

## **APPENDIX D MAGNETIC SALIENCY AND THE GENERATOR TRANSIENT VOLTAGE**

This appendix shows magnetic saliency affects the value the transient generator voltage has.

### **D.1 $|E'_{KBG}|$ WHEN MAGNETIC SALIENCY IS CONSIDERED**

The steady state operating point of the Koeberg generator of the improved two generator model shown in Chapter 3, figure 3.25 is  $P = 450$  MW,  $Q = 13.6$

MVAR and  $|V_{KBG LV}| = 1.005$  per unit.

The q-axis synchronous reactance of the Koeberg machine, expressed on a 1072 MVA base, is  $x_q = 2.28$  per unit.

The angle,  $\delta$ , between the generator q-axis and the terminal voltage can be computed using (Appendix F, equation F.7):

$$\delta = \tan^{-1} \left( \frac{x_q P}{V^2 + x_q Q} \right) \quad (D.1)$$

$\delta$  obtained for the Koeberg generator is:

$$\begin{aligned} \delta &= \tan^{-1} \left( \frac{x_q P}{V^2 + x_q Q} \right) \\ &= \tan^{-1} \left[ \frac{2.28 * \left( \frac{450}{1072} \right)}{(1.005)^2 + 2.28 * \left( \frac{13.6}{1072} \right)} \right] \\ &= 42.65^\circ \end{aligned} \quad (D.2)$$

The d- and q-axis components of the terminal voltage,  $V$ , at Koeberg can be computed by using equation F.8.  $V_d$  and  $V_q$  are:

$$\begin{aligned}
V_d &= V \sin(\delta) \\
&= 1.005 \sin(42.65^\circ) \\
&= 0.6809
\end{aligned} \tag{D.3-a}$$

$$\begin{aligned}
V_q &= V \cos(\delta) \\
&= 1.005 \cos(42.65^\circ) \\
&= 0.7392
\end{aligned} \tag{D.3-b}$$

The d- and q-axis components of the stator current at Koeberg, expressed on a 1072 MVA base, are (Appendix F, equation F.16):

$$\begin{aligned}
I_d &= \frac{-PV_d - QV_q}{-V_d^2 - V_q^2} \\
&= \frac{-\left(\frac{450}{1072}\right) * 0.6809 - \left(\frac{13.6}{1072}\right) * 0.7392}{-(0.6809)^2 - (0.7392)^2} \\
&= 0.2923 \text{ per unit; } S_{BASE} = 1072 \text{ MVA}
\end{aligned} \tag{D.4-a}$$

$$\begin{aligned}
I_q &= \frac{QV_d - PV_q}{-V_d^2 - V_q^2} \\
&= \frac{\left(\frac{13.6}{1072}\right) * 0.6809 - \left(\frac{450}{1072}\right) * 0.7392}{-(0.6809)^2 - (0.7392)^2} \\
&= 0.2987 \text{ per unit; } S_{BASE} = 1072 \text{ MVA}
\end{aligned} \tag{D.4-b}$$

The d- and q-axis transient reactances of the Koeberg machine, expressed on a 1072 MVA base are  $x'_d = 0.395$  per unit and  $x'_q = 0.689$  per unit. Hence, the transient voltage of the Koeberg generator is (Appendix F, equation F.1):

$$\begin{aligned}
E'_{KBG} &= (V_d - x'_q I_q) + j (V_q + x'_d I_d) \\
&= E'_d + j E'_q \\
&= (0.6809 - 0.689 * 0.2987) + j (0.7392 + 0.395 * 0.2923) \\
&= 0.4751 + j 0.8547 \\
&= 0.9778 \angle (90^\circ - 60.93^\circ) \\
&= 0.9778 \angle 29.07^\circ
\end{aligned} \tag{D.5}$$

## D.2 $|E'_{KBG}|$ WHEN MAGNETIC SALIENCY IS NOT CONSIDERED

For the case where the generator is modelled using the constant voltage behind transient reactance model  $E'_{KBG}$  can be computed using [1, 187]:

$$E'_{KBG} = V + (R_a + j x'_i) I \tag{D.6}$$

$R_a$  is very small and is usually neglected.

The constant voltage behind transient reactance generator model does not consider magnetic saliency.

When magnetic saliency is not modelled armature reaction,  $x'_i$ , should be computed using [41, p84]:

$$x'_i = \left( \frac{x'_d + x'_q}{2} \right) \tag{D.7-a}$$

For the Koeberg generator  $x'_i$ , expressed on a 1072 MVA base, is:

$$\begin{aligned}
&= \left( \frac{0.395 + 0.689}{2} \right) \\
&= 0.542
\end{aligned} \tag{D.7-b}$$

Hence,  $E'_{KBG}$  is:

$$\begin{aligned}
 E'_{KBG} &= V + j x_i \frac{S}{V} \\
 &= 1.005 + j 0.542 \frac{\sqrt{\left(\frac{450}{1072}\right)^2 + \left(\frac{13.6}{1072}\right)^2}}{1.005} \\
 &= 1.005 + j 0.2265 \\
 |E'_{KBG}| &= 1.03 \text{ p.u.}
 \end{aligned} \tag{D.8}$$