:	. DIVI
	LDA 0. N		STA 1. NN5		DADD:	. DADD
	MOVZR 0. 0	S91:	LDA 1. 020		DSOR:	. DSOR
	STA 0. NH		LDA 2. 021		DDF:	0
			JSR 0DIVI		LCK:	40000
STR:	LDA 1. 020		JSR 0BD		RDOS:	37000
	LDA 2. 021		DSZ . NN5		ASS:	0
	JSR PTG		JMP 591			
	LDA 2. 022		JMP 0SPET			
	STA 2. TDF					
	SUBO 2. 1	S6:	STA 3. SRET			
	MOVL# 1. 1. SZC		STA 1. 20			
	NEG 1. 1		LDA 1. NN5			
	JSR 0ESR		STA 1. NN5			
	DSZ . NH	S61:	LDA 1. 020			
	JMP STR		JSR 0BD			
	DSZ . NR		DSZ . NN5			
	JMP 052		JMP 561			
	HALT		JMP 0SPET			

```

.ESR: STA 3, RESR
      LDA 2, TDF
      LDA 3, LCK

      AND# 2, 3, SZR
      JMP L15
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L11
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L13
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L12
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L11
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L10
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L9
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L8
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L7
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L6
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L5
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L4
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L3
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L2
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L1

```

```

L5: .L5
L4: .L4
L3: .L3
L2: .L2
L1: .L1

```

```

L15: LDA 2, ET15
      ADD 1, 2
      STA 2, ET15
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST15
      ADD 1, 2
      STA 2, ST15
      ISZ N15
      JMP L8
L14: LDA 2, ET14
      ADD 1, 2
      STA 2, ET14
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST14
      ADD 1, 2
      STA 2, ST14
      ISZ N14
      JMP L8
L13: LDA 2, ET13
      ADD 1, 2
      STA 2, ET13
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST13
      ADD 1, 2
      STA 2, ST13
      ISZ N13
      JMP L8
L12: LDA 2, ET12
      ADD 1, 2
      STA 2, ET12
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST12
      ADD 1, 2
      STA 2, ST12
      ISZ N12
      JMP L8
L11: LDA 2, ET11
      ADD 1, 2
      STA 2, ET11
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST11
      ADD 1, 2
      STA 2, ST11
      ISZ N11
      JMP L8
ET15: 0
ET14: 0
ET13: 0
ET12: 0
ET11: 0
ST15: 0
ST14: 0
ST13: 0
ST12: 0
ST11: 0
N15: 0
N14: 0
N13: 0
N12: 0
N11: 0
L8: JMP @RESR
RESR: 0
AMPY: 0

```

```

252
L10: LDA 2, ET10
      ADD 1, 2
      STA 2, ET10
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST10
      ADD 1, 2
      STA 2, ST10
      ISZ N10
      JMP L8
L9: LDA 2, ET9
      ADD 1, 2
      STA 2, ET9
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST9
      ADD 1, 2
      STA 2, ST9
      ISZ N9
      JMP L8
L8: LDA 2, ET8
      ADD 1, 2
      STA 2, ET8
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST8
      ADD 1, 2
      STA 2, ST8
      ISZ N8
      JMP L8
L7: LDA 2, ET7
      ADD 1, 2
      STA 2, ET7
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST7
      ADD 1, 2
      STA 2, ST7
      ISZ N7
      JMP L8
L6: LDA 2, ET6
      ADD 1, 2
      STA 2, ET6
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST6
      ADD 1, 2
      STA 2, ST6
      ISZ N6
      JMP L8
ET10: 0
ET9: 0
ET8: 0
ET7: 0
ET6: 0
ST10: 0
ST9: 0
ST8: 0
ST7: 0
ST6: 0
N10: 0
N9: 0
N8: 0
N7: 0
N6: 0

```

```

.L5:   LDA     2,ET5
       ADD     1,2
       STA     2,ET5
       MOV     1,2
       JSR     @AMPY
       LDA     2,ST5
       ADD     1,2
       STA     2,ST5
       ISZ     N5
       JMP     L0
.L4:   LDA     2,ET4
       ADD     1,2
       STA     2,ET4
       MOV     1,2
       JSR     @AMPY
       LDA     2,ST4
       ADD     1,2
       STA     2,ST4
       ISZ     N4
       JMP     L0
.L3:   LDA     2,ET3
       ADD     1,2
       STA     2,ET3
       MOV     1,2
       JSR     @AMPY
       LDA     2,ST3
       ADD     1,2
       STA     2,ST3
       ISZ     N3
       JMP     L0
.L2:   LDA     2,ET2
       ADD     1,2
       STA     2,ET2
       MOV     1,2
       JSR     @AMPY
       LDA     2,ST2
       ADD     1,2
       STA     2,ST2
       ISZ     N2
       JMP     L0
.L1:   LDA     2,ET1
       ADD     1,2
       STA     2,ET1
       MOV     1,2
       JSR     @AMPY
       LDA     2,ST1
       ADD     1,2
       STA     2,ST1
       ISZ     N1
       JMP     L0
ET5:   0
ET4:   0
ET3:   0
ET2:   0
ET1:   0
ST5:   0
ST4:   0
ST3:   0
ST2:   0
ST1:   0
N5:    0
N4:    0
N3:    0
N2:    0
N1:    0
.END

```

```

        .TITL      G512
        .ENT       STLU,RB
        .EXTN      .DIVI,PUTC
        .ENT       R1,SA1,CA1,SA2,CA2,SA3,CA3
        .EXTD      CFTST,HCON,CCAL,N
        .EXTN      .DADD,.MPY,.DSAR,.BDEC,SCNT,TLUD
        .EXTN      Q1.1
        .ZREL
        .LOC       250

STLU:   .STLU
XR:     Q1.1
BD:     .BDEC
ASCNT:  SCNT
R1:     .R1-1
I1:     .SA1-1
.N:     0
RB:     .RB-1
S7:     .S7
        .LOC       371

SA1:    .SA1-1
SA2:    .SA2-1
SA3:    .SA3-1
CA1:    .CA1-1
CA2:    .CA2-1
CA3:    .CA3-1

        .NREL
        LDA       1,S5
        STA       1,S5
B2:     LDA       1,ATLU
        STA       1,20
        STA       1,21
        LDA       1,NTLU
        STA       1,NTLU
B3:     LDA       1,Q20
        MOVZR     1,1
        STA       1,Q21
        DSZ       .NTLU
        JMP       23
        LDA       1,RS
        INC       1,1
        STA       1,RS
        DSZ       .S5
        JMP       B2
        JSR       @CCAL
        JSR       @HCON
        LDA       1,RS
        JSR       @BD
        JMP       @S7

        .STLU:    LDA       1,ATLU
        STA       1,20
        STA       1,21
        LDA       1,NTLU
        STA       1,NTLU
B1:     LDA       1,Q20
        MOVZR     1,1
        STA       1,Q21
        DSZ       .NTLU
        JMP       B1
        LDA       1,RS
        INC       1,1
        STA       1,RS
        LDA       1,MAN
        INC       1,1
        STA       1,MAN
        JMP       @XR

```

```

ATLU: .TLUD          LDA      1,RET15
NTLU: 764           LDA      2,AN15
. NTLU: 0            JSR      S9
RS: 0               LDA      1,RET10
SS: 5               LDA      2,AN10
MAN: 5              JSR      S9
.SS: 0              LDA      1,RET5
.RB: .BLK 400        LDA      2,AN5
Z: 0                JSR      S9
                      LDA      0,ASS
.S7: LDA 2,N         JSR      @APUTC      PTG: STA 3,RPTG
                      STA 2,N          STA 2,TC
                      LDA 2,I1
                      STA 2,20
                      LDA 1,2
S4: STA 1,020        JSR      1,RET15
                      DSZ .N           JSR      S6
                      JMP S4           LDA      1,RET10
                      LDA 2,N          JSR      S6
                      STA 2,N          LDA      1,RET5
                      JSR @CFTST       JSR      S6
A: 0                 LDA      0,ASS
.NN: 0              JSR      @APUTC
.R1: .BLK 1000       LDA      1,AST15
.SA1: .BLK 200       JSR      S6
.CA1: .BLK 200       LDA      1,AST10
.SA2: .BLK 100       JSR      S6
.CA2: .BLK 100       LDA      1,AST5
.SA3: .BLK 100       JSR      S5
.CA3: .BLK 100       LDA      0,ASS
                      JSR      @APUTC
                      LDA 1,AN15
                      JSR S6
                      LDA 1,AN10
                      JSR S6
                      LDA 1,AN5
                      JSR S6
                      LDA 0,ASS
                      JSR @APUTC
                      LDA 0,ASS
                      JSR @APUTC
                      JMP @RDOS
                      LDA 3,SRET
S9: STA 1,20
                      STA 2,21
                      LDA 1,NN5
                      STA 1,NN5
S91: LDA 1,020
                      LDA 2,021
                      JSR @DIVI
                      JSR @B0
                      DSZ .NN5
                      JMP S91
                      JMP @SRET
S6: STA 3,SRET
                      STA 1,20
                      LDA 1,NN5
                      STA 1,NN5
S61: LDA 1,020
                      JSR @B0
                      DSZ .NN5
                      JMP S61
                      JMP @SRET
                      LDA 1,RET15
                      LDA 2,AN15
                      JSR S9
                      LDA 1,RET10
                      LDA 2,AN10
                      JSR S9
                      LDA 1,RET5
                      LDA 2,AN5
                      JSR S9
                      LDA 0,ASS
                      JSR @APUTC
                      LDA 1,AST15
                      JSR S6
                      LDA 1,AST10
                      JSR S6
                      LDA 1,AST5
                      JSR S5
                      LDA 0,ASS
                      JSR @APUTC
                      LDA 1,AN15
                      JSR S6
                      LDA 1,AN10
                      JSR S6
                      LDA 1,AN5
                      JSR S6
                      LDA 0,ASS
                      JSR @APUTC
                      LDA 0,ASS
                      JSR @APUTC
                      JMP @RDOS
                      STA 3,SRET
                      STA 1,20
                      STA 2,21
                      LDA 1,NN5
                      STA 1,NN5
                      LDA 1,020
                      JSR @B0
                      DSZ .NN5
                      JMP S61
                      JMP @SRET
                      PTG: STA 3,RPTG
                      STA 2,TC
                      MOV 1,2
                      JSR @MPY
                      STA 0,HS
                      STA 1,LS
                      LDA 1,TC
                      LDA 2,TC
                      JSR @MPY
                      JSR @DADD
                      HS
                      LDA 3,SRS
                      STA 3,SRS
                      MOVZ 0,0
                      MOVZ 1,1
                      DSZ .SRS
                      JMP S1
                      JSR @DSOR
                      JMP @PPTG
                      AHS: HS
                      LDA 3,SRS
                      STA 3,SRS
                      MOVZ 0,0
                      MOVZ 1,1
                      DSZ .SRS
                      JMP S1
                      JSR @DSOR
                      JMP @PPTG
                      AMAN: MAN
                      SRS: 0
                      .SRS: 0
                      NN5: 5
                      .NN5: 0
                      .NH: 0
                      S2: .S2
                      RET15: ET15-1
                      RET10: ET10-1
                      RET5: ET5-1
                      AST15: ST15-1
                      AST10: ST10-1
                      AST5: ST5-1
                      AN15: N15-1
                      AN10: N10-1
                      AN5: N5-1
                      SRET: 0
                      APUTC: PUTC
                      .NR: 40
                      ESR: .ESR
                      TC: 0
                      HS: 0
                      LS: 0
                      RPTG: 0
                      MPY: .MPY
                      DIVI: .DIVI
                      DADD: .DADD
                      DSOR: .DSOR
                      TDF: 0
                      LCK: 40000
                      RDOS: 37500
                      ASS: 0

```

```

.ESP: STA 2,RESP
      LDA 2,TDF
      LDA 3,LCK

      AND# 2,2,SZR
      JMP L15
      MOVZP 3,2
      AND# 2,2,SZR
      JMP L14
      MOVZP 2,3
      AND# 2,3,SZR
      JMP L13
      MOVZP 3,3
      AND# 2,3,SZR
      JMP L12
      MOVZP 3,3
      AND# 2,3,SZR
      JMP L11
      MOVZP 3,3
      AND# 2,3,SZR
      JMP L7
      MOVZP 3,3
      AND# 2,3,SZR
      JMP L6
      MOVZP 3,3
      AND# 2,3,SZR
      JMP L5
      MOVZP 3,3
      AND# 2,3,SZR
      JMP L4
      MOVZP 3,3
      AND# 2,3,SZR
      JMP L3
      MOVZP 3,3
      AND# 2,3,SZR
      JMP L2
      MOVZP 3,3
      AND# 2,3,SZR
      JMP L1

L5: .L5
L4: .L4
L3: .L3
L2: .L2
L1: .L1

L15: LDA 2,ET15
      ADD 1,2
      STA 2,ET15
      MOV 1,2
      JSR @AMPY
      LDA 2,ST15
      ADD 1,2
      STA 2,ST15
      ISZ N15
      JMP L0

L14: LDA 2,ET14
      ADD 1,2
      STA 2,ET14
      MOV 1,2
      JSR @AMPY
      LDA 2,ST14
      ADD 1,2
      STA 2,ST14
      ISZ N14
      JMP L0

L13: LDA 2,ET13
      ADD 1,2
      STA 2,ET13
      MOV 1,2
      JSR @AMPY
      LDA 2,ST13
      ADD 1,2
      STA 2,ST13
      ISZ N13
      JMP L0

L12: LDA 2,ET12
      ADD 1,2
      STA 2,ET12
      MOV 1,2
      JSR @AMPY
      LDA 2,ST12
      ADD 1,2
      STA 2,ST12
      ISZ N12
      JMP L0

L11: LDA 2,ET11
      ADD 1,2
      STA 2,ET11
      MOV 1,2
      JSR @AMPY
      LDA 2,ST11
      ADD 1,2
      STA 2,ST11
      ISZ N11
      JMP L0

ET15: 0
ET14: 0
ET13: 0
ET12: 0
ET11: 0
ST15: 0
ST14: 0
ST13: 0
ST12: 0
ST11: 0
N15: 0
N14: 0
N13: 0
N12: 0
N11: 0
L0: JMP @RESR
RESP: 0
AMPY: .MPY

L10: LDA 2,ET10
      ADD 1,2
      STA 2,ET10
      MOV 1,2
      JSR @AMPY
      LDA 2,ST10
      ADD 1,2
      STA 2,ST10
      ISZ N10
      JMP L0

L9: LDA 2,ET9
      ADD 1,2
      STA 2,ET9
      MOV 1,2
      JSR @AMPY
      LDA 2,ST9
      ADD 1,2
      STA 2,ST9
      ISZ N9
      JMP L0

L8: LDA 2,ET8
      ADD 1,2
      STA 2,ET8
      MOV 1,2
      JSR @AMPY
      LDA 2,ST8
      ADD 1,2
      STA 2,ST8
      ISZ N8
      JMP L0

L7: LDA 2,ET7
      ADD 1,2
      STA 2,ET7
      MOV 1,2
      JSR @AMPY
      LDA 2,ST7
      ADD 1,2
      STA 2,ST7
      ISZ N7
      JMP L0

L6: LDA 2,ET6
      ADD 1,2
      STA 2,ET6
      MOV 1,2
      JSR @AMPY
      LDA 2,ST6
      ADD 1,2
      STA 2,ST6
      ISZ N6
      JMP L0

ET10: 0
ET9: 0
ET8: 0
ET7: 0
ET6: 0
ST10: 0
ST9: 0
ST8: 0
ST7: 0
ST6: 0
N10: 0
N9: 0
N8: 0
N7: 0
N6: 0

```

```

.L5:   LDA      2, ET5
      ADD      1, 2
      STA      2, ET5
      MOV      1, 2
      JSR      @AMPY
      LDA      2, ST5
      ADD      1, 2
      STA      2, ST5
      ISZ      N5
      JMP      L0
.L4:   LDA      2, ET4
      ADD      1, 2
      STA      2, ET4
      MOV      1, 2
      JSR      @AMPY
      LDA      2, ST4
      ADD      1, 2
      STA      2, ST4
      ISZ      N4
      JMP      L0
.L3:   LDA      2, ET3
      ADD      1, 2
      STA      2, ET3
      MOV      1, 2
      JSR      @AMPY
      LDA      2, ST3
      ADD      1, 2
      STA      2, ST3
      ISZ      N3
      JMP      L0
.L2:   LDA      2, ET2
      ADD      1, 2
      STA      2, ET2
      MOV      1, 2
      JSR      @AMPY
      LDA      2, ST2
      ADD      1, 2
      STA      2, ST2
      ISZ      N2
      JMP      L0
.L1:   LDA      2, ET1
      ADD      1, 2
      STA      2, ET1
      MOV      1, 2
      JSR      @AMPY
      LDA      2, ST1
      ADD      1, 2
      STA      2, ST1
      ISZ      N1
      JMP      L0
ET5:   0
ET4:   0
ET3:   0
ET2:   0
ET1:   0
ST5:   0
ST4:   0
ST3:   0
ST2:   0
ST1:   0
N5:    0
N4:    0
N3:    0
N2:    0
N1:    0
.END

```

```

      .TITL  G1024
      .ENT   STLU, RB
      .EXTN   .DIVI, PUTC
      .ENT   R1, SA1, CA1, SA2, CA2, SA3, CA3
      .EXTD   CFTST, MCON, CCAL, N
      .EXTN   .PACD, .MPY, .DSAR, .BDEC, SCNT, .TLUD
      .EXTN   Q1, 1
      .ZREL
      .LOC    250

STLU:  .STLU
XR:    Q1, 1
BD:    .BDEC
ASCNT: SCNT
R1:    .R1-1
I1:    .SA1-1
.N:    0
RB:    .RB-1
S7:    .S7
      .LOC    371

SA1:   .SA1-1
SA2:   .SA2-1
SA3:   .SA3-1
CA1:   .CA1-1
CA2:   .CA2-1
CA3:   .CA3-1

      .NREL
      LDA    1, S5
      STA    1, S5
B2:     LDA    1, ATLU
      STA    1, 20
      STA    1, 21
      LDA    1, NTLU
      STA    1, NTLU
B3:     LDA    1, 020
      MOVZR   1, 1
      STA    1, 021
      DSZ     .NTLU
      JMP     B3
      LDA    1, RS
      INC     1, 1
      STA    1, RS
      DSZ     .S5
      JMP     B2
      JSR     @CCAL
.S2:    JSR     @MCON
      LDA    1, RS
      JSR     @BD
      JMP     @S7

.STLU:  LDA    1, ATLU
      STA    1, 20
      STA    1, 21
      LDA    1, NTLU
      STA    1, NTLU
B1:     LDA    1, 020
      MOVZR   1, 1
      STA    1, 021
      DSZ     .NTLU
      JMP     B1
      LDA    1, RS
      INC     1, 1
      STA    1, RS
      LDA    1, MAN
      INC     1, 1
      STA    1, MAN
      JMP     @XP

```



```

ESR: STA 3, RESR
      LDA 2, TDF
      LDA 3, LCK

      AND# 2, 3, SZR
      JMP L15
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L14
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L13
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L12
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L11
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L10
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L9
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L8
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L7
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L6
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L5
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L4
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L3
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L2
      MOVZR 3, 3
      AND# 2, 3, SZR
      JMP L1

```

```

L5: .L5
L4: .L4
L3: .L3
L2: .L2
L1: .L1

```

```

L15: LDA 2, ET15
      ADD 1, 7
      STA 2, ET15
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST15
      ADD 1, 2
      STA 2, ST15
      ISZ N15
      JMP L8

L14: LDA 2, ET14
      ADD 1, 2
      STA 2, ET14
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST14
      ADD 1, 2
      STA 2, ST14
      ISZ N14
      JMP L8

L13: LDA 2, ET13
      ADD 1, 2
      STA 2, ET13
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST13
      ADD 1, 2
      STA 2, ST13
      ISZ N13
      JMP L8

L12: LDA 2, ET12
      ADD 1, 2
      STA 2, ET12
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST12
      ADD 1, 2
      STA 2, ST12
      ISZ N12
      JMP L8

L11: LDA 2, ET11
      ADD 1, 2
      STA 2, ET11
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST11
      ADD 1, 2
      STA 2, ST11
      ISZ N11
      JMP L8

```

```

ET15: 0
ET14: 0
ET13: 0
ET12: 0
ET11: 0
ST15: 0
ST14: 0
ST13: 0
ST12: 0
ST11: 0
N15: 0
N14: 0
N13: 0
N12: 0
N11: 0
L8: JMP @RESR
RESR: 0
AMPY: 0

```

```

L10: LDA 260
      ADD 2, ET10
      STA 2, ET10
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST10
      ADD 1, 2
      STA 2, ST10
      ISZ N10
      JMP L3

L9: LDA 2, ET9
      ADD 1, 2
      STA 2, ET9
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST9
      ADD 1, 2
      STA 2, ST9
      ISZ N9
      JMP L8

L8: LDA 2, ET8
      ADD 1, 2
      STA 2, ET8
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST8
      ADD 1, 2
      STA 2, ST8
      ISZ N8
      JMP L8

L7: LDA 2, ET7
      ADD 1, 2
      STA 2, ET7
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST7
      ADD 1, 2
      STA 2, ST7
      ISZ N7
      JMP L8

L6: LDA 2, ET6
      ADD 1, 2
      STA 2, ET6
      MOV 1, 2
      JSR @AMPY
      LDA 2, ST6
      ADD 1, 2
      STA 2, ST6
      ISZ N6
      JMP L8

```

```

ET10: 0
ET9: 0
ET8: 0
ET7: 0
ET6: 0
ST10: 0
ST9: 0
ST8: 0
ST7: 0
ST6: 0
N10: 0
N9: 0
N8: 0
N7: 0
N6: 0

```

```

.L5:  LDA      2,ET5
      ADD      1,2
      STA      2,ET5
      MOV      1,2
      JSR      @AMPY
      LDA      2,ST5
      ADD      1,2
      STA      2,ST5
      ISZ      N5
      JMP      L0
.L4:  LDA      2,ET4
      ADD      1,2
      STA      2,ET4
      MOV      1,2
      JSR      @AMPY
      LDA      2,ST4
      ADD      1,2
      STA      2,ST4
      ISZ      N4
      JMP      L0
.L3:  LDA      2,ET3
      ADD      1,2
      STA      2,ET3
      MOV      1,2
      JSR      @AMPY
      LDA      2,ST3
      ADD      1,2
      STA      2,ST3
      ISZ      N3
      JMP      L0
.L2:  LDA      2,ET2
      ADD      1,2
      STA      2,ET2
      MOV      1,2
      JSR      @AMPY
      LDA      2,ST2
      ADD      1,2
      STA      2,ST2
      ISZ      N2
      JMP      L0
.L1:  LDA      2,ET1
      ADD      1,2
      STA      2,ET1
      MOV      1,2
      JSR      @AMPY
      LDA      2,ST1
      ADD      1,2
      STA      2,ST1
      ISZ      N1
      JMP      L0
ET5:  0
ET4:  0
ET3:  0
ET2:  0
ET1:  0
ST5:  0
ST4:  0
ST3:  0
ST2:  0
ST1:  0
N5:   0
N4:   0
N3:   0
N2:   0
N1:   0
.END

```

A4.13 X - Y Plotter Control Subroutine

The plotter, device code 23, has 3 control lines

- 1 A - X direction
- 2 B - Y direction
3. C - Pen lift.

Subroutines CPB and CPE mark the start and the end of the frequency axis by drawing a small mark in the Y direction of $X = -1000_g$ and $X = 0_g$.

Subroutine SRTB moves the pen in the X direction by the value in TBI and then draws a vertical line from Y equal to the harmonic magnitude to $Y = 0$. Subroutine SRTC is used to plot the error $G_k - F_k$. It also moves the pen in the X direction by TBI and draws a vertical line from Y equal to the error value to $Y = -400_g$. The format of the plot is given in Fig.5.4 in chapter 5.2.1.

Subroutine DOR contains the Assembler instructions that control the plotter. The following convention is adopted for this subroutine.

Register 0 controls line A - X direction

Register 1 controls line B - Y direction

Register 2 controls line C - Pen lift.

The plotter has a built in delay of about 300 mS because of the inertia of the pen carriage. Subroutine DEL increases this delay to about 1 second.

Subroutine SRTB.

SRTB: STA 3,RET	Save return
MOVZR 1,1	Halve harmonic
LDA 0,.TB	Get current X coordinate
LDA 2,TB1	Get X shift
ADD 2,0	Calculate next X coordinate
STA 0,.TB	Store X coordinate
LDA 2,PU	Raise pen
JSR .DOR	Output the contents of registers 0,1 and 2 to the plotter control subroutine
LDA 2,PD	Lower pen
JSR .DOR	Output reg. 0,1,2 to plotter control subroutine
LDA 1,PU	Load zero into reg. 1.
JSR .DOR	Output reg. 0,1,2 to plotter control subroutine. The plotter draws a line proportional to the original contents of reg 1.
LDA 2,PU	Raise pen
JSR .DOR	Output reg. 0,1,2 to plotter control subroutine
JMP RET	Return

[illegible]

[illegible]

A4.14 The LINK Software

The LINK software¹ links all the subprograms into one program which is loaded into the computer core and run when the name of the program is keyed in. The programs are denoted as follows.

- 1) The Plotted Harmonics and Errors $DP(X)I$
 - 2) The Numerical Error Analysis $DV(X)I$
- (X) = 128,256,512,1024

The LINK software lists the subprograms names and core addresses.

```

: LINK(DP1281, #VDU, 0=DL, S=1000, BSR128:B, CUL128:B, MCN52:B, DP21:B, DP25:B, DP3X:B,
004X:B, D05X:B, DP61:B, DP7551:B, PLP5:B, RV0:B, DP125:B, DP143:B, ARTH:B

```

```

LINK(DP1231, #VNU, 0=DL, S=1000, BSR128:B, CUL128:B, MCN54:B, DP21:B, DP25:B, D
PX:B, D04X:B, D05X:B, DP61:B, DP7551:B, PLP5:B, RV0:B, DP125:B, DP143:B, ARTH:
B

```

```

DDOS 1 6 RELOCATING LINE# VEP 1 0 - 05/19/76 DP1281

```

TITLE	NREL	ZREL	START
D=DL			
S=1000			
.B128	001000	000000	
.C0L5	001667	000050	
.MCN4	002100	000000	
.P21	002476	000000	
.P25	002546	000050	
.P31	002576	000050	
.P32	002662	000050	
.P33	003016	000050	
.P34	003102	000050	
.P35	003166	000050	
.P36	003222	000050	
.P37	003406	000050	
.P38	003472	000050	
.P39	003556	000050	
.041	003642	000050	
.042	003670	000050	
.P43	003730	000050	
.044	003768	000050	
.045	004016	000050	
.046	004051	000050	
.047	004104	000050	
.048	004137	000050	
.049	004177	000050	
.R61	004232	000050	
.R61	004365	000050	
.P62	004524	000050	
.B62	004657	000050	
.C64	005005	000050	
.D64	005247	000050	
.E64	005500	000050	
.F64	005700	000050	
.R63	006175	000050	
.R63	006320	000050	
.R63	006465	000050	
.H63	006620	000050	
.I63	006757	000050	
.J63	006777	000050	
.K63	007176	000050	
.L63	007175	000050	
.I611	007332	000050	
.J61	007352	000050	
.P612	007511	000050	
.I64	007546	000050	
.H64	007566	000050	
.H64	007595	000050	
.O64	007597	000050	
.P61	010001	000050	
.P775	010005	000050	

: LINK(DP256),#VDU,0=DL,S=1000, RSP256:B, CCL256:B, MCN52:B, DP21:B, DP25:B, DP34:B,
 4X:B, D05X:B, DP61:B, DP7551:B, PLP5:B, RVO:B, DP125:B, DP143:B, ARH:B, HTPA:, ARTH:B

RIN:B, DP48:B, P63, DP6751:B, DP7571:B, P, POL6551:B, DP120, DP21, DP25, DP34, B
 B

DDOS 1.6 RELOCATING LINER VER 1.0 - 05/12/76 DP2561

TITLE NREL CREL START

0=DL

S=1000

.B256 001000 000050

.CCL5 002367 000050

.14 002610 000050

.P21 003176 000050

.P25 003246 000050

.P31 003276 000050

.P32 003362 000050

.P33 003516 000050

.P34 003662 000050

.P35 003666 000050

.P36 004012 000050

.P37 004106 000050

.P38 004172 000050

.P39 004238 000050

.Q41 004342 000050

.Q42 004376 000050

.P43 004430 000050

.Q44 004462 000050

.Q45 004516 000050

.Q46 004551 000050

.47 004604 000050

.Q48 004637 000050

.Q49 004677 000050

.R61 004732 000050

.R61 004865 000050

.R62 005224 000050

.R62 005257 000050

.D64 005306 000050

.D64 005747 000050

.E64 006280 000050

.F64 006420 000050

.R63 006675 000050

.R63 007066 000050

.G63 007165 000050

.H63 007320 000050

.I63 007457 000050

.J63 007477 000050

.K63 007636 000050

.L63 007675 000050

.I611 010002 000050

.J61 010002 000050

.K612 010211 000050

.I64 010240 000050

.M64 010366 000050

.4 010503 000050

.O64 010612 000050

.P61 010604 000050

.P755 011007 000050

.PLP5 011007 000050

LINK(DP5121, #VDU, 0=DL, S=1000, BSP512:B, CCL512:B, MCN52:B, DP21:B, DP25:B, DP3X:B, DP4X:B, DP5X:B, DP61:B, DP752:B, PLPG:B, RY0:B, DP125:B, DP143:B, HRTH:B

LINK(DP5121, #VDU, 0=DL, S=1000, DP5122:B, CCL512:B, MCN52:B, DP21:B, DP25:B, DP3X:B, DP4X:B, DP5X:B, DP61:B, DP752:B, PLPG:B, RY0:B, DP125:B, DP143:B, HRTH:B

LDOS 1.6 RELOCATING LINER VER 1.0 - 05/24/76 DP5121

TITLE	NREL	ZREL	START
-------	------	------	-------

0=DL

S=1000

B512	001000	000000	
------	--------	--------	--

.CCL5	002002	000000	
-------	--------	--------	--

.MCN4	004013	000000	
-------	--------	--------	--

.P21	004411	000000	
------	--------	--------	--

.P25	004451	000000	
------	--------	--------	--

.P21	004451	000000	
------	--------	--------	--

.P22	004470	000000	
------	--------	--------	--

.P23	004471	000000	
------	--------	--------	--

.P34	005010	000000	
------	--------	--------	--

.P35	005011	000000	
------	--------	--------	--

.P36	005020	000000	
------	--------	--------	--

.P37	005021	000000	
------	--------	--------	--

.P38	005460	000000	
------	--------	--------	--

.P39	005471	000000	
------	--------	--------	--

.Q41	005550	000000	
------	--------	--------	--

.Q42	005610	000000	
------	--------	--------	--

.P43	005640	000000	
------	--------	--------	--

.Q44	005676	000000	
------	--------	--------	--

.Q45	005721	000000	
------	--------	--------	--

.Q46	005764	000000	
------	--------	--------	--

.Q47	005817	000000	
------	--------	--------	--

.Q48	006002	000000	
------	--------	--------	--

.Q49	006112	000000	
------	--------	--------	--

.R61	006140	000000	
------	--------	--------	--

.R61	006100	000000	
------	--------	--------	--

.R62	006427	000000	
------	--------	--------	--

.R62	006572	000000	
------	--------	--------	--

.C64	006731	000000	
------	--------	--------	--

.D64	007162	000000	
------	--------	--------	--

.E64	007420	000000	
------	--------	--------	--

.F64	007601	000000	
------	--------	--------	--

.R62	010106	000000	
------	--------	--------	--

.R63	010391	000000	
------	--------	--------	--

.R63	010400	000000	
------	--------	--------	--

.R63	010523	000000	
------	--------	--------	--

.I63	010672	000000	
------	--------	--------	--

.J63	010712	000000	
------	--------	--------	--

.K63	011001	000000	
------	--------	--------	--

.L63	011106	000000	
------	--------	--------	--

.I611	011295	000000	
-------	--------	--------	--

.J61	011360	000000	
------	--------	--------	--

.K612	011404	000000	
-------	--------	--------	--

.I64	011461	000000	
------	--------	--------	--

.R64	011501	000000	
------	--------	--------	--

.R64	011501	000000	
------	--------	--------	--

```

.P64 011625 000000
.P61 011714 000000
P7502 012000 000000
.PLP6 012410 000000
.PVO 012501 000000
.P125 013707 000000
.P143 014605 000000
.MPY 016772 000000
.DRND 016790 000000
.DGUR 016791 000000
.SMB0 017017 000000
.RDEU 017041 000000
.TT10 017142 000000
017202 000000
026230

```

```
START ADDR 001000
```

SYMBOL TABLE

C16	000147	C161	000150	C12	000151	C321	000151
C4J	000153	C441	000154	CH1	000174	CR2	000175
CR3	000176	CCRL	000141	CFT51	000173	CP8	000140
CPE	000241	CSR	000112	CT1	000144	CT2	000145
CT3	000146	DEL	000146	DOP	000144	GETC	017141
IH1	000050	IH2	000053	IH3	000103	IH4	000054
IH5	000062	IH6	000104	IH7	000075	IH8	000101
IH9	000105	I11	000061	I12	000066	I13	000067
I14	000070	I15	000072	I16	000072	I17	000071
I18	000074	I19	000075	I19H	000043	MB	000044
MB0	000116	MB1	000117	MB10	000110	MB11	000111
MB12	000112	MB13	000113	MB14	000114	MB15	000115
MB16	000116	MB17	000117	MB18	000140	MB19	000141
MB2	000120	MB20	000142	MB21	000143	MB2	000121
MB4	000112	MB5	000113	MB6	000124	MB7	000125
MB8	000126	MB9	000127	MB1	000115	MC0N	000160
MSK1	000111	MSK2	000111	N	000114	NH	000110
PUTC	017162	011	004875	R1	000254	RB	000257
SR1	000101	SR2	000101	SR2	000172	SR01	000101
SR42	000102	SR43	000100	SR61	000201	SR62	000203
SR44	000101	SR64	000104	SR7	013016	SR64	000107
SR64	000106	SR69	000107	SR62	000112	SR1	000045
SR2	000146	SR3	000101	SR4	000041	SR5	000101
SR6	000177	SR62	000112	SR7	000100	SR8	000101
SR9	000101	SR1	000101	SR2	000100	SR7	000107
SR14	000100	SR1	000100	SR6	000105	SR11	000100
SR63	000100	SR64	000101	SR7	000100	SR8	000107
SR9	000110	SR61	000101	SR62	000115	SR12	000102
SP62	000116	SR61	000117	SR64	000104	SR64	000101
SP64	000106	SP61	000104	SP25	000165	SP211	000200
SP212	000101	SP211	000101	SP220	000101	SP251	000104
SP232	000105	SP231	000206	SP240	000207	SP251	000210
SP252	000101	SP261	000101	SP262	000112	SP271	000104
SP272	000110	SP271	000216	SP280	000117	SP290	000220
SP292	000101	SP411	000117	SP412	000112	SP421	000104
SP433	000220	SP421	000226	SP422	000227	SP441	000230
SP442	000101	SP411	000101	SP410	000101	SP411	000101
SP482	000101	SP482	000101	SP483	000101	SP484	000101
SP41	000100	SP411	000104	SP412	000105	SP42	000101
SP62	000101	SP64	000101	SP75	000101	SP76	000101
SP70	000101	SP70	000101	T81	000172	T80L	017071
CT1	000172	DH4	000101	D1V1	016772	D1V0	016774
DH3	000100	HS	000170	15	000171	MB	014711
MBV	000101	158	016772	SR60	000101	TLU	017101

```

:
: LINK(DP1024I, #VDU, 0=DL, S=1000, BSR1024:B, CCL1024:B, MCN52:B, DP21:B, DP25:B, DP2X:E
, DFP64X:B, D05X:B, DP61:B, DP7552:B, PLP6:B, RVO:B, DP125:B, DP143:B, ARTH:B

```

```

LINK(DP1024I, #VDU, 0=DL, S=1000, BSR1024:B, CCL1024:B, MCN52:B, DP21:B, DP25:
B, DP2X:E, D05X:B, D05X:B, DP61:B, DP7552:B, PLP6:B, RVO:B, DP125:B, DP143:B, AR
TH:B

```

DDOS 1.6 RELOCATING LIMER VER 1.0 - 05/22/76 DP1024I

TITLE	NREL	ZREL	START
-------	------	------	-------

0=DL

S=1000

B1024	0001000	0000000	
-------	---------	---------	--

.CCL5	0002002	0000000	
-------	---------	---------	--

.MCN4	0004001	0000000	
-------	---------	---------	--

.P21	0007011	0000000	
------	---------	---------	--

.P25	0007051	0000000	
------	---------	---------	--

.P21	0007111	0000000	
------	---------	---------	--

.P42	0007175	0000000	
------	---------	---------	--

.P33	0007221	0000000	
------	---------	---------	--

.P34	0007415	0000000	
------	---------	---------	--

.P35	0007501	0000000	
------	---------	---------	--

.P36	0007610	0000000	
------	---------	---------	--

.P37	0007721	0000000	
------	---------	---------	--

.P38	0100005	0000000	
------	---------	---------	--

.P39	0100071	0000000	
------	---------	---------	--

.041	0101155	0000000	
------	---------	---------	--

.042	0102210	0000000	
------	---------	---------	--

.P43	0102243	0000000	
------	---------	---------	--

.044	0102276	0000000	
------	---------	---------	--

.045	0102311	0000000	
------	---------	---------	--

.046	0103004	0000000	
------	---------	---------	--

.047	0104417	0000000	
------	---------	---------	--

.048	0104452	0000000	
------	---------	---------	--

.049	0105112	0000000	
------	---------	---------	--

.A61	0105445	0000000	
------	---------	---------	--

.B41	0107000	0000000	
------	---------	---------	--

.A62	0110227	0000000	
------	---------	---------	--

.B62	0111172	0000000	
------	---------	---------	--

.C64	0111321	0000000	
------	---------	---------	--

.D64	0111562	0000000	
------	---------	---------	--

.E64	0120070	0000000	
------	---------	---------	--

.F64	0122251	0000000	
------	---------	---------	--

.A63	0122500	0000000	
------	---------	---------	--

.B63	0122641	0000000	
------	---------	---------	--

.C63	0123000	0000000	
------	---------	---------	--

.H63	0123123	0000000	
------	---------	---------	--

.I62	0123272	0000000	
------	---------	---------	--

.J63	0123312	0000000	
------	---------	---------	--

.K63	0123451	0000000	
------	---------	---------	--

.L63	0123590	0000000	
------	---------	---------	--

.I631	0123630	0000000	
-------	---------	---------	--

.J63	0123665	0000000	
------	---------	---------	--

.K612	0140004	0000000	
-------	---------	---------	--

.I64	0140061	0000000	
------	---------	---------	--

.M64	0141101	0000000	
------	---------	---------	--

.N64	0141170	0000000	
------	---------	---------	--

.O64	0141170	0000000	
------	---------	---------	--

.P61	0141214	0000000	
------	---------	---------	--

.P62	0141214	0000000	
------	---------	---------	--

```

.PLP6 015040 000000
.RVO 015051 000000
.P125 015107 000000
.P143 015279 000000
.MPY 021112 000000
.DRFD 021142 000000
.D.S.R 021169 000000
.SPBR 021407 000000
.RDEC 021541 000000
.TTIO 021543 000000
      021560 000000
      020730

```

```
START ADDR 001000
```

SYMBOL TABLE

C16 000147	C161 000149	C32 000151	C721 000153
C64 000152	C641 000154	C81 000154	C82 000155
CR3 000276	CCAL 000042	CFTST 000072	CPB 000296
CPE 000341	CSR 000113	CTL 000144	CT2 000145
CT3 000146	DEL 000145	DOR 000144	GEYC 021541
IH1 000090	IH2 000053	IH3 000102	IH4 000054
I 000092	IH5 000104	IH7 000072	IH8 000051
IH9 000105	I11 000061	I12 000066	I13 000067
I14 000096	I15 000072	I16 000073	I17 000071
I18 000074	I19 000075	I194 000043	IB 000044
MB8 000116	MB1 000117	MB10 000118	MB11 000119
MB12 000122	MB13 000123	MB14 000124	MB15 000125
MB16 000126	MB17 000127	MB18 000128	MB19 000129
MB2 000120	MB20 000142	MB21 000143	MB2 000121
MB4 000122	MB5 000123	MB6 000124	MB7 000125
MB8 000126	MB9 000127	MB1 000125	MB10 000126
MSK1 000111	MSK2 000112	N 000124	NH 000125
PI10 011562	PI 1 000425	P1 000204	RE 000257
SR1 000171	SR2 000372	SR3 000373	SR61 000369
SR62 011592	SR63 000310	SR64 000301	SR62 000303
SR63 000111	SR64 000124	SCNT 011546	SR64 000365
SR44 000098	SR64 000207	SO63 000122	SH1 000045
SH2 000040	SH3 000043	SH4 000047	SH5 000051
SH6 000072	SH63 000117	SH7 000100	SH8 000101
SH9 000103	S11 000101	S12 000099	S13 000097
S 000094	S15 000064	S16 000065	S1611 000220
S173 000094	S164 000101	S17 000099	S18 000100
S19 000110	S661 000211	S663 000215	S1112 000222
SK63 000106	SL63 000117	SH64 000124	SH64 000125
SO64 000226	SP10 000164	SP25 000166	SP211 000200
SP112 000091	SP223 000167	SP229 000167	SP211 000200
SP115 000095	SP161 000106	SP162 000107	SP191 000210
SP233 000111	SP261 000111	SP163 000112	SP371 000210
SP374 000215	SP164 000216	SP182 000217	SP374 000220
SP392 000201	SP411 000125	SP412 000121	SP421 000120
SP422 000205	SP423 000206	SP424 000207	SP441 000220
SP442 000208	SP451 000210	SP452 000211	SP461 000212
SP462 000215	SP471 000216	SP472 000217	SP481 000240
SP482 000241	SP483 000242	SP491 000243	SP492 000244
SP61 000250	SP111 000254	SP112 000255	SP62 000251
SP63 000252	SP64 000253	SP75 000255	SP70 000252
SRT0 000143	ST10 000250	IB1 000173	.SDEC 021471
.C5 000177	0000 021141	.DIV1 021172	.DIVU 021174
.R 000260	.H5 000170	.I5 000171	.HE 017141
.MPY 021142	.SB 017273	.SR00 021417	.TLU 010210
.TLUD 010097			

: LINK(DV128I, #VDU, 0=DL, S=1000, GSP128:B, CCL128:B, DRXX:B
 LINK(DV128I, #VDU, 0=DL, S=1000, GSP128:B, CCL128:B, DRXX:B

DDOS 1.5 RELOCATING LINKER VER 1.0 - 06/22/76 DV128I

TITLE NREL ZREL START

0=DL

S=1000

G128 001000 000050

.CCL5 002267 000050

.MCN4 002510 000050

.P21 003176 000050

.P25 003246 000050

.P21 003276 000050

.P32 003362 000050

.P33 003516 000050

.P34 003602 000050

.P35 003666 000050

.P36 004012 000050

.P37 004106 000050

.P38 004172 000050

.P38 004256 000050

.Q41 004342 000050

.Q42 004375 000050

.Q43 004430 000050

.Q44 004463 000050

.Q45 004516 000050

.Q46 004551 000050

.Q47 004604 000050

.Q48 004617 000050

.Q49 004677 000050

.Q61 004732 000050

.Q61 005065 000050

.Q62 005224 000050

.Q62 005357 000050

.Q64 005516 000050

.Q64 005747 000050

.E64 006205 000050

.F64 006416 000050

.G63 006671 000050

.G63 007016 000050

.G63 007185 000050

.H63 007320 000050

.I63 007457 000050

.J63 007477 000050

.K63 007626 000050

.L63 007677 000050

.L611 010012 000050

.J61 010052 000050

.K612 010011 000050

.I64 010046 000050

.H64 010046 000050

.H64 010055 000050

.Q64 010042 000050

.F61 010001 000050

```

P7552 011065 000050
RVO 011171 000050
P125 012217 000050
P143 012215 000050
MPV 015512 000050
ORAO 015542 000050
OSOR 015400 000050
SNEO 015437 000050
BLTC 015511 000050
TTIO 015563 000050
      015622 000050
      025207

```

```

START ADDR      001000

```

SYMBOL TABLE

C16	000147	C161	000150	C32	000151	C721	000152
C64	000152	C641	000154	C81	000174	C82	000175
CA3	000175	CCAL	000145	CFTST	000271	CSR	000112
CT1	000144	CT2	000145	CT3	000146	GETC	015563
IH1	000050	IH2	000051	IH3	000103	IH4	000054
IH5	000052	IH6	000104	IH7	000055	IH8	000055
I4	000105	I11	000051	I12	000056	I13	000057
I4	000070	I15	000072	I16	000073	I17	000071
I18	000074	I19	000075	I15H	000043	NE	000044
ME8	000116	ME1	000117	ME10	000110	ME11	000111
ME12	000112	ME13	000113	ME14	000114	ME15	000115
ME16	000116	ME17	000117	ME18	000140	ME19	000141
ME2	000120	ME20	000142	ME21	000143	ME1	000121
ME4	000122	ME5	000123	ME6	000124	ME7	000125
ME8	000126	ME9	000127	MB1	000115	NCON	000160
MSK1	000111	MSK2	000112	N	000114	NH	000155
PUTC	015602	OL 1	002622	S1	000254	FB	000257
SA1	000171	SA2	000172	SA3	000173	SA61	000160
SA62	000162	SA63	000163	SEG1	000101	SE62	000103
SB63	000111	SC64	000104	SCNT	011456	ST64	000105
SE64	000106	SF64	000107	SG63	000112	SH1	000045
SH2	000044	SH3	000076	SH4	000047	SW5	000052
SH6	000077	SH63	000113	SH7	000100	SH8	000101
SH9	000102	S11	000051	S12	000056	S17	000057
S14	000050	S15	000054	S16	000065	S1611	000120
T163	000114	S164	000112	S17	000106	S18	000107
J18	000110	S161	000121	S163	000113	S1612	000122
SP63	000116	S165	000117	SH64	000124	SH64	000125
S064	000126	SP21	000104	SP25	000106	SP111	000100
SP312	000101	SP121	000102	SP122	000103	SP121	000104
SP312	000105	SP141	000106	SP142	000107	SP151	000110
SP152	000111	SP161	000112	SP162	000113	SP171	000114
SP172	000115	SP181	000116	SP182	000117	SP191	000120
SP192	000121	SP411	000122	SP412	000123	SP421	000124
SP422	000125	SP431	000126	SP432	000127	SP441	000129
SP442	000131	SP461	000132	SP452	000133	SP461	000134
SP462	000135	SP471	000136	SP472	000137	SP481	000140
SP482	000141	SP483	000142	SP491	000143	SP492	000144
SP61	000150	SP611	000151	SP612	000152	SP62	000153
SP63	000154	SP64	000155	SP75	000156	STLU	000150
T81	000175	B0EX	015611	C5	000172	I400	015563
DIW1	015417	DIWU	015414	OSOP	015400	W5	000170
I15	000171	M8	015511	KPY	015522	W6	012215
SM60	017407	TLU	012220	TLU0	012227		

A4.15. The Stored Table of Values STV

The format of the block is described in section A 3.10.2

The data is given in decimal form but the Assembler software converts this to octal code.

0
17
74
56
57
141
223
769
478
650
568
1411
2010
2358
4032
5744
6178
11520
16100
0
0
0
0
0
0
0
0
0
0
0
17
72
56
56
55
55
1411
2014
2012
4071
5071
6178
11507
16134
0
END

A5 The Fast Fourier Transform (FFT)

The input and output specifications and operating instructions are given in the listing at the end of this chapter. A discussion on the errors is given in reference 18.

A5.1 The Scale Factors MAN and SCNT

The FFT is programmed to allow the harmonics to have the maximum machine code values but not to overflow. Thus the harmonics are represented at maximum resolution but the scale is not compatible with that of the DFTTLU. If the FFT analyses a maximum dc level (Fig.A5.1) ie the ADC output is 2047_{10} , the harmonic G_0 always has a machine code value equivalent to 32768_{10} . The value of SCNT is dependent on N and is given in Table A5.1. These are the maximum values of SCNT and are termed MAN.

Table A5.2 lists the value of MAN where the input signal is time varying and the maximum value of the harmonics, $\frac{N}{2}$ has the value equivalent to 16384_{10} , 8192_{10} etc.

TABLE A5.1

N	MAN ^(MAX. SCNT)
128	3
256	4
512	5
1024	6

Table A.5.2 MAN for different N and $(\frac{N}{2})$

MAN	128	256	512	1024
3	15364			
4	8192	16384		
5	4096	8192	16384	
6	2048	4096	8192	16384
7	1024	2048	4096	8192
8		1024	2048	4096
9			1024	2048

When a noiselike signal is analysed, the maximum value of the harmonic is set by the corresponding value of MAN. eg for $N = 1024$ and $(\frac{N}{2}) = 8192$, $MAN = 7$. SCNT can be less than or equal to MAN depending on the amplitude of the signal. If SCNT is less than MAN, the harmonics are NOT to the scale and the scale must be adjusted by the difference between MAN and SCNT ie. All harmonics must be shifted by $MAN - SCNT$ times to the right.

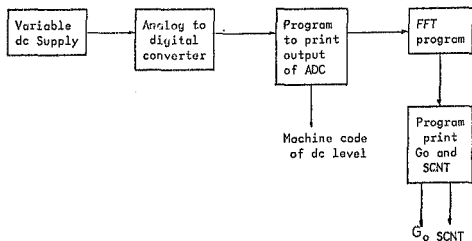


Fig.A5.1

A5.2 Discussion on the Accuracy of a Fixed Point FFT

In reference 18, Welch presents a fixed point FFT error analysis which compares the results of a fixed point FFT with those of a floating point FFT. The floating point FFT uses a word with a 27 bit mantissa and is considered to be the 'accurate' answer. The analysis results in an expression for the upper bound error which is confirmed with experimental results.

The expression for the upper bound error is

$$\frac{\text{rms (error)}}{\text{rms (result)}} \leq \frac{2^{(M+3)/2} 2^{-B} C}{\text{rms (initial sequence)}} \quad \text{A5.1}$$

$M = \log_2 N$

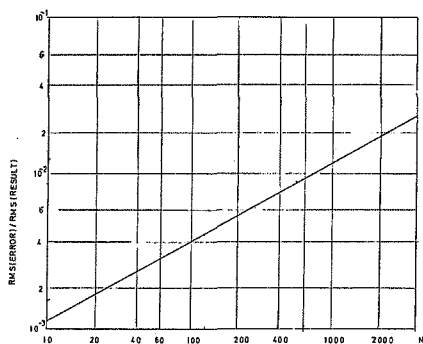
B = number of bits in the fixed point word excluding the sign bit.

= 15 (Nova 1200)

C = constant

= 0,9 (for 2's complement machine with truncation).

The signal used in the error analysis described has a ptp value of ± 1 and an rms value of 0,2. The variation of $\text{rms(error)}/\text{rms(result)}$ with N is given in fig. A5.2.



B=15

C=0.9

Input Signal. Random Numbers between -1 and +1, rms value=0.2

Fig.A.52 Theoretical Upper Bound of Error

NOVA FAST FOURIER TRANSFORM CALCULATION

DEPARTMENT OF ELECTRICAL ENGINEERING
UNIVERSITY OF THE #11#ALABAMA

APRIL 1972

THE DISCRETE TRANSFORM (DFT) OF A COMPLEX SERIES $F(N)$ IS

$$G(K) = \sum_{N=0}^{N-1} F(N) \cdot \exp(-j \cdot 2\pi \cdot N \cdot K / \text{NUM})$$

WHERE THE SUM IS FROM $N=0$ TO $N=\text{NUM}-1$, AND $L=2\pi / (\text{NUM})$

THE INVERSE TRANSFORM (IDFT) IS

$$F(L) = (1/\text{NUM}) \cdot \sum_{K=0}^{N-1} G(K) \cdot \exp(j \cdot 2\pi \cdot L \cdot K / \text{NUM})$$

AND THE SUM IS OVER K FROM 0 TO $\text{NUM}-1$

THE FACTOR $(1/\text{NUM})$ IS NOT INCLUDED IN THIS PROGRAM.

DEFINITIONS:

NUM IS THE NUMBER OF SAMPLE POINTS. IT MUST BE AN INTEGER POWER OF 2.
M IS THE INTEGER POWER OF 2, THUS $\text{NUM} = 2^M$.

N IS AN INDEX INDICATING THE ELEMENTS OF THE INPUT SERIES. THUS
 $X(1)$, $X(2)$, ..., $X(N)$, ..., $X(\text{NUM}-1)$ FORM THE INPUT SERIES X .

I IS AN INDEX INDICATING THE PARTIAL SUMS AS THE DFT IS CALCULATED.
THUS $I=0$ INDICATES THE INPUT ARRAY, $I=M$ INDICATES THE DFT WITH ITS
ELEMENTS IN HIT REVERSE ORDER.

CALLING SEQUENCE:

```

      LOC 400
JSR PS; LOC 5 CONTAINS STARTING ADDRESS OF DFT PROGRAM (7102)
A: <0 0H> 0 FOR FORWARD TRANSFORM, 1 FOR REVERSE.
  <NUM>
  <X(N)> REAL PART OF INPUT SERIES.
    :
    : THIS TAKES NUM LOCATIONS
  <X(NUM-1)>
  <Y(0)> IMAGINARY PART OF INPUT SERIES
    :
    : THIS ALSO TAKES NUM LOCATIONS
  <Y(NUM-1)>
  <CONTINUE MAIN PROGRAM HERE> THE ADDRESS OF THIS LOCATION
                                IS A + 2*NUM + 2

```

THE TRANSFORMED DATA WILL HAVE REPLACED THE INPUT DATA WHEN CONTROL
RETURNS FROM THIS SUBROUTINE. SEE SCMT FOR SCALING OF OUTPUT DATA.

NOTES:

SCALING. TO AVOID OVERFLOW EVERY ARRAY EXCEPT THE FIRST IS DIVIDED BY 2 IF IT HAS ANY ELEMENT LARGER THAN 31463 (OCTAL). THE CONDITION IS NOT NECESSARY ON A 16 BIT MACHINE.

CADITION: INPUT ARRAY DATA MUST BE LESS THAN $2^{*}14$ (DECIMAL) TO AVOID OVERFLOW ON THE I=1 ARRAY.

SCN1. THE NUMBER OF TIMES THE DATA HAS BEEN SCALED IS STORED IN LOC 7265. THE OUTPUT SERIES MUST BE MULTIPLIED BY $2^{*}SCN1$ FOR THE FORWARD TRANSFORM AND $2^{*}SCN1 - 1$ FOR THE INVERSE.

FIXED POINT. ALL SINES AND COSINES ARE MULTIPLIED BY $2^{*}14$ (DEC). ALL ARITHMETIC IS INTEGER MODE AND ALL DATA ARE ASSUMED INTEGER.

MAXIMUM LENGTH. THE INPUT SERIES IS LIMITED TO 1024 (DECIMAL) COMPLEX VALUES. A REAL SERIES OF DOUBLE LENGTH CAN BE TRANSFORMED FOR BROAD BAND SPECTRAL PURPOSES BY TREATING IT AS A COMPLEX SERIES OF HALF LENGTH.

COSINE ARRAY. LOCATIONS 6377 THROUGH 6777 CONTAIN ALL THE COSINES NECESSARY TO COMPUTE THE SINUSOIDAL FACTORS OF $EXP(2^{*}PI^{*}NSK/NUM)$. THEY ARE IN A FORMAT WHEREBY 1.0 IS REPRESENTED BY 40000 (OCTAL)

REENTRY. INITIAL VALUES FOR SUBROUTINE ARE ALL AUTOMATICALLY COMPUTED ON ENTRY. HENCE SUBROUTINE IS POTENTIALLY REENTRANT. IT DOES NOT NOW PROVIDE FOR SAVING OF AC'S AND C.

*U*U*U*

```

000002 .LUC 02
--- 000002 000000 NUM: 0
000003 000000 ALPHA: 0

```

```

000004 000000 N: 0
000005 007102 CF151: FF1ST

```

```

000006 000000 FLAG: 0
000007 000000 NUM4: 0

```

```

007000 .LUC 7000
07000 020424 FF1A: LDA 0,SPT
07001 101235 MOVSK# 0,0,SKP
07002 002530 JMP 06BWP
07003 030526 LDA 2,BETA
07004 034417 LDA 3,MAX4
07005 024007 LDA 1,NUM4
07006 133000 ADD 1,2
07007 151400 INC 2,2
07010 024414 LDA 1,SPT
07011 050030 STA 2,30
07012 050031 STA 2,31
07013 021400 LDA 0,0,3
07014 032030 LDA 2,030
07015 042031 STA 0,031
07016 051400 STA 2,0,3
07017 136400 SUB 1,3
07020 014007 DSE NUM4
07021 000772 JMP *-6
07022 002510 JMP 06BWP
07023 066777 MAX4: 0777
07024 000000 SPT: 0
07025 067404 FF1A: FFTWC

```

```

07026 054407 GETDA: STA 3,BACK
07027 133000 ADD 1,2
07030 052020 STA 2,020
07031 021000 LDA 0,0,2
07032 004443 JSK FF15C
07033 042021 STA 0,021
07034 062401 JMP 06BACK

```

```

07035 060000 BACK: 0

```

```

07036 101132 TEST: MOVZL# 0,0,SAC
07037 101241 MOVOR 0,0,SKP
07040 101220 MOVZK 0,0
07041 001400 JMP 0,3

```

```

07042 034467 FFTCC: LDA 3,BETA
07043 054020 STA 3,20
07044 054021 STA 3,21
07045 020426 LDA 0,0,0

```

07046 020000 LDA 1,0
 07047 123000 ADD 1,0
 07050 120520 SUBAL 1,1
 07051 101404 INC 0,0,SKP
 07052 125121 MOVSL 1,1,SKP
 07053 101001 MOV 0,0,SKP
 07054 000775 JMP *-3
 07055 044747 STA 1,SKP
 07056 000002 LDA 0,NUM
 07057 101223 MOVSL 0,0
 07060 101223 MOVSL 0,0
 07061 040007 STA 0,NUM4
 07062 040753 STA 0,BACK

07063 137000 ADD 1,3
 07064 021400 LDA 0,0,3
 07065 032020 LDA 2,020
 07066 042021 STA 0,021
 07067 051400 STA 2,0,3
 07070 014745 USE BACK
 07071 000772 JMP *-6
 07072 002733 JMP 06FF10

07073 177765 END -13
 07074 063077 FACF1: HALT

07075 024562 FFTSG: LDA 1,ATF+1
 07076 125014 MOV# 1,1,SKP
 07077 000737 JMP TEST

07100 001400 JMP 0,3
 07101 063077 HALT

07102 021400 FFTST: LDA 0,0,3
 07103 040006 STA 0,FLAG
 07104 021401 LDA 0,1,3
 07105 040002 STA 0,NUM
 07106 126440 SUBU 1,1
 07107 101223 MOVSL 0,0,SKP
 07110 125101 INC 1,1,SKP
 07111 000402 JMP *-2
 07112 060775 JMP *-3

07113 044004 STA 1,4
 07114 175400 INC 3,3
 07115 175400 INC 3,3
 07116 054003 STA 3,ALPHA
 07117 020002 LDA 0,NUM
 07120 105120 MOVSL 0,1
 07121 167000 ADD 3,1

07122 044410 STA 1,CLW1
 07123 126400 SUB 1,1
 07124 044532 STA 1,ALF
 07125 044532 STA 1,ALF+1
 07126 044537 STA 1,SCWT
 07127 044675 STA 1,SPF
 07130 080712 JMP FFICG

07131 006377 GETA: 6377
 07132 000000 GIMP: 0

1PAGES 142

07133 054522 CALC: STA 3,KEIN
 07134 024576 LDA T,IN
 07135 004531 JSR FFTAG
 07136 030512 LI, 2,SAP
 07137 050020 STA 2,20
 07140 030520 LDA 2,1AN
 07141 050021 STA 2,21
 07142 030003 LDA 2,ALPHA
 07143 024567 LDA 1,IN
 07144 004662 JSR GETDA
 07145 024002 LDA 1,NUM
 07146 004660 JSR GETDA
 07147 024564 LDA 1,IN
 07150 004656 JSR GETDA
 07151 024002 LDA 1,NUM
 07152 124400 NEG 1,1
 07153 004653 JSR GETDA

1PAGE 2

07154 024472 LDA 1,CUS
 07155 004557 JSR FFTN1
 07156 131000 MOV 1,2
 07157 024505 LDA 1,LEAF3
 07160 004554 JSR FFTN1
 07161 004561 JSR MULL
 07162 042472 STA 0,OSAV3
 07163 024464 LDA 1,5IN
 07164 004550 JSR FFTN1
 07165 131000 MOV 1,2
 07166 024475 LDA 1,LEAF4
 07167 004545 JSR FFTN1
 07170 004552 JSR MULL
 07171 032463 LDA 2,OSAV3
 07172 113000 ADD 0,2
 07173 024466 LDA 1,LEAF1
 07174 140400 NEG 2,0
 07175 133000 ADD 1,2
 07176 123000 ADD 1,0
 07177 052452 STA 2,OSAV1
 07200 042454 STA 0,OSAV3
 07201 004565 JSR FFTN1

```

07202 010454 ISZ AIF
07203 101000 MOV G,0
07204 111000 MOV G,2
07205 004561 JSR FFI1A1
07206 010450 ISZ AIF
07207 101000 MOV G,0
07210 024436 LDA 1,CUS
07211 004503 JSR FFI1A1
07212 131000 MOV 1,2
07213 024450 LDA 1,TEMP4
07214 004500 JSR FFI1A1
07215 004505 JSR MUL1
07216 042435 STA 0,OSAV4
07217 024430 LDA 1,SIN
07220 124400 NEG 1,1
07221 004513 JSR FFI1A1
07222 131000 MOV 1,2
07223 024441 LDA 1,TEMP3
07224 004510 JSR FFI1A1
07225 004515 JSR MUL1
07226 032435 LDA 2,OSAV4
07227 113000 ADD G,2
07230 140400 NEG 2,0
07231 024431 LDA 1,TEMP2
07232 130000 ADD 1,2
07233 123000 ADD 1,0
07234 052416 STA 2,OSAV2
07235 042416 STA 0,OSAV4
07236 004530 JSR FFI1A1
07237 010417 ISZ AIF
07240 101000 MOV G,0
07241 111000 MOV G,2
07242 004524 JSR FFI1A1
07243 010413 ISZ AIF
07244 101000 MOV G,0
07245 002416 JNP 0,NETN

```

```

07246 000000 CUS : 0
07247 000000 SIN : 0
07250 007250 SAP : SAP
07251 000000 SAV1 : 0
07252 000000 SAV2 : 0
07253 000000 SAV4 : 0
07254 000000 SAV3 : 0
07255 000000 RETN : 0
07256 000000 AIF : 0
07257 000000 AIFC : 0
07260 007260 IAN : IAN
07261 000000 TEMP1 : 0
07262 000000 TEMP2 : 0
07263 000000 TEMP4 : 0
07264 000000 TEMP3 : 0

```

```

07265 000000 SCW1 : 0

```

```

07260 054476 FFLAG: STA 00000V
07261 020573 LDA 0,1
07270 030004 LDA 2,0
07271 142405 SUB 2,0,SNC
07272 000404 JNP WID
07273 125220 MOVAR 1,1
07274 101404 INC 0,0,SNC
07275 000776 JNP *-2
07276 004565 WID: JNR FFLAG

```

```

07277 020007 LDA 0,0,0,4
07300 111000 MOV 0,2
07301 122422 SUB# 1,0,SEC
07302 000407 JNP *-1
07303 143000 ADD 2,0
07304 030625 LDA 2,BETA
07305 113000 ADD 0,2
07306 021000 LDA 0,0,2
07307 100400 NEG 0,0
07310 000404 JNP *-4
07311 030620 LDA 2,BETA
07312 133000 ADD 1,2
07313 021000 LDA 0,0,2
07314 040732 STA 0,CUS
07315 020007 LDA 0,0,0,4
07316 122032 ADC# 1,0,SEC
07317 122401 SUB 1,0,SXP
07320 106401 SUB 0,1,SXP
07321 105000 MOV 0,1

```

```

07322 030607 LDA 2,BETA
07323 133000 ADD 1,2
07324 021000 LDA 0,0,2
07325 030006 LDA 2,FLAG
07326 151232 MOVAR 2,2,SEC
07327 100400 NEG 0,3
07330 040717 STA 0,SIN
07331 002433 JNP 0,0,SAV
07332 000000 A: 0
07333 000000 A: 0

```

```

07334 125133 FFLAG: MOVAR 1,1,SNC
07335 001400 JNP 0,3
07336 124400 NEG 1,1
07337 010402 ISZ ASK
07340 001400 JNP 0,3

```

```

07341 000000 ASK: 0

```

07342 102460 MULT: SUBC 0,0
 07343 054421 STA 3,NSAV
 07344 054421 LDA 3,NSAV
 07345 125203 MOVCL: MOVCL 1,1,SNC
 07346 101201 MOVCL 0,0,SLK
 07347 143220 ADDCL 0,0
 07350 175404 INC 3,3,SLK
 07351 000774 JNP MOVCL
 07352 101100 MOVCL 0,0
 07353 125120 MOVCL 1,1
 07354 101100 MOVCL 0,0

07355 024764 LDA 1,ASF
 07356 125233 MOVCL# 1,1,SNC
 07357 002405 JNP NSAV
 07360 100400 NEG 0,0
 07361 126400 SUB 1,1
 07362 044757 STA 1,ASF
 07363 002401 JNP NSAV
 07364 000000 NSAV: 0
 07365 177760 R20: -20

07366 014670 FTA1: USE ATF
 07367 010667 ISZ ATF
 07370 001400 JNP 0,3

THE EST

07371 024412 LDA 1,CUTO
 07372 151132 MOVCL# 2,2,SNC
 07373 000404 JNP NSGA
 07374 132032 ADCCL# 1,2,SNC
 07375 001400 JNP 0,3
 07376 001401 JNP 1,3
 07377 124400 NSGA: NEG 1,1
 07400 132032 ADCCL# 1,2,SNC

07401 001401 JNP 1,3
 07402 001400 JNP 0,3

07403 031463 CUTO: 31463

07404 024004 FFINC: LDA 1,0
 07405 044452 STA T,ACNT
 07406 102520 SUBCL 0,0
 07407 040453 STA 0,1

07410 126400 NUUS: SUB 1,1
07411 044721 STA 1,N

07412 020450 AGE1: LDA 0,I
07413 030002 LDA 2,NUU
07414 102400 NEG 0,0
07415 151220 NUVER 2,2
07416 101404 INC 0,0,SEK
07417 000776 JNP *-2
07420 050713 STA 2,A
07421 050437 STA 2,NUWT

07422 006437 ROAD: JNR 0GCALC
07423 014435 DSE ACNT
07424 000427 JNP AIND
07425 010705 ISE N
07426 030705 LDA 2,A
07427 050431 STA 2,ACNT
07430 024702 LDA 1,N
07431 147000 ADD 2,1
07432 044700 STA 1,N
07433 030002 LDA 2,NUU
07434 152404 SUB 1,2,SEK
07435 000705 JNP ROAD
07436 014421 DSE ACNT
07437 000416 JNP AIND
07440 000434 JNP UUT

07441 020615 STSR: LDA 0,ATF
07442 101134 NUVEL# 0,0,SEK
07443 000403 JNP SCALE
07444 040613 STA 0,ATF+1
07445 000743 JNP NUUS

07446 010611 SCALE: ISE ATF+1
07447 010616 ISE SCNT
07450 102400 SUB 0,N
07451 040605 STA 0,ATF
07452 000736 JNP NUUS

07453 010657 AIND: ISE N
07454 000746 JNP ROAD

07455 010405 AIND: ISE I
07456 000763 JNP STSR

07457 000000 ALV1: 0
 07460 000000 ALV1: 0
 07461 007133 GCALC: CALC
 07462 000000 I: 0
 07463 030004 FTRV: LDA 2,N
 07464 121000 MOV 1,0
 07465 126400 SUB 1,1
 07466 150400 WGS 2,2
 07467 101200 MOVSK 0,0
 07470 125100 MOVL 1,1
 07471 151004 INC 2,2,SKR
 07472 000775 JNP *-3
 07473 001400 JNP 0,3

07474 024437 OUT: LDA 1,PHASE
 07475 044020 STA 1,20
 07476 024013 LDA 1,ALPHA
 07477 044433 STA 1,ALPHA
 07500 101001 MOV 0,0,SKP
 07501 002433 JNP OFFFA
 07502 126400 SUB 1,1
 07503 044627 STA 1,N
 07504 024002 LDA 1,NUM
 07505 044753 STA 1,RCV1

07506 024624 CYCLE: LDA 1,N
 07507 004754 JSK FTRV

07510 030422 LDA 2,ALPHA

07511 034621 LDA 3,N
 07512 130432 SUBS# 1,3,SEC
 07513 000407 JNP ECUAL
 07514 157000 ADD 2,3
 07515 133000 ADD 1,2
 07516 025000 LDA 1,0,2
 07517 021400 LDA 0,0,3
 07520 041000 STA 0,0,2
 07521 045400 STA 1,0,3

07522 010010 ECUAL: ISZ W
 07523 014730, DSE, WCVI
 07524 000762 JNP CYCLE
 07525 030405 LDA 2,ALPHA
 07526 024002 LDA 1,NUM
 07527 133000 ADD 1,2
 07530 050402 STA 2,ALPHA
 07531 002000 JNP 020
 07532 000600 ALPHA: 0

07533 007477 PHASE: OUT+3

006377 .LOC 6377

06400 040000 040000
06401 040000 040000
06402 037777 037777
06403 037773 037773
06404 037770 037770
06405 037765 037765
06406 037761 037761
06407 037754 037754
06410 037747 037747
06411 037741 037741
06412 037733 037733
06413 037724 037724
06414 037714 037714
06415 037704 037704
06416 037693 037693
06417 037681 037681
06420 037647 037647
06421 037634 037634
06422 037621 037621
06423 037605 037605
06424 037570 037570
06425 037553 037553
06426 037535 037535
06427 037517 037517
06430 037500 037500
06431 037480 037480
06432 037440 037440
06433 037417 037417
06434 037375 037375
06435 037353 037353
06436 037330 037330
06437 037305 037305
06440 037261 037261
06441 037235 037235
06442 037210 037210
06443 037162 037162
06444 037134 037134
06445 037105 037105
06446 037055 037055
06447 037025 037025
06450 036774 036774
06451 036743 036743
06452 036711 036711
06453 036657 036657
06454 036623 036623
06455 036570 036570
06456 036533 036533
06457 036477 036477
06460 036441 036441
06461 036403 036403
06462 036344 036344
06463 036305 036305
06464 036245 036245
06465 036205 036205

06466 036144 036144
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06470 036040 036040
06471 035775 035775
06472 035732 035732
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06474 035622 035622
06475 035555 035555
06476 035507 035507
06477 035441 035441
06500 035372 035372
06501 035323 035323
06502 035253 035253
06503 035202 035202
06504 035131 035131
06505 035060 035060
06506 035006 035006
06507 034733 034733
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06513 034453 034453
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06516 034241 034241
06517 034161 034161
06520 034102 034102
06521 034022 034022
06522 033741 033741
06523 033660 033660
06524 033576 033576
06525 033513 033513
06526 033430 033430
06527 033345 033345
06530 033261 033261
06531 033175 033175
06532 033110 033110
06533 033022 033022
06534 032734 032734
06535 032645 032645
06536 032556 032556
06537 032467 032467
06540 032377 032377
06541 032306 032306
06542 032215 032215
06543 032123 032123
06544 032031 032031
06545 031737 031737
06546 031643 031643
06547 031550 031550
06550 031454 031454
06551 031357 031357
06552 031262 031262
06553 031164 031164
06554 031066 031066
06555 030770 030770
06556 030671 030671
06557 030571 030571
06560 030471 030471
06561 030371 030371

06562 030370 030370
 06563 030160 030160
 06564 030064 030064
 06565 027762 027762
 06566 027657 027657
 06567 027554 027554
 06570 027450 027450
 06571 027344 027344
 06572 027237 027237
 06573 027132 027132
 06574 027025 027025
 06575 026917 026917
 06576 026810 026810
 06577 026701 026701
 06600 026372 026372
 06601 026262 026262
 06602 026152 026152
 06603 026041 026041
 06604 025930 025930
 06605 025817 025817
 06606 025705 025705
 06607 025593 025593
 06610 025480 025480
 06611 025365 025365
 06612 025250 025250
 06613 025136 025136
 06614 025021 025021
 06615 024905 024905
 06616 024787 024787
 06617 024672 024672
 06620 024554 024554
 06621 024437 024437
 06622 024320 024320
 06623 024203 024203
 06624 024085 024085
 06625 023967 023967
 06626 023849 023849
 06627 023730 023730
 06630 023612 023612
 06631 023494 023494
 06632 023375 023375
 06633 023257 023257
 06634 023138 023138
 06635 023020 023020
 06636 022901 022901
 06637 022783 022783
 06640 022664 022664
 06641 022546 022546
 06642 022427 022427
 06643 022309 022309
 06644 022190 022190
 06645 022072 022072
 06646 021953 021953
 06647 021835 021835
 06650 021716 021716
 06651 021598 021598
 06652 021479 021479
 06653 021361 021361
 06654 021242 021242
 06655 021124 021124

06656 017204 017204
06657 017053 017053
06660 016723 016723
06661 016571 016571
06662 016440 016440
06663 016306 016306
06664 016154 016154
06665 016022 016022
06666 015870 015870
06667 015535 015535
06670 015402 015402
06671 015247 015247
06672 015113 015113
06673 014757 014757
06674 014623 014623
06675 014467 014467
06676 014333 014333
06677 014176 014176
06700 014041 014041
06701 013704 013704
06702 013546 013546
06703 013411 013411
06704 013253 013253
06705 013114 013114
06706 012756 012756
06707 012620 012620
06710 012461 012461
06711 012322 012322
06712 012163 012163
06713 012023 012023
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06715 011524 011524
06716 011364 011364
06717 011224 011224
06720 011064 011064
06721 010723 010723
06722 010563 010563
06723 010422 010422
06724 010261 010261
06725 010120 010120
06726 007756 007756
06727 007615 007615
06730 007453 007453
06731 007312 007312
06732 007150 007150
06733 007006 007006
06734 006644 006644
06735 006501 006501
06736 006337 006337
06737 006174 006174
06740 006032 006032
06741 005667 005667
06742 005524 005524
06743 005361 005361
06744 005216 005216
06745 005053 005053
06746 004707 004707
06747 004544 004544
06750 004401 004401
06751 004235 004235

06752 004071 004071
06753 003726 003726
06754 003562 003562
06755 003416 003416
06756 003252 003252
06757 003106 003106
06760 002742 002742
06761 002576 002576
06762 002432 002432
06763 002265 002265
06764 002121 002121
06765 001755 001755
06766 001610 001610
06767 001444 001444
06770 001300 001300
06771 001133 001133
06772 000767 000767
06773 000622 000622
06774 000456 000456
06775 000311 000311
06776 000145 000145
06777 000000 000000
•END

A 007333
 ACNT 007457
 AGE1 007412
 AIND 007455
 ALPHA 000003
 ALPHA 007532
 ASK 007341
 ATP 007256
 ATFC 007257
 BACK 007035
 BETA 007131
 CALC 007133
 CFI 01 000005
 COS 007246
 CUTO 007403
 CYCLE 007506
 EQUAL 007522
 FACPT 007074
 FTAG 007266
 FIAT 007366
 FICC 007042
 FINC 007404
 FINI 007334
 FTRA 007000
 FTRV 007463
 FTS 007075
 FTSI 007102
 FLAG 000006
 GBP 007132
 GCALC 007461
 GELDA 007126
 GFFA 007534
 GFFIN 007025
 I 007402
 J 000004
 M20 007365
 MAX4 007023
 MID 007276
 MLOOP 007345
 MY 007073
 NSAV 007364
 NULT 007342
 N 007332
 NCNT 007460
 NEGA 007377
 NIND 007453
 NUDS 007416
 NUM 000002
 NUM4 000007
 OUT 007474
 PHASE 007533
 RETW 007255
 RUAD 007422
 SAP 007250
 SAV1 007251
 SAV2 007252
 SAV3 007254
 SAV4 007253
 SCALE 007446
 SCNT 007265

SIN 007241
SPP 007024
STSN 007441
TAN 007260
TEMP1 007261
TEMP2 007262
TEMP3 007264
TEMP4 007263
TEST 007026

A6 System to Perform Error Tests

Fig. A6.1 shows the error test system block diagram. The system can be divided into 2 parts,

- 1) The Hardware ie the noise generators, amplifiers etc.
- 2) The Software ie. the FFT and DFTTLU programs.

A6.1 The Hardware

The hardware consists of a noise generator, filter set, amplifier and attenuator. The noise generator has a frequency range of 20Hz to 20KHz at a voltage of 1 volt peak to peak. The noise, filtered by the filter set, is amplified to approximately 10V peak to peak and is fed to three inputs.

- 1) The ADC, used in conjunction with the FFT.
- 2) A true r.m.s. voltmeter.
- 3) An attenuator set to approximately 12dB which attenuates the signal to about 2.5V peak to peak. This signal is fed to the LADC and is processed by the DFTTLU.
- 4) An oscillator controlled pulse generator controls the sampling rate which is set at 20,48 KHz.

A6.2 Notes on the System

- 1) The filter set allows a variety of noise signals to be generated ie bandpass, band reject and low pass wide and narrow band signals.
- 2) The oscillator sets the sampling rate of the system. For a sampling rate of 20,48 KHz the following integral multiples of frequencies can be extracted.

N	freq (Hz)
128	160
256	80
512	40
1024	20

3) Noise generator is set so that rms value of noise at the 12 bit A/D is 2 volts (Peak value of noise generator output is 5 times its rms value)

4) The LADC and ADC are peripherals of the Nova 1200

but the sampling rate in this case is controlled externally

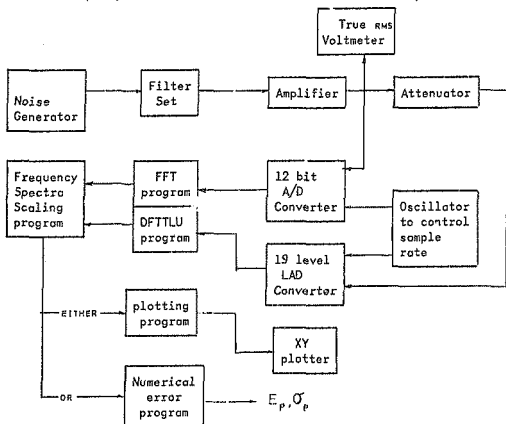


Fig.A6.1 Block Diagram of System to Measure Errors

A6.3 Scaling the Input Signals

The ADC has a peak to peak (ptp) voltage swing of approximately -10V to +10V. The binary output for the maximum positive level and maximum negative level is equivalent to 2047_{10} and -2048_{10} respectively. The LADC has a ptp voltage swing of approximately $\pm 2.5V$. Sign magnitude notation is used and the binary output is equivalent to $\pm 18_{10}$. The attenuator must be set so that a peak signal gives maximum output at both analog to digital converters. The attenuator in Fig.A6.2 is set to a nominal value of 12dB and a short program is written to print the output of both analog to digital converters. The dc supply is adjusted until the printer shows that the ADC output is equivalent to 2047_{10} . The attenuation is then adjusted until the printer shows that the LADC output is equivalent to 18_{10} . The value of the attenuation is 11,7dB.

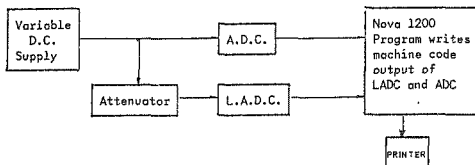


Fig.A6.2 System to calibrate the FFT and DF1TLU

A6.4 Specifications and Interconnection
Diagram of Error Test System

<u>Instrument</u>	<u>Store Number</u>
1. Noise Generator: Rohde and Schwarz Type SVF BN 4150 30 Hz - 6MHz	
2. Filter Set: (1) Bruel and Kjaer. Filter Set Type. 1614. (2) Krohn - Hite Model 3550 2Hz - 200KHz	AL41
3. Amplifier: Bruel and Kjaer Measuring Amplifier Type 2609 20Hz - 20 000 Hz	
4. Attenuator: Marconi Instruments MF Attenuator TF 2162 DC - 1MHz	AL15
5. ADC: Experimental Instrument	
6. LADC: Experimental Instrument	
7. Plotter System: (1) DAC. Experimental Instrument (2) Hewlett-Packard 7005B X - Y Recorder	R-17
8. Pulse Generator: Hewlett Packard Type 80034	
9. Oscillator: General Radio Corp Type 1309-A 10Hz - 100KHz	102-30

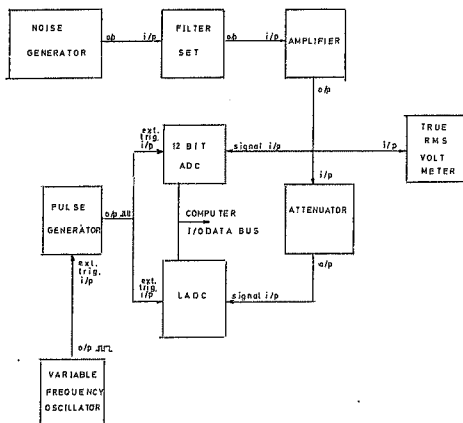


Fig. A 5.3 DETAILED INTERCONNECTIONS

A7 A Simple Worked Example of an 8 point DFTTLU

The example has the following specifications.

- 1) The X channel has 5 linearly spaced quantising levels.
- 2) The Y channel has 4 sinusoidally spaced abscissas
- 3) The tangent rule is used to solve the integration in both channels.
- 4) $N = 16$

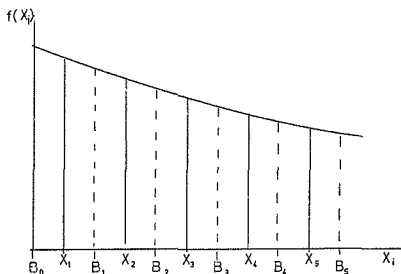


Fig.A 7.1 X Channel Quantising Levels

A7.1 The X Channel

The quantising thresholds are placed in the centre of each panel.

The area of the i th panel is $(B_i - B_{i-1}) f(X_i)$.

The total area under the function is

$$\int_0^1 f(x) dx \doteq \sum_{i=1}^5 a_i$$

$$\begin{aligned}\sum_{i=1}^5 a_i &= \sum_{i=1}^5 (B_i - B_{i-1}) f(x_i) \\ &= h_x \sum_{i=1}^5 w_i f(x_i)\end{aligned}$$

Now $X_5 \equiv 1$ and the abscissas are linear

$$B_i - B_{i-1} = 0,2 = w_i$$

i	1	2	3	4	5
w _i	0,2	0,2	0,2	0,2	0,2

s	1	2	3	4	5
$\sum_{i=1}^s w_i$	0,2	0,4	0,6	0,8	1,0

$$s = 1, M_x$$

M_x is the number of
quantising levels

$$M_x = 5$$

$$w_i = 0,2$$

$$h_x = 1$$

A7.2 TheY Channel

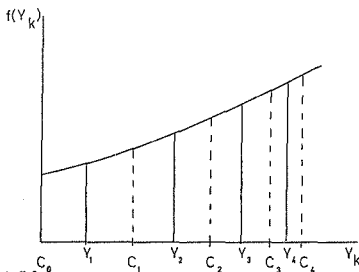


Fig. A 7.2

$$C_k = \sin\left(\frac{k\pi}{8}\right), \quad k = 0, 1, 2, 3, 4 \quad y_k = \frac{C_k + C_{k-1}}{2}$$

The area, a_k , of the k th panel $= (C_k - C_{k-1}) f(y_k)$

The total area under the function is $\int_0^1 f(y) dy \doteq \sum_{k=1}^4 a_k$

$$\begin{aligned} &= \sum_{k=1}^4 (C_k - C_{k-1}) f(y_k) \\ &= h_y \sum_{k=1}^4 u_k f(y_k) \end{aligned}$$

ie. $h_y = 1$

$$u_k = C_k - C_{k-1}$$

k	1	2	3	4
u_k	0,38	0,32	0,22	0,08

r	1	2	3	4
$\sum_{k=1}^r u_k$	0,38	0,70	0,92	1,00

M_y = number of
quantising levels

$$r = 1 \dots M_y$$

$$M_y = 4$$

Equivalent signed address generator output	Y channel weight contribution to STV
$0 \leq \theta < \frac{\pi}{8}$	0,38
$\frac{\pi}{8} \leq \theta < \frac{2\pi}{8}$	0,70
$\frac{2\pi}{8} \leq \theta < \frac{3\pi}{8}$	0,92
$\frac{3\pi}{8} \leq \theta \leq \frac{4\pi}{8}^*$	1,00

* The limits of this level are defined as in A1.2.3.

A7.4 The Derivation of the STV

$$S(s, r) = \sum_{\text{row}}^s \sum_{\text{column}}^r w_i u_k \quad \left. \begin{array}{l} s = 1 \dots M_x \\ r = 1 \dots M_y \end{array} \right\}$$

The two dimensional array is derived as follows

s \ r	1	2	3	4
1	(0,38)(0,20)	(0,70)(0,20)	(0,92)(0,20)	(1,00)(0,20)
2	(0,38)(0,40)	(0,70)(0,40)	(0,92)(0,40)	(1,00)(0,40)
3	(0,38)(0,60)	(0,70)(0,60)	(0,92)(0,60)	(1,00)(0,60)
4	(0,38)(0,80)	(0,70)(0,80)	(0,92)(0,80)	(1,00)(0,80)
5	(0,38)(1,00)	(0,70)(1,00)	(0,92)(1,00)	(1,00)(1,00)

eg. $S(2,3) = (0,92)(0,40)$

Fig.A 7.3 STV Array

D_x and D_y are scaling factors. If the STV is set up in a minicomputer, the machine code representation is usually a different set of values. D_x and D_y are the scaling factors of these values.

In this case $D_x = 1$ $D_y = 1$

A7.5 Simple Fourier Analysis

The signal to be analysed is a 16 point sampled sine wave.

Consider the system in Fig.2.3. 'Clock 1' is initially set to the same frequency as 'Clock 2' ie $k = 1$. 'Clock 1' is then set to double the frequency of 'Clock 2' ie. $k = 2$.

Equation 2.32 is used.

k refers to frequency index in this section

$$\overline{xy} = \frac{h_x h_y}{D_x D_y N} \sum_{n=0}^{N-1} \text{sgn}(x(t), y(t)) S(I_n K_{nk})$$

$$\overline{xy} = \frac{1}{16} \sum_{n=1}^{16} \text{sgn}(x(t), y(t)) S(I_n K_{nk})$$

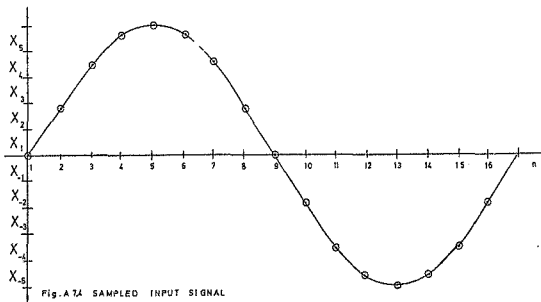


Fig. A.7A SAMPLED INPUT SIGNAL

TABLE
A.7.1

time n	I_n	K_{n1}	K_{n2}	$S(I_n K_{n1})$	$S(I_n K_{n2})$
1	x_1	y_1	y_1	$(0,38)(0,20)$	$(0,38)(0,20)$
2	x_2	y_2	y_3	$(0,70)(0,40)$	$(0,92)(0,40)$
3	x_4	y_3	y_4	$(0,92)(0,80)$	$(1,00)(0,80)$
4	x_5	y_4	y_3	$(1,00)(1,00)$	$(0,92)(1,00)$
5	x_5	y_4	$-y_1$	$(1,00)(1,00)$	$(0,38)(1,00)(-1)$
6	x_5	y_4	$-y_3$	$(1,00)(1,00)$	$(0,92)(1,00)(-1)$
7	x_4	y_3	$-y_4$	$(0,92)(0,80)$	$(1,00)(0,80)(-1)$
8	x_2	y_2	$-y_3$	$(0,70)(0,40)$	$(0,92)(0,40)(-1)$
9	$-x_1$	$-y_1$	y_1	$(0,38)(0,20)$	$(0,38)(0,20)(-1)$
10	$-x_2$	$-y_2$	y_3	$(0,70)(0,40)$	$(0,92)(0,40)(-1)$
11	$-x_4$	$-y_3$	y_4	$(0,92)(0,80)$	$(1,00)(0,80)(-1)$
12	$-x_5$	$-y_4$	y_3	$(1,00)(1,00)$	$(0,92)(1,00)(-1)$
13	$-x_5$	$-y_4$	$-y_1$	$(1,00)(1,00)$	$(0,38)(1,00)$
14	$-x_5$	$-y_4$	$-y_3$	$(1,00)(1,00)$	$(0,92)(1,00)$
15	$-x_4$	$-y_3$	$-y_4$	$(0,92)(0,80)$	$(1,00)(0,80)$
16	$-x_2$	$-y_2$	$-y_3$	$(0,70)(0,40)$	$(0,92)(0,40)$
		$Ck_2 = Ck_1$	$Ck_2 \cdot Ck_1$	$\sum = 10,22$	$\sum = 0,00$
				$Ck_2 = Ck_1$	$Ck_2 \cdot Ck_1$

$S(I_{n, K_{nk}})$ is the array in A7.3

Table A7.1 gives the quantised values of I_n of the signal as well as the values of K_{n1} and K_{n2} , that with I_n , form the address pairs of the STV. (I_n, K_{n1}) and (I_n, K_{n2}) are listed.

There is clearly, harmonic at $k = 2$ as the signal is a pure sine wave of frequency $k = 1$.

$$\text{ie. } \overline{xy}/k = 1 = \frac{1}{16}(10.22)$$

$$\overline{xy}/k = 2 = 0$$



Author Cohen David Stephen

Name of thesis The Implementation Of The Discrete Fourier Transform By Table Look Up Technique. 1976

PUBLISHER:

University of the Witwatersrand, Johannesburg

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